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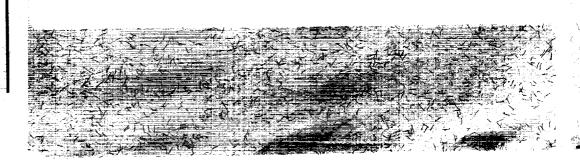
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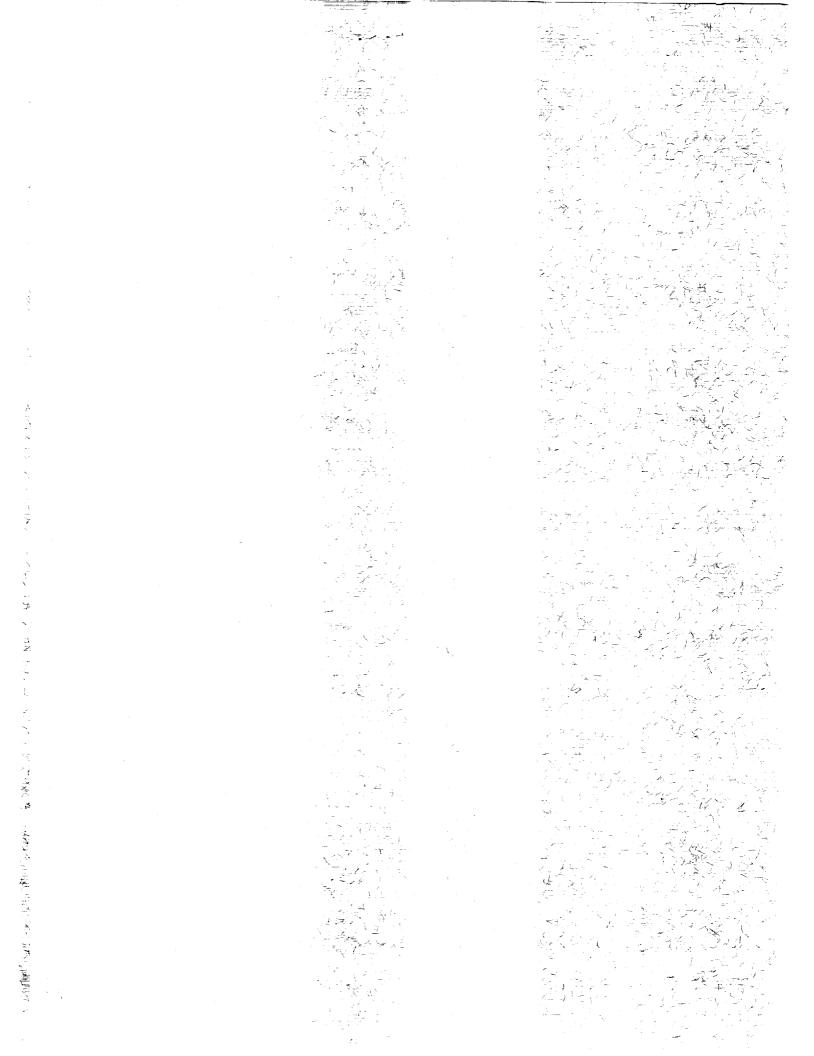
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Summary

A parametric study has been conducted in the Langley 16-Foot Transonic Tunnel on an isolated nonaxisymmetric fuselage model that simulates a twin-engine fighter. The effects of aft-end closure distribution (top/bottom nozzle-flap boattail angle versus nozzle-sidewall boattail angle) and afterbody and nozzle corner treatment (sharp or radius) were investigated. Four different closure distributions with three different corner radii were tested. Tests were conducted over a range of Mach numbers from 0.40 to 1.25 and over a range of angles of attack from -3° to 9°. Solid plume simulators were used to simulate the jet exhaust.

An analysis of the results of this study indicates that for a given closure distribution in the range of Mach numbers tested, the sharp corner nozzles generally have the highest drag and the 2-in. corner-radius nozzles generally have the lowest drag. The effect of closure distribution on afterbody drag is highly dependent on configuration, plume simulation, and Mach number. Except at high subsonic Mach numbers, the nozzles with the top and bottom terminal boattail angle $(\beta_{t,\mathrm{top/bot}})$ of 17.3° and sidewall terminal boattail angle $(\beta_{t,\mathrm{side}})$ of 9.7° generally have the lowest drag for the plume-on configurations, whereas the nozzles with $\beta_{t,\text{top/bot}} = \beta_{t,\text{side}} = 16.4^{\circ}$ generally have the lowest drag for the plume-off configurations. The nozzles with $\bar{\beta}_{t,\text{top/bot}} = 15.0^{\circ}/\beta_{t,\text{side}} = 22.4^{\circ}$ generally have the highest drag. However, the nozzles with $\beta_{t,\mathrm{side}} = 0^{\circ}$ have the lowest drag in the range of Mach numbers (approximately between 0.90 and 0.95) where the pressure recovery on the surfaces of the other nozzles is not sufficient to produce dragreducing positive pressures. Further trade studies are necessary to determine which range of Mach numbers is most mission critical in order to choose the most beneficial closure distribution. All the nozzles had lower drag with the solid plume simulators installed (simulating a fully expanded jet exhaust) than with them removed (simulating a nonoperating jet).

Introduction

The mission of the next generation of fighter aircraft will dictate a highly versatile and maneuverable vehicle that is capable of operating over a wide range of flight conditions. These aircraft require variable-geometry nozzles that change the aft-end shape, closure (the ratio of nozzle exit area to maximum fuselage cross-sectional area), and local boattail angle continuously throughout the operating range of Mach number, angle of attack, and engine pressure ratio. As demonstrated by test results, many studies have shown the importance of minimizing adverse interference from propulsion exhaust-system integration. (See refs. 1 to 3.) In these studies the afterbodies of various aircraft, which accounted for only a small portion of the total aircraft, produced 38-50 percent of the total aircraft drag. These studies examined axisymmetric nozzles at cruise operating conditions with boattail angles of 15° to 20°. Current interest in nonaxisymmetric nozzles led to the study of twin-engine configurations with rectangular afterbodies and nozzles that achieved aft-end closure with large, variable boattail angles of the upper and lower nozzle flaps with the nozzle sidewalls having a small or 0° boattail angle (ref. 4). These results indicated that the best subsonic/transonic performance was obtained with nozzles having terminal boattail angles between 7.8° and 20°.

In order to obtain the required aft-end closure and maintain the recommended boattail angles, nozzles with nonzero sidewall boattail angles The study reported in referwere investigated. ence 5 examined three nonaxisymmetric nozzles with chord boattail angles (β_c) of $\beta_{c,\text{top/bot}}/\beta_{c,\text{side}} =$ $11.0^{\circ}/19.5^{\circ}, 13.5^{\circ}/13.5^{\circ}, 15.0^{\circ}/7.5^{\circ},$ and it concluded that the nozzle with $\beta_{c,\text{top/bot}} = \beta_{c,\text{side}}$ had the lowest nozzle drag and generally the least unfavorable tail interference. Since reference 5 considered only three nozzles, a more detailed investigation was warranted.

This paper presents the results of a parametric study in which aft-end closure distribution (top/ bottom nozzle-flap boattail angle $(\beta_{t,top/bot})$ versus nozzle-sidewall boattail angle $(\beta_{t,\text{side}})$ afterbody and nozzle corner treatment (sharp or radius) were varied. Four different closure distributions $(\beta_{t,\text{top/bot}} = 17.9^{\circ}/\beta_{t,\text{side}} = 0^{\circ}, \beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}, \beta_{t,\text{top/bot}} = \beta_{t,\text{side}} = 16.4^{\circ}, \text{ and } \beta_{t,\text{top/bot}} = 15.0^{\circ}/\beta_{t,\text{side}} = 22.4^{\circ})$ with three different corner radii (sharp, 1 in., and 2 in.) were tested. Tests were conducted on an isolated nonaxisymmetric fuselage model that simulated a twinengine fighter. The model was tested in the Langley 16-Foot Transonic Tunnel over a range of Mach numbers from 0.40 to 1.25, Reynolds numbers per foot of 2.25×10^6 to 4.20×10^6 , and angles of attack from -3° to 9° . Solid plume simulators of constant cross section were used to simulate fully expanded jet exhaust.

Symbols and Abbreviations

base area of solid plume simulator $A_{
m base}$ or nozzle exit (when solid plume is removed), in²

nozzle exit area, in² A_e

$A_{ m max}$	model fuselage maximum cross-	p_{∞}	free-stream static pressure, psi
	sectional area, in ²	q_{∞}	free-stream dynamic pressure, psi
$A_{ m seal}$	cross-sectional area enclosed by seal strip at M.S. 33.10, in ²	R	local corner radius, in.
<i>A</i> .	nozzle throat area, in ²	w_e	nozzle exit width (see fig. 3), in.
$rac{A_t}{ ext{AR}}$		x	distance from nozzle connect station
AII	nozzle throat aspect ratio, Throat width/Throat height		(M.S. 41.27) along model longitudinal axis, in.
C_A	corrected axial-force coefficient,	Y	local half-width of nozzle, in.
C	$F_A/q_{\infty}A_{ m max}$	y	lateral distance from model centerline,
$C_{A,\mathrm{bal}}$	axial-force coefficient measured by balance, $F_A/q_{\infty}A_{\max}$	4.	in.
C_D	drag coefficient measured by balance,	y_R	lateral distance of local corner-radius center from model centerline, in.
	$\mathrm{Drag}/q_{\infty}A_{\mathrm{max}}$	Z	local half-height of nozzle, in.
$C_{D,f}$	skin-friction drag coefficient on nozzle	z	vertical distance from model center-
$C_{D,p}$	pressure drag coefficient on nozzle with solid plume simulator, computed		line, in.
	by pressure integration	z_R	vertical distance of local corner-radius center from model centerline, in.
$(\Delta C_{D,i})_{ m plume}$		α	angle of attack, deg
	interference	eta_c	chord boattail angle, deg
C_p	static pressure coefficient, $(p-p_{\infty})/q_{\infty}$	eta_t	terminal boattail angle (see fig. 3), deg
$C_{p, m crit}$	critical static pressure coefficient (sonic flow)	Subscripts:	angle (we ag o), deg
c	chord of model support strut	plume off	solid plume simulator removed (blank-
D_f	sum of skin-friction drag on cen-	nluma an	ing plate installed)
	terbody section from M.S. 33.10 to M.S. 41.27 and on solid plume, when	plume on	solid plume simulator present
	present, lbf	side	nozzle sidewall
d_e	equivalent diameter of nozzle exit, in.	top/bot	top and bottom nozzle flaps
d_f	equivalent diameter of model fuselage,	Abbreviation	
	in.	B.L.	buttline, measured laterally from model centerline, positive to right
F_A	corrected axial force, positive when measured in streamwise direction, lbf	M.S.	model station, measured aft from
$F_{A,\mathrm{bal}}$	axial force measured by balance, lbf	TT / Y	model nose, in.
h_e	nozzle exit height (see fig. 3), in.	W.L.	waterline, measured vertically from model centerline, positive up
l	nozzle length, 9.5 in.		
M_{∞}	free-stream Mach number	Apparatus and Methods	
p	local static pressure on nozzle, psi	Facility	
		I his inves	tigation was conducted in the Langley

This investigation was conducted in the Langley 16-Foot Transonic Tunnel, which is a continuous-flow, single-return, atmospheric wind tunnel with a slotted octagonal test section and continuous air exchange. The wind tunnel has a continuously variable airspeed up to a Mach number of 1.30 with test-section plenum suction used for speeds above a Mach

 \bar{p}_i

 \bar{p}_{base}

 \bar{p}_{es}

average static pressure on solid-plume-

simulator base or nozzle-exit base, psi

average static pressure at external seal

at metric break (M.S. 33.10), psi

average internal static pressure, psi

number of 1.05. A complete description of the facility and operational characteristics can be found in reference 6.

Model Design and Support System

The model tested, which was an isolated non-axisymmetric fuselage that simulated a twin-engine fighter, was mounted on a sting-strut support as shown in figure 1. This type of support system was chosen to minimize the effects of the support system on the afterbody flow. The model consisted of four parts: the forebody from M.S. 0.00 to M.S. 33.10, the centerbody from M.S. 33.10 to M.S. 41.27, the nozzle from M.S. 41.27 to M.S. 50.77, and the solid plume simulator from M.S. 50.77 to M.S. 62.15. Photographs of the model and support system installed in the Langley 16-Foot Transonic Tunnel are shown in figure 2.

The parameters selected for study were afterbody and nozzle corner radius and nozzle closure distribution (top/bottom nozzle-flap boattail angle versus nozzle-sidewall boattail angle). Model design began by specifying the maximum cross-sectional area (fuselage centerbody). Typical of twin-engine models previously tested (refs. 4 and 5), a 5.00-in-high by 10.00-in-wide rectangle was chosen with corner radius as the parameter to be varied. Three different forebody/centerbody combinations were designed with corner radii of 0.05 in. (sharp), 1 in., and 2 in. with a maximum cross-sectional area of the fuselage of 49.99 in^2 , 49.12 in^2 , and 46.57 in^2 , respectively. For each corner radius, the centerbody (M.S. 33.10 to M.S. 41.27) had a constant cross section. Three forebodies were then designed, one to join smoothly with each of the three centerbodies. The most aft section of each forebody had the same dimensions and corner radius as its corresponding centerbody and was faired forward by decreasing cross-sectional area and corner radius to a sharply pointed conical nose. To minimize strut interference on the metric portion of the model, forcbody length was chosen so that the metric break was at least one equivalent fuselage diameter (that is, $d_f = 2\sqrt{A_{
m max}/\pi})$ downstream of the strut trailing edge.

To establish a criterion for the model afterbody and nozzle closure (the ratio of nozzle exit area to maximum fuselage cross-sectional area), typical current twin-engine fighters (e.g., the F-15 and F-18) were examined. These aircraft have a ratio of combined (dry power) nozzle throat area to maximum fuselage cross-sectional area $(2A_t/A_{\rm max})$ of about 0.11. For the previously chosen maximum cross-sectional area of approximately 50.00 in², this ratio

gives a nozzle throat area of 2.75 in^2 per engine. A nozzle expansion ratio (A_e/A_t) of 1.15 was chosen as being typical of a nozzle at transonic flight, thus giving a combined nozzle exit area of 6.33 in^2 . All nozzles were designed with this exit area except for the nozzles with zero sidewall boattail angle, which had an exit area of 6.88 in^2 to allow for an internal longitudinal stiffener for structural considerations in a nozzle with internal flow.

Previous studies (e.g., ref. 4, which was also conducted in the 16-Foot Tunnel at Mach numbers similar to those of the present investigation) indicated that to maintain attached flow, the boattail angles should not exceed 20°. Nozzle length was chosen to be 9.50 in. (measured from the nozzle-to-centerbody connect station at M.S. 41.27) so that this maximum boattail angle criterion would be met for most of the closure distributions. To minimize support system interference in the region of interest, the length of the centerbody was chosen so that the beginning of the nozzle boattail would be greater than two equivalent fuselage diameters downstream of the strut trailing edge. This results in an overall model length of approximately 60 in., which is typical of 1/12-scale twin-engine fighter models tested in the 16-Foot Tunnel. A sketch of the nozzle geometry is shown in figure 3.

With the centerbody and nozzle exit areas determined, four fuselage closure distributions (top/ bottom nozzle-flap boattail angle versus nozzlesidewall boattail angle) shown in figure 4 were selected: zero sidewall boattail angle ($\beta_{t,\text{side}} = 0^{\circ}$) from which $\beta_{t,\text{top/bot}} = 17.9^{\circ}$ and AR = 14.49 are derived; equal top/bottom nozzle-flap boattail and nozzlesidewall boattail angles ($\beta_{t,\text{top/bot}} = \beta_{t,\text{side}} = 16.4^{\circ}$) which gives AR = 5.76; and two additional closure distributions where $\beta_{t, \mathrm{top/bot}} = 17.3^{\circ}, \beta_{t, \mathrm{side}} = 9.7^{\circ},$ and AR = 9.23 and $\beta_{t,\mathrm{top/bot}} = 15.0^{\circ},\,\beta_{t,\mathrm{side}} = 22.4^{\circ},$ and AR = 3.28. A nozzle with each closure distribution was then mated to each of the three centerbodies (sharp, 1-in., and 2-in. corner radii) to complete a matrix of 12 nozzles. The most forward section of each nozzle had the same dimensions as its corresponding centerbody. In the case of the 1-in. and 2in. corner-radius nozzles, the corner radius decreased along the nozzle length to a value of 0.05 in. (sharp) at the nozzle exit. The sharp-corner (0.05 in.) nozzles maintained this corner radius along the entire length of the nozzle, and therefore they are described completely in figure 3. Cross-sectional coordinates of the 1- and 2-in. corner-radius nozzles tested are given in table 1. The coordinates x, y_R , and z_R in table 1 were measured from the wind tunnel model, and the corner radius R was computed from these coordinates. The apparent discontinuity in corner radius is an artifact of this calculation and is not evident in the model.

To simulate fully expanded jet exhaust (except for the jet entrainment effects), a solid plume simulator having a constant cross section of the same dimensions as the nozzle exit was employed. (See fig. 2(b).) The solid plume simulator extended downstream four equivalent diameters of the nozzle exit (that is, $d_e = 2\sqrt{A_e/\pi}$). Solid plumes have been verified as reasonable approximations of the fully expanded exhaust plume of axisymmetric nozzles at an angle of attack of 0° (ref. 7). To determine the effect of the solid plume simulator on flow over the nonaxisymmetric nozzles of this investigation, a blanking plate was substituted for the solid plume simulator at the nozzle exit (plume off) as shown in figure 2(a). Because of structural considerations, the configurations with the solid plume simulator were tested only at an angle of attack of 0°.

Since the aft end is the region of interest, only the model aft of M.S. 33.10 was metric (mounted on the force balance). A clearance gap (metric break) was provided between the nonmetric and metric portions of the model at M.S. 33.10 to prevent fouling of the components upon each other. A flexible plastic strip inserted into circumferentially machined grooves in the components on either side of the metric break impeded flow into or out of the model cavity. The low coefficient of friction of the plastic strip minimized restraint between the metric and nonmetric portions of the model.

Instrumentation

Forces and moments on the metric portion of the model (aft of M.S. 33.10) were measured by a sixcomponent strain gauge balance that had an accuracy of ± 1.25 lb in axial force and ± 4 lb in normal force. Five static pressures were measured in the gap at the metric break (M.S. 33.10) external to the plastic seal strip. These pressure orifices were spaced about the right side of the model perimeter on the forebody. An additional two pressures were measured inside the model cavity at the metric break. These pressures were measured with individual pressure transducers, each with an accuracy of ± 0.013 psi. Ten static pressures were measured that were spaced on the right side of the solid-plumesimulator base. When the solid plume simulator was removed, the nozzle exit was sealed by a blanking plate, and five static pressure orifices were spaced across the width of the nozzle exit to measure the exit base pressure. These base pressures were measured with electronically scanned pressure modules

with an accuracy of ± 0.075 psi. These pressure measurements (external seal, internal cavity, and base) were then used to correct axial force measured by the balance for pressure-area tares as discussed in the "Data Reduction" section.

One hundred and ten static pressure orifices were located on the left side of the nozzle in 12 longitudinal rows as described in figure 5: four rows (42 orifices) on the upper (or "top") nozzle flap, three rows (28 orifices) on the lower (or "bottom") nozzle flap, and four rows (40 orifices) on the nozzle sidewall. Individual orifice locations for each nozzle are given in table 2. All model pressures were measured with electronically scanned pressure modules with an accuracy of ± 0.075 psi, and the modules were located in the (metric) model afterbody. Data obtained during each tunnel run were recorded on magnetic tape and were reduced with standard data reduction procedures. For each data point, 50 samples of data were recorded over a period of 5 sec and were averaged.

Tests

This investigation was conducted in the Langley 16-Foot Transonic Tunnel at Mach numbers from 0.40 to 1.25, Reynolds numbers per foot of 2.25×10^6 to 4.20×10^6 , and angles of attack from -3° to 9° . As recommended in references 8 and 9, all tests were conducted with a 0.125-in-wide boundary-layer transition strip consisting of No. 120 silicon carbide grit sparsely distributed in a thin film of lacquer. This strip was located 1.0 in. from the tip of the forebody nose.

Data Reduction

Corrections. The strain gauge balance, which was mounted on the model centerline, measured the forces and moments due to the external flow field on the portion of the model (external and internal) aft of M.S. 33.10. In order to achieve the correct axial force, the axial force measured by the balance must be corrected for pressure-area tare forces acting on the model. The internal pressure at any given set of test conditions was uniform throughout the inside of the model; thus, no cavity flow was indicated. The external and internal pressure tare forces on the model were obtained by multiplying the difference between the average pressure (external seal, base, or internal pressures) and free-stream static pressure by the affected projected area normal to the model axis. Axial force was computed from the balance axial force with the following relationship:

$$\begin{split} F_A &= F_{A,\text{bal}} + (\bar{p}_{es} - p_{\infty})(A_{\text{max}} - A_{\text{seal}}) \\ &+ (\bar{p}_i - p_{\infty})A_{\text{seal}} - (\bar{p}_{\text{base}} - p_{\infty})A_{\text{base}} - D_f \end{split} \tag{1}$$

where the first term $(F_{A,\text{bal}})$ includes all pressure and viscous forces on the model aft of M.S. 33.10. The second and third terms account for the forward seal rim and the interior pressure forces at the metric break, respectively. A negative differential pressure acting at the metric break, which is forward of the balance center (see fig. 1), causes a thrust tare. The fourth term accounts for the pressure forces on the base of either the solid plume simulator or the nozzle exit when the solid plume simulator is removed. A negative differential pressure acting at the plume or nozzle base, which is aft of the balance center, causes a drag tare. The last term (D_f) is the sum of the skin-friction drag on the centerbody section from M.S. 33.10 to M.S. 41.27 and on the solid plume simulator when present. The skin-friction drag of all components was computed using the method of Frankl and Voishel (refs. 10 and 11) for compressible turbulent flow on a flat plate. The exact calculation method is described in detail in reference 11. An example (nozzle 10 with solid plume simulator) of the relative sizes of each of the terms in equation (1) is presented in coefficient form in chart A. Also presented in coefficient form is the balance accuracy $(\pm 1.25 \text{ lb}).$

The adjusted forces and moments were then transferred from the body axis of the metric portion of the model to the stability axis. The attitude of the metric afterbody relative to gravity was determined from a calibrated attitude indicator located in the (metric) model centerbody. Angle of attack α , which is the angle between the afterbody centerline and the relative wind, was determined by applying a flow angularity term to the angle measured by the attitude indicator. The flow angularity adjustment was 0.1° , which is the average angle measured in the Langley 16-Foot Transonic Tunnel.

Calculations. The plume-interference drag increment was defined as

$$(\Delta C_{D,i})_{\text{plume}} = (C_D)_{\text{plume on}} - (C_D)_{\text{plume off}}$$
 (2)

where $(C_D)_{\text{plume on}}$ is the measured nozzle drag for a given nozzle with the solid plume simulator on, and $(C_D)_{\text{plume off}}$ is the measured nozzle drag for the same nozzle with the solid plume simulator off (nozzle exit blanking plate installed). Hence, this interference increment represents the interference effects of the solid plume simulator on the nozzle.

Nozzle boattail static pressures were integrated to determine nozzle pressure drag $C_{D,p}$ for the nozzles with the solid plume simulator installed. Since successful pressure integration is dependent on the density of the pressure taps, only the pressures on the upper quadrant of the nozzle, which contains 72 of the 110 orifices, were used for the pressure drag integration. This was a reasonable approach since the nozzle was symmetric about both the vertical and horizontal axes, and all data for these configurations (plume on) were obtained at a nominal angle of attack of 0°. If an individual pressure measurement was bad (from a plugged orifice, for instance), a pressure from the corresponding location on the bottom of the model was substituted where possible. An example of the grid used to divide the nozzle area is shown in figure 6. The axially and normally projected areas and the wetted area of each panel were computed, and the panels were then assigned to a pressure orifice with each panel area multiplied by 4.0 to account for the entire nozzle. From an examination of the pressure data, which will be presented in the "Discussion" section, it was determined that pressures changed rapidly along the length of the nozzle boattail, but they were fairly constant laterally across the nozzle flap or sidewall (except near the corners). An attempt was made to assign a panel to a given orifice based on this knowledge of the pressure distribution. (See fig. 6.)

Chart A

M_{∞}	C_A	$C_{A,\mathrm{bal}}$	First term	Second term	Third term	$C_{D,f}$	Accuracy
0.402	0.0179	0.0392	-0.0064	-0.0182	-0.0269	0.0236	±0.0180
.900	.1650	.1871	0066	0158	0212	.0209	$\pm .0055$
1.202	.2417	.2847	0085	0198	0051	.0198	$\pm .0044$

Presentation of Results

The results of this investigation, including repeated conditions, are presented in both tabular and plotted form. Table 3(a) presents an index of the configurations tested, and table 3(b) presents an index to the data presented in tables 4 to 21 and in figures 7 to 17. No data are presented for nozzles 1 and 4 (see table 3(a)), and for some nozzles, only the plume-on data or only the plume-off data are presented. Data for these configurations, as well as data at some Mach numbers for the other configurations, were compromised because of instrumentation problems encountered during testing. In cases where the data from an individual orifice in a key location were bad (for example, a plugged orifice), the pressure distribution was faired with a dashed line estimating the shape of the distribution.

Discussion

Basic Data

Pressures.Static pressure coefficients on the nozzle boattail and the effect of the solid plume simulator (when available) are shown in figure 7 at Mach numbers of 0.60, 0.90, and 1.20. Data for other Mach numbers may be found in tables 4 to 21. The external flow over all nozzle surfaces having a nonzero boattail angle (which excludes the sidewalls of nozzles 5 and 9) exhibited a strong expansion at the beginning of the nozzle boattail. This expansion was strong enough to produce a region of supersonic flow for $M_{\infty} \geq 0.70$ or $M_{\infty} \geq$ 0.80, depending on the boattail angle of the nozzle surface. At the lower subsonic Mach numbers, the initial expansion was followed by a strong pressure recovery as the flow continued downstream. This strong pressure recovery was sufficient to produce positive pressure coefficients which, when acting on the aft-facing nozzle boattail, decreased the drag on the nozzle.

If the initial expansion was strong enough to produce supersonic flow and the minimum pressure coefficient in the expansion was much less than $C_{p,\text{crit}}$, the region of supersonic flow terminated in a standing shock. Downstream of the shock, flow separation probably occurred as indicated by the suddenly reduced slope or flattening of the pressure recovery.

The external flow over the sidewalls of nozzles 5 and 9 ($\beta_{t,\text{side}} = 0^{\circ}$, see figs. 7(g) to 7(i) and 7(r) to 7(t), respectively) exhibits a weak expansion and pressure recovery at subsonic Mach numbers. The expansion is sufficient to produce local supersonic flow at $M_{\infty} \geq 0.875$ (as shown in the data tables).

At $M_{\infty}=0.60$, the downstream pressure recovery is generally sufficient to produce positive pressure coefficients. The pressure orifices located along the top/side corner are in a region where the boattail angle is transitioning from the top nozzle-flap boattail angle to $\beta_{t,\mathrm{side}}=0^{\circ}$, and therefore pressures measured at this orifice row follow the same trends as pressures along a nonzero boattail angle surface.

The shape of the pressure distributions is consistent between the top and bottom nozzle flaps. However, at $M_{\infty} = 0.60$, the initial expansion is generally slightly stronger on the top nozzle flap than on the bottom flap although the pressure recovery is generally similar. At $M_{\infty} = 0.90$ the situation is reversed (a slightly stronger initial expansion on the bottom flap than on the top). Since the pressure gradients are steep at the beginning of the nozzle boattail, the pressure orifices may not be placed at the exact location of the maximum expansion. Therefore, the observed expansion-strength differences between the top and bottom flaps may actually be expansionlocation differences. Since these differences are small. only the pressures from the top quadrant were used in the pressure integration, as was discussed in the "Data Reduction" section.

Keeping in mind the limitations of orifice location discussed previously, one would expect that the strength of the initial flow expansion over the nozzle boattail and the following pressure recovery would be strongly dependent on the boattail angle of the surface, but this is generally not the case. Examine, for example, the pressure distributions in figures 7(a) and 7(b) (nozzle 2 with $\beta_{t, \mathrm{top/bot}} = 17.3^{\circ}/\beta_{t, \mathrm{side}} =$ 9.7°). At $M_{\infty} = 0.60$ (fig. 7(a)), the expansion on the top and bottom nozzle flaps is much stronger than on the nozzle sidewalls, as would be expected since $\beta_{t,\text{top/bot}} > \beta_{t,\text{side}}$, but at $M_{\infty} = 0.90$ (fig. 7(b)) the expansion on the nozzle sidewalls is stronger. Also, nozzles 3, 7, and 11 (figs. 7(d) to 7(f), 7(m) to 7(o), and 7(x) to 7(z), respectively), which have $\beta_{t,\text{top/bot}} = \beta_{t,\text{side}} = 16.4^{\circ}$, have different pressure distributions on the top and bottom nozzle flaps and nozzle sidewalls.

At all but a few locations, nozzle pressure coefficients are higher with the solid plume simulator installed than with it removed (nozzle exit blanking plate installed). The shape of the pressure distribution is generally unaffected. Notable exceptions are pressure distributions over the bottom flaps of nozzles 5, 11, and 12 at $M_{\infty} = 1.20$ (figs. 7(i), 7(z), and 7(cc), respectively). In these cases, the separated flow downstream of the standing shock behaves differently for simulated plume-on and plume-off

conditions. The reasons for this difference are not known. As was noted in reference 7, solid plume simulators are reasonably effective at duplicating the effects of the exhaust plume of axisymmetric nozzles operating at design conditions. Therefore, the nozzle pressures with the solid plume simulators installed, compared with the nozzle pressures with the solid plume simulators off, should correspond to an operating and nonoperating jet, respectively. Nozzle boattail pressure coefficients were observed to be higher with an operating jet than with a nonoperating jet in the investigations of references 5, 12, and 13. The external flow over a nozzle with a nonoperating jet (solid plume simulator off) must expand over the nozzle boattail to fill in the large base region at the nozzle exit. This expansion acts to lower pressures on the nozzle boattail. When the jet is operating (solid plume simulator on), this expansion of the external flow is reduced, thus increasing boattail pressures.

 $Nozzle\ drag\ characteristics.$ The various component drag coefficients for each of the nozzles tested are presented in figure 8 as a function of freestream Mach number. The left-hand plots show a comparison of several computed components of total drag: skin-friction drag on the nozzle $(C_{D,f})$ (from M.S. 41.27 to M.S. 50.77); pressure drag on the nozzle with the solid plume simulator $(C_{D,v})$ obtained from pressure integration; and the drag interference increment due to the solid plume simulator $((\Delta C_{D,i})_{\mathrm{plume}})$ (when data are available for both plume-on and plume-off cases). The right-hand plots show a comparison of the drag measured by the force balance C_D with the sum of $C_{D,f}$ and $C_{D,p}$. The plume-interference increment was not included in this summed drag coefficient because the effect of the plume is to change the nozzle boattail pressures, and therefore it is already included in the integrated pressure drag coefficient. Similarly, wave-drag coefficient (for $M_{\infty} \ge 1.0$) was not determined separately since it is also included in $C_{D,p}$.

Figure 8 clearly shows that pressure drag is the largest contributor to nozzle drag at all Mach numbers by exhibiting the classic sharp rise in drag coefficient as subsonic Mach number increases above $M_{\infty}=0.70$, and then the decrease in drag coefficient as Mach number continues to increase supersonically. As expected, the skin-friction drag coefficient was small and remained nearly constant across the range of Mach numbers tested. The plume-interference increments were negative and were fairly constant over the range of Mach numbers tested. Negative plume-interference increments would be expected from the previous discussion of the pressure distributions. Since the boattail pressures are lower

in the absence of the solid plume simulator, higher drag occurs for plume-off configurations.

An examination of the right-hand plots of figure 8 shows that the sum of pressure drag coefficient and skin-friction drag coefficient (both of which were computed as described in the "Data Reduction" section) is generally higher than the total afterbody drag C_D measured by the force balance. Differences between the measured and computed drag coefficients are much larger at the lower Mach numbers (as much as 125 percent of the measured drag coefficient). As with any attempt at pressure integration, the number of pressure orifices is finite, and care must be taken in assigning an area to each pressure in regions of rapid pressure changes. Since there is greater uncertainty in computing drag coefficient using pressure integration, the parameter C_D (the drag coefficient measured by the force balance) will be used to compare configurations in subsequent discussions.

Effect of Corner Radius

Figures 9 12 present the effect of afterbody and nozzle corner radius for each boattail closure distribution with the solid plume simulator installed. Part (a) of these figures shows the measured (by the balance) drag coefficient as a function of Mach number, and parts (b) to (d) (parts (b) and (c) of fig. 12) show the boattail static pressure distributions. Note that the longitudinal rows of pressure orifices are at different spanwise locations for the different nozzle corner radii, as was shown in figure 5. Because of data availability, a complete comparison of the three corner radii can be made only for the nozzles with closure distribution of $\beta_{t,\text{top/bot}} = \beta_{t,\text{side}}$ (fig. 11) at subsonic Mach numbers. The effect of corner radius on drag was generally less than 0.015 in C_D between any nozzles of a given closure distribution. However, an important point to recall is that C_D is an afterbody drag coefficient that is nondimensionalized by maximum fuselage cross-sectional area instead of an aircraft drag coefficient that is nondimensionalized by wing area. Therefore, afterbody drag coefficients are approximately an order of magnitude larger than aircraft drag coefficients.

In general, for the range of Mach numbers tested, the sharp-corner nozzles have the highest drag and the 2-in. corner-radius nozzles have the lowest drag. A notable exception is the nozzles with $\beta_{t,\mathrm{side}}=0^\circ$ (fig. 9) at supersonic speeds where the 1-in. corner-radius nozzle (nozzle 5) had the lowest drag. (Sharp-corner-radius data are not available for this closure distribution.) The reason for this exception is not known. The observed effect of corner radius on

drag is expected since any differences between the top flap pressures and sidewall boattail pressures can be equalized more easily by flow traveling from high-pressure to low-pressure regions around a large corner radius.

The pressure distributions for the nonzero boattail angle nozzles generally support this expectation. For example, on the nozzles with $\beta_{t,\text{top/bot}}$ = $17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ} \text{ at } M_{\infty} = 0.60 \text{ (fig. 10(b)), the}$ pressures in the initial expansion region exhibit a smooth transition from the top flap to the sidewall on the 2-in. corner-radius nozzle, but they exhibit a sharp jump between the top flap and sidewall on the sharp-corner nozzle. Downstream in the pressure recovery region, the pressure levels are similar for all the orifice rows on each nozzle despite the apparent lack of pressure equalization around the corner of the nozzle in the initial expansion region. At $M_{\infty} = 0.90$ and 1.20 (for example, figs. 10(c) and 10(d), respectively), the pressure distributions indicate a highly complex flow field with shocks and separation regions that form at different streamwise locations on the different nozzle surfaces.

In contrast, the pressure distributions at M_{∞} = 0.60 on the nozzles with $\beta_{t,\mathrm{side}} = 0^{\circ}$ (fig. 9(b)) behave differently. The far outboard row of orifices on the top flap (which are in the corner region of the nozzle for x/l < 0.3) and the row of orifices along the top/side corner have pressures in the initial expansion region that transition between those on the top flap and the sidewall, as would be expected. However, this trend is not continued through the pressure recovery region farther downstream. Pressures for the top/side corner row do not recover to the level of either the top flap or the sidewall pressures, although those on the 2-in. corner-radius nozzle recover better than those on the 1-in. corner-radius nozzle. Since the change in boattail angle from 17.9° on the top/bottom nozzle flaps to 0° on the sidewalls is the most severe in this investigation, a vortex could form on the nozzle corner. The severity of this vortex would be mitigated by the larger corner radii, which is consistent with the observed pressure trends.

Figure 13 presents the effect of angle of attack on the measured (by the balance) afterbody drag coefficient for the various corner radii with the solid plume removed. Drag coefficients for plume-on configurations (tested only at $\alpha=0^{\circ}$) are presented for reference as solid symbols. Generally, the nozzle with the lowest drag at $\alpha=0^{\circ}$ had the lowest drag across the angle-of-attack range tested. As with the plume-on configurations, the 2-in. corner-radius nozzles generally had the lowest drag.

Effect of Closure Distribution

Figures 14 to 16 present the effect of closure distribution for each nozzle corner radius with the solid plume simulator installed. Part (a) of these figures shows the measured drag coefficient as a function of Mach number, and parts (b) to (d) (parts (b) and (c) of fig. 14) show the static pressure distributions. As before, complete comparisons are not always possible. For certain corner radii at some Mach numbers, closure distribution has little or no effect on measured drag such as the sharpcorner nozzles at $M_{\infty} \leq 0.70$ (fig. 14(a)) or the 1-in. corner-radius nozzles at $M_{\infty} \ge 1.20$ (fig. 15(a)). The drag of the sharp-corner nozzles seems to be the least sensitive to closure distribution, but only data from the two nozzles with the least extreme closure distributions ($\beta_{t,\mathrm{top/bot}} = 17.3^{\circ}/\beta_{t,\mathrm{side}} = 9.7^{\circ}$ and $\beta_{t,\text{top/bot}} = \beta_{t,\text{side}} = 16.4^{\circ}$) are available. When closure distribution does have an appreciable effect on drag, the nozzles with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} =$ 9.7° generally have the lowest drag and the nozzles with $\beta_{t,\text{top/bot}} = 15.0^{\circ}/\beta_{t,\text{side}} = 22.4^{\circ}$ generally have the highest drag.

A notable exception occurs for $0.90 \leq M_{\infty} \leq$ 0.95 with the 1- and 2-in. corner-radius nozzles (figs. 15(a) and 16(a), respectively) where the nozzle with $\beta_{t,\text{side}} = 0^{\circ}$ has the lowest drag. Note, however, that data for the closure distribution of $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ are not available for the 1-in. corner-radius nozzle. An examination of the pressure distributions for these nozzles at $M_{\infty}=0.90$ (figs. 15(c) and 16(c)) shows little effect of closure distribution for the pressures on the top or bottom nozzle flaps except in the strength of the initial expansion. However, this is not the case on the nozzle sidewalls. As was discussed previously, the flow over the nozzle sidewalls on the nozzles with $\beta_{t.\text{side}} = 0^{\circ}$ exhibits neither the strong initial expansion nor the strong downstream pressure recovery seen for the nonzero boattail angle surfaces. At the lower subsonic Mach numbers, the strong downstream recovery on the nonzero boattail angle surfaces is sufficient to produce positive pressures that apparently offset the drag produced by the low pressures in the initial expansion region. At the higher subsonic Mach numbers, the pressure recovery on the nonzero boattail angle surfaces is not strong enough to produce positive pressures, and thus all the nonzero boattail angle surfaces contribute to drag. The sidewalls of the nozzles with $\beta_{t,\mathrm{side}} = 0^{\circ}$ have no aft-facing area for the pressures to act on, and thus they do not contribute to the pressure drag on the nozzle. Therefore, the nozzles with $eta_{t,\mathrm{side}} = reve{0}^\circ$ tend to have the lowest

drag in the range of Mach numbers where the pressure recovery on the surfaces of the other nozzles is not sufficient to produce positive pressures. Further trade studies are necessary to determine which range of Mach numbers is most mission critical in order to choose the most beneficial closure distribution.

A further examination of the pressure distributions does not disclose why the nozzles with a closure distribution of $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ generally have the lowest drag. For example, the two sharp-corner nozzles (figs. 14(b) and 14(c)) have nearly identical pressure distributions on the top and bottom nozzle flaps. This result is expected since the boattail angle differs only by 0.9°. On the nozzle sidewall at $M_{\infty} = 0.60$ (fig. 14(b)), the notably stronger pressure recovery for nozzle 3 indicates that the drag should be lower, especially since the larger sidewall boattail angle ($\beta_{t, \text{side}} = 16.4^{\circ} \text{ versus } \beta_{t, \text{side}} = 9.7^{\circ}$) yields more aft-facing area on which these positive pressures can act. However, no real difference occurs between the drag coefficients of these two nozzles at this Mach number. (See fig. 14(a).) On the other hand, at $M_{\infty}=0.90$ where there is a difference in drag, the differences in the sidewall boattail pressures between the two closure distributions are not as pronounced (fig. 14(c)) as they are at $M_{\infty} = 0.60$. The sidewall boattail pressures for nozzle 2 are somewhat higher than those of nozzle 3. This can result in lower drag for nozzle 2 if the aft-facing areas that these pressures act on are the same; but in fact nozzle 2 has less aft-facing area for these pressures to act on than nozzle 3, thus further reducing the significance of this pressure difference. Yet, examination of figure 14(a) clearly shows that C_D for nozzle 2 is lower at $M_{\infty} = 0.90$.

Figure 17 presents the effect of angle of attack on the measured afterbody drag for the various closure distributions with the solid plume simulator removed at Mach numbers of 0.60, 0.90, and 1.20. plume-on drag coefficients at $\alpha = 0^{\circ}$ are presented as solid symbols for reference purposes. For the 2-in. corner-radius nozzles (fig. 17(b)), the nozzle with the lowest drag at $\alpha = 0^{\circ}$ generally has the lowest drag across the angle-of-attack range tested, as was observed previously. In the high-subsonic Mach number range ($M_{\infty} = 0.90$), the nozzles with $\beta_{t,\mathrm{side}} = 0^{\circ}$ again have the lowest drag. However, in contrast to the plume-on configurations where the nozzles with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ generally have the lowest drag at $M_{\infty}=0.60$ and 1.20, the nozzles with $\beta_{t,\text{top/bot}} = \beta_{t,\text{side}} = 16.4^{\circ}$ generally have the lowest drag for the plume-off configurations. The cause is not clear, even with a further examination of the pressure distributions.

Concluding Remarks

A parametric study has been conducted in the Langley 16-Foot Transonic Tunnel on an isolated nonaxisymmetric fuselage model that simulates a twin-engine fighter. The effects of aft-end closure distribution (top/bottom nozzle-flap boattail angle versus nozzle-sidewall boattail angle) and afterbody and nozzle corner treatment (sharp or radius) were investigated. Four different closure distributions with three different corner radii were tested. Tests were conducted over a range of Mach numbers from 0.40 to 1.25 and over a range of angles of attack from -3° to 9°. Solid plume simulators were used to simulate the jet exhaust.

For a given closure distribution in the range of Mach numbers tested, the sharp-corner nozzles generally have the highest drag and the 2-in. corner-radius nozzles generally have the lowest drag.

The effect of closure distribution on afterbody drag is highly dependent on configuration, plume simulation, and Mach number. Except at high subsonic Mach numbers, the nozzles with the top and bottom terminal boattail angle $(\beta_{t,top/bot})$ of 17.3° and sidewall terminal boattail angle ($\beta_{t,\text{side}}$) of 9.7° generally have the lowest drag for the plume-on configurations, whereas the nozzles with $\beta_{t,\text{top/bot}} =$ $eta_{t,\mathrm{side}}=16.4^\circ$ generally have the lowest drag for the plume-off configurations. The nozzles with $\beta_{t,\text{top/bot}} = 15.0^{\circ}/\beta_{t,\text{side}} = 22.4^{\circ}$ generally have the highest drag. However, the nozzles with $\beta_{t,\text{side}} = 0^{\circ}$ have the lowest drag in the range of Mach numbers (approximately between 0.90 and 0.95) where the pressure recovery on the surfaces of the other nozzles is not sufficient to produce drag-reducing positive pressures. Further trade studies are necessary to determine which range of Mach numbers is most mission critical in order to choose the most beneficial closure distribution.

All nozzles had lower drag with the solid plume simulators installed (approximating a fully expanded jet exhaust) than with them removed (approximating a nonoperating jet). This result has been noted previously for nozzles with a flowing jet.

NASA Langley Research Center Hampton, VA 23681-0001 June 24, 1992

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Table 1. Nozzle Cross-Section Coordinates for One Quadrant
[All dimensions are given in inches]

(a) Nozzle 5

х	y_R	z_R	R
0.9999	4.0120	1.4996	0.9934
1.0999	4.0034	1.4918	1.0049
1.1999	4.0202	1.5077	0.9827
1.2999	4.0227	1.5094	0.9798
1.3999	4.0182	1.5058	0.9857
1.4999	4.0173	1.5048	0.9869
1.5999	4.0166	1.5041	0.9879
1.6999	4.0075	1.4949	1.0006
1.7999	4.0078	1.4949	1.0004
1.8999	4.0168	1.5045	0.9876
1.9999	4.0126	1.4990	0.9941
2.0999	4.0146	1.5014	0.9910
2.1999	4.0104	1.4969	0.9970
2.2999	4.0200	1.5065	0.9834
2.3999	4.0213	1.5093	0.9797
2.4999	4.0348	1.5282	0.9553
2.5967	4.0241	1.5217	0.9640
2.6000	4.0095	1.5111	0.9810
2.7000	4.0057	1.5097	0.9758
2.8000	3.9732	1.4683	1.0147
2.9000	3.9619	1.4344	1.0313
3.0000	3.9775	1.4215	1.0136
3.1000	3.9865	1.3988	1.0068
3.2000	3.9950	1.3747	1.0014
3.3000	4.0160	1.3650	0.9774
3.4000	4.0326	1.3507	0.9592
3.5000	4.0381	1.3234	0.9581
3.6000	4.0698	1.3228	0.9196
3.7000	4.0851	1.3063	0.9041
3.8000	4.0890	1.2766	0.9055
3.9000	4.0887	1.2427	0.9129
4.0000	4.1360	1.2599	0.8513
4.1000	4.1397	1.2306	0.8524
4.2000	4.1844	1.2475	0.7925
4.3000	4.1946	1.2249	0.7849
4.4000	4.2144	1.2161	0.7604
4.5000	4.2324	1.2013	0.7418
4.5999	4.2038	1.1303	0.7950
4.6999	4.2298	1.1265	• 0.7635

х	y_R	z_R	R
4.7999	4.2401	1.1043	0.7551
4.8999	4.2638	1.0962	0.7282
4.9999	4.2750	1.0744	0.7189
5.0999	4.2859	1.0533	0.7096
5.1999	4.3125	1.0475	0.6787
5.2999	4.3272	1.0303	0.6642
5.3999	4.3361	1.0065	0.65~გ
5.4999	4.3537	0.9917	0.6394
5.5999	4.3674	0.9721	0.6268
5.6999	4.3903	0.9620	0.6013
5.7999	4.4034	0.9426	0.5893
5.8999	4.4147	0.9216	0.5796
5.9999	4.4295	0.9037	0.5650
6.0999	4.4450	0.8865	0.5498
6.1999	4.4635	0.8724	0.5301
6.2999	4.4760	0.8528	0.5184
6.3999	4.4925	0.8363	0.5017
6.4999	4.5048	0.8166	0.4904
6.5999	4.5145	0.7927	0.4834
6.6999	4.5329	0.7799	0.4631
6.7070	4.5333	0.7747	0.4650
6.8000	4.5379	0.7506	0.4630
6.9000	4.5635	0.7451	0.4334
7.0000	4.5897	0.7394	0.4025
7.1000	4.6002	0.7169	0.3943
7.2000	4.6154	0.6995	0.3791
7.3000	4.6191	0.6706	0.3798
7.4000	4.6438	0.6628	0.3515
7.5000	4.6559	0.6431	0.3403
7.6000	4.6695	0.6228	0.3281
7.7000	4.6878	0.6097	0.3078
7.8000	4.7014	0.5903	0.2949
7.9000	4.7167	0.5734	0.2795
8.0000	4.7364	0.5604	0.2581
8.1000	4.7456	0.5373	0.2514
8.2000	4.7685	0.5283	0.2248
8.3000	4.7641	0.4920	0.2366
8.4000	4.7892	0.4842	0.2077
8.4898	4.8062	0.4698	0.1911

Table 1. Continued

(b) Nozzle 6

x y _R z _R R 1.0001 4.0060 1.4894 0.9955 1.1001 4.0085 1.4909 0.9936 1.2001 4.0049 1.4863 0.9978 1.3001 4.0097 1.4903 0.9916 1.4001 4.0079 1.4888 0.9936 1.5001 4.0094 1.4875 0.9930 1.5001 4.0091 1.4875 0.9930 1.7001 4.0090 1.4871 0.9932 1.8001 4.0068 1.4846 0.9958 1.9001 4.0058 1.4830 0.9974 2.0001 4.0046 1.4810 0.9989 2.1001 4.0035 1.4792 1.0003 2.2001 4.0026 1.4776 1.0013 2.3001 3.9978 1.4722 1.0074 2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0048 1.4758 0.9940 <th></th> <th></th> <th></th> <th>· ·</th>				· ·
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1.4001 4.0079 1.4888 0.9936 1.5001 4.0094 1.4897 0.9917 1.6001 4.0091 1.4875 0.9930 1.7001 4.0090 1.4871 0.9932 1.8001 4.0068 1.4846 0.9958 1.9001 4.0058 1.4830 0.9974 2.0001 4.0046 1.4810 0.9989 2.1001 4.0035 1.4792 1.0003 2.2001 4.0026 1.4776 1.0013 2.3001 3.9978 1.4722 1.0074 2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7764 4.0117 1.4848 0.9772 2.8000 4.0189 1.4941 0.9453 3.0000 4.0189 1.4941 0.9453 3.2000 4.0189 1.4941 0.9453 3.2000 4.0013 1.4473	1.2001	4.0049	1.4863	0.9978
1.5001 4.0094 1.4897 0.9917 1.6001 4.0091 1.4875 0.9930 1.7001 4.0090 1.4871 0.9932 1.8001 4.0068 1.4846 0.9958 1.9001 4.0058 1.4830 0.9974 2.0001 4.0046 1.4810 0.9989 2.1001 4.0035 1.4792 1.0003 2.2001 4.0026 1.4776 1.0013 2.3001 3.9978 1.4722 1.0074 2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.0085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655	1.3001	4.0097	1.4903	0.9916
1.6001 4.0091 1.4875 0.9930 1.7001 4.0090 1.4871 0.9932 1.8001 4.0068 1.4846 0.9958 1.9001 4.0058 1.4830 0.9974 2.0001 4.0046 1.4810 0.9989 2.1001 4.0035 1.4792 1.0003 2.2001 4.0026 1.4776 1.0013 2.3001 3.9978 1.4722 1.0074 2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.0189 1.4941 0.9453 3.0000 4.0189 1.4941 0.9453 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308		4.0079	1.4888	0.9936
1.7001 4.0090 1.4871 0.9932 1.8001 4.0068 1.4846 0.9958 1.9001 4.0058 1.4830 0.9974 2.0001 4.0046 1.4810 0.9989 2.1001 4.0035 1.4792 1.0003 2.2001 4.0026 1.4776 1.0013 2.3001 3.9978 1.4722 1.0074 2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 <	1.5001	4.0094	1.4897	0.9917
1.8001 4.0068 1.4846 0.9958 1.9001 4.0058 1.4830 0.9974 2.0001 4.0046 1.4810 0.9989 2.1001 4.0035 1.4792 1.0003 2.2001 4.0026 1.4776 1.0013 2.3001 3.9978 1.4722 1.0074 2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.0085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9883 1.3772	1.6001	4.0091	1.4875	0.9930
1.9001 4.0058 1.4830 0.9974 2.0001 4.0046 1.4810 0.9989 2.1001 4.0035 1.4792 1.0003 2.2001 4.0026 1.4776 1.0013 2.3001 3.9978 1.4722 1.0074 2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.0885 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.99883 1.3172 0.8523 3.7000 3.9883 1.3772	1.7001	4.0090	1.4871	0.9932
2.0001 4.0046 1.4810 0.9989 2.1001 4.0035 1.4792 1.0003 2.2001 4.0026 1.4776 1.0013 2.3001 3.9978 1.4722 1.0074 2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.0085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.99883 1.3172 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420	1.8001	4.0068	1.4846	0.9958
2.1001 4.0035 1.4792 1.0003 2.2001 4.0026 1.4776 1.0013 2.3001 3.9978 1.4722 1.0074 2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 4.0000 3.9735 1.3038 <		4.0058	1.4830	0.9974
2.2001 4.0026 1.4776 1.0013 2.3001 3.9978 1.4722 1.0074 2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7001 4.048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9845 1.3589 0.8391 3.8000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 <t< td=""><td>2.0001</td><td>4.0046</td><td>1.4810</td><td>0.9989</td></t<>	2.0001	4.0046	1.4810	0.9989
2.3001 3.9978 1.4722 1.0074 2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9760 1.3215 0.8131 4.0000 3.9699 1.2860 <	2.1001	4.0035	1.4792	1.0003
2.4001 3.9979 1.4713 1.0072 2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.0085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9760 1.3215 0.8131 4.0000 3.9699 1.2860 0.7845 4.2000 3.9633 1.2504	2.2001	4.0026	1.4776	1.0013
2.5001 3.9963 1.4697 1.0084 2.6001 4.0000 1.4721 1.0032 2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.0085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9699 1.2860 0.7845 4.2000 3.9633 1.2504	2.3001	3.9978	1.4722	1.0074
2.6001 4.0000 1.4721 1.0032 2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.0085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9699 1.2860 0.7845 4.2000 3.9633 1.2504 0.7560 4.3000 3.9633 1.2504		3.9979	1.4713	1.0072
2.7001 4.0048 1.4758 0.9940 2.7764 4.0117 1.4848 0.9772 2.8000 4.0085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9633 1.2504 0.7560 4.4000 3.9633 1.2504 0.7560 4.5000 3.9586 1.2151	2.5001	3.9963	1.4697	1.0084
2.7764 4.0117 1.4848 0.9772 2.8000 4.0085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9699 1.2860 0.7845 4.2000 3.9633 1.2504 0.7560 4.3000 3.9633 1.2504 0.7560 4.4000 3.9666 1.2151 0.7280 4.6000 3.9484 1.1773	2.6001	4.0000	1.4721	1.0032
2.8000 4.0085 1.4819 0.9780 2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9666 1.2151 0.7280 4.6000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600		4.0048	1.4758	0.9940
2.9000 4.0189 1.4941 0.9453 3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9666 1.2151 0.7280 4.6000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600		4.0117	1.4848	0.9772
3.0000 4.0153 1.4839 0.9297 3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600	2.8000	4.0085	1.4819	0.9780
3.1000 4.0064 1.4655 0.9215 3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877	2.9000	4.0189	1.4941	0.9453
3.2000 4.0013 1.4473 0.9090 3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9532 1.1965 0.7149 4.7000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877		4.0153	1.4839	0.9297
3.3000 3.9987 1.4308 0.8942 3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877	3.1000	4.0064	1.4655	0.9215
3.4000 3.9958 1.4132 0.8796 3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877	3.2000	4.0013	1.4473	0.9090
3.5000 3.9914 1.3947 0.8671 3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877	3.3000	3.9987	1.4308	0.8942
3.6000 3.9883 1.3772 0.8523 3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877	3.4000	3.9958	1.4132	0.8796
3.7000 3.9845 1.3589 0.8391 3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877	3.5000	3.9914	1.3947	0.8671
3.8000 3.9820 1.3420 0.8236 3.9000 3.9760 1.3215 0.8131 4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9532 1.1965 0.7149 4.7000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877	3.6000	3.9883	1.3772	0.8523
3.9000 3.9760 1.3215 0.8131 4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9532 1.1965 0.7149 4.7000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877	3.7000	3.9845	1.3589	0.8391
4.0000 3.9735 1.3038 0.7982 4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9532 1.1965 0.7149 4.7000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877		3.9820		0.8236
4.1000 3.9699 1.2860 0.7845 4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9532 1.1965 0.7149 4.7000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877		3.9760	1.3215	0.8131
4.2000 3.9674 1.2690 0.7692 4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9532 1.1965 0.7149 4.7000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877			1.3038	0.7982
4.3000 3.9633 1.2504 0.7560 4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9532 1.1965 0.7149 4.7000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877			1.2860	0.7845
4.4000 3.9607 1.2334 0.7414 4.5000 3.9566 1.2151 0.7280 4.6000 3.9532 1.1965 0.7149 4.7000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877		3.9674	1.2690	0.7692
4.5000 3.9566 1.2151 0.7280 4.6000 3.9532 1.1965 0.7149 4.7000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877	4.3000	3.9633	1.2504	0.7560
4.5000 3.9566 1.2151 0.7280 4.6000 3.9532 1.1965 0.7149 4.7000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877		3.9607	1.2334	0.7414
4.7000 3.9484 1.1773 0.7029 4.8000 3.9458 1.1600 0.6877				
4.8000 3.9458 1.1600 0.6877			1.1965	0.7149
4.8000 3.9458 1.1600 0.6877	4.7000	3.9484	1.1773	
4.9000 3.9391 1.1364 0.6803		3.9458	1.1600	
	4.9000	3.9391	1.1364	
5.0000 3.9384 1.1234 0.6604		3.9384	1.1234	0.6604
5.1000 3.9334 1.1030 0.6496		3.9334	1.1030	0.6496
5.2000 3.9278 1.0826 0.6387	5.2000	3.9278	1.0826	0.6387

x y _R z _R R 5.3003 3.9062 1.0486 0.6493 5.4003 3.9182 1.0408 0.6179 5.5003 3.9144 1.0216 0.6048 5.6003 3.9089 0.9873 0.5750 5.8003 3.9064 0.9696 0.5600 5.9003 3.9028 0.9511 0.5469 6.0003 3.8978 0.9313 0.5348 6.1003 3.8948 0.9138 0.5206 6.2003 3.8917 0.8958 0.5061 6.3003 3.8846 0.8594 0.4789 6.5003 3.8846 0.8594 0.4789 6.5003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8559 0.7310 0.3843 <th></th> <th></th> <th></th> <th></th>				
5.3003 3.9062 1.0486 0.6493 5.4003 3.9182 1.0408 0.6179 5.5003 3.9144 1.0216 0.6048 5.6003 3.9122 1.0053 0.5890 5.7003 3.9089 0.9873 0.5750 5.8003 3.9064 0.9696 0.5600 5.9003 3.9028 0.9511 0.5469 6.0003 3.8948 0.9313 0.5348 6.1003 3.8948 0.9138 0.5206 6.2003 3.8917 0.8958 0.5061 6.3003 3.8846 0.8594 0.4789 6.5003 3.8807 0.8410 0.4659 6.6003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8550 0.7497	X	y_R	z_R	R
5.5003 3.9144 1.0216 0.6048 5.6003 3.9122 1.0053 0.5890 5.7003 3.9089 0.9873 0.5750 5.8003 3.9064 0.9696 0.5600 5.9003 3.9028 0.9511 0.5469 6.0003 3.8978 0.9313 0.5348 6.1003 3.8948 0.9138 0.5206 6.2003 3.8917 0.8958 0.5061 6.3003 3.8876 0.8774 0.4932 6.4003 3.8846 0.8594 0.4789 6.5003 3.8758 0.8208 0.4544 6.7003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8552 0.7118 0.3714 7.3003 3.8540 0.6942	5.3003	3.9062		0.6493
5.6003 3.9122 1.0053 0.5890 5.7003 3.9089 0.9873 0.5750 5.8003 3.9064 0.9696 0.5600 5.9003 3.9028 0.9511 0.5469 6.0003 3.8978 0.9313 0.5348 6.1003 3.8948 0.9138 0.5206 6.2003 3.8917 0.8958 0.5061 6.3003 3.8876 0.8774 0.4932 6.4003 3.8846 0.8594 0.4789 6.5003 3.8807 0.8410 0.4659 6.6003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8552 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764	5.4003	3.9182	1.0408	0.6179
5.7003 3.9089 0.9873 0.5750 5.8003 3.9064 0.9696 0.5600 5.9003 3.9028 0.9511 0.5469 6.0003 3.8978 0.9313 0.5348 6.1003 3.8948 0.9138 0.5206 6.2003 3.8917 0.8958 0.5061 6.3003 3.8846 0.8594 0.4789 6.5003 3.8807 0.8410 0.4659 6.6003 3.8758 0.8208 0.4544 6.7003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8383 0.6197	5.5003	3.9144	1.0216	0.6048
5.8003 3.9064 0.9696 0.5600 5.9003 3.9028 0.9511 0.5469 6.0003 3.8978 0.9313 0.5348 6.1003 3.8948 0.9138 0.5206 6.2003 3.8917 0.8958 0.5061 6.3003 3.8876 0.8774 0.4932 6.4003 3.8846 0.8594 0.4789 6.5003 3.8807 0.8410 0.4659 6.6003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8665 0.7674 0.4120 7.0003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8447 0.6561 0.3313 7.6003 3.8447 0.6561 0.3313 7.8003 3.8346 0.6017	5.6003	3.9122	1.0053	0.5890
5.9003 3.9028 0.9511 0.5469 6.0003 3.8978 0.9313 0.5348 6.1003 3.8948 0.9138 0.5206 6.2003 3.8917 0.8958 0.5061 6.3003 3.8876 0.8774 0.4932 6.4003 3.8846 0.8594 0.4789 6.5003 3.8807 0.8410 0.4659 6.6003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8552 0.7118 0.3714 7.3003 3.8553 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017	5.7003	3.9089	0.9873	0.5750
6.0003 3.8978 0.9313 0.5348 6.1003 3.8948 0.9138 0.5206 6.2003 3.8917 0.8958 0.5061 6.3003 3.8876 0.8774 0.4932 6.4003 3.8846 0.8594 0.4789 6.5003 3.8807 0.8410 0.4659 6.6003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8552 0.7118 0.3714 7.3003 3.8552 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8447 0.6561 0.3313 7.6003 3.8441 0.6379 0.3177 7.7003 3.8383 0.6197 0.2898 7.9003 3.8305 0.5829	5.8003	3.9064	0.9696	0.5600
6.1003 3.8948 0.9138 0.5206 6.2003 3.8917 0.8958 0.5061 6.3003 3.8876 0.8774 0.4932 6.4003 3.8846 0.8594 0.4789 6.5003 3.8807 0.8410 0.4659 6.6003 3.8758 0.8208 0.4544 6.7003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8383 0.6197 0.3032 7.8003 3.83846 0.6017 0.2898 7.9003 3.83846 0.6017 0.2898 7.9003 3.8395 0.5829 0.2767 8.0003 3.8277 0.5646	5.9003	3.9028	0.9511	0.5469
6.2003 3.8917 0.8958 0.5061 6.3003 3.8876 0.8774 0.4932 6.4003 3.8846 0.8594 0.4789 6.5003 3.8807 0.8410 0.4659 6.6003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8346 0.6017 0.2898 7.9003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8395 0.5829 0.2767 8.0003 3.8277 0.5646	6.0003	3.8978	0.9313	0.5348
6.3003 3.8876 0.8774 0.4932 6.4003 3.8846 0.8594 0.4789 6.5003 3.8807 0.8410 0.4659 6.6003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461	6.1003	3.8948	0.9138	0.5206
6.4003 3.8846 0.8594 0.4789 6.5003 3.8807 0.8410 0.4659 6.6003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8637 0.7497 0.3973 7.1003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8329 0.5461 0.2496 8.2003 3.8229 0.5461 0.2496 8.2003 3.8167 0.5096	6.2003	3.8917	0.8958	0.5061
6.5003 3.8807 0.8410 0.4659 6.6003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8559 0.7310 0.3843 7.2003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8447 0.6561 0.3313 7.8003 3.8383 0.6197 0.3032 7.8003 3.83846 0.6017 0.2898 7.9003 3.8393 0.5829 0.2767 8.0003 3.8237 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8167 0.5096	6.3003	3.8876	0.8774	0.4932
6.6003 3.8758 0.8208 0.4544 6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8637 0.7497 0.3973 7.1003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919	6.4003	3.8846	0.8594	0.4789
6.7003 3.8727 0.8038 0.4398 6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8637 0.7497 0.3973 7.1003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734	6.5003	3.8807	0.8410	0.4659
6.8003 3.8708 0.7860 0.4247 6.9003 3.8665 0.7674 0.4120 7.0003 3.8637 0.7497 0.3973 7.1003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8082 0.4562	6.6003	3.8758	0.8208	0.4544
6.9003 3.8665 0.7674 0.4120 7.0003 3.8637 0.7497 0.3973 7.1003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8082 0.4562	6.7003	3.8727	0.8038	0.4398
7.0003 3.8637 0.7497 0.3973 7.1003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409	6.8003	3.8708	0.7860	0.4247
7.1003 3.8559 0.7310 0.3843 7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097	6.9003	3.8665	0.7674	0.4120
7.2003 3.8562 0.7118 0.3714 7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7968 0.3760	7.0003	3.8637	0.7497	0.3973
7.3003 3.8534 0.6942 0.3566 7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7941 0.3594	7.1003	3.8559	0.7310	0.3843
7.4003 3.8503 0.6764 0.3424 7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594	7.2003	3.8562	0.7118	0.3714
7.5003 3.8447 0.6561 0.3313 7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594	7.3003	3.8534	0.6942	0.3566
7.6003 3.8411 0.6379 0.3177 7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368	7.4003	3.8503	0.6764	0.3424
7.7003 3.8383 0.6197 0.3032 7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758	7.5003	3.8447	0.6561	0.3313
7.8003 3.8346 0.6017 0.2898 7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758	7.6003	3.8411	0.6379	0.3177
7.9003 3.8305 0.5829 0.2767 8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758	7.7003	3.8383	0.6197	0.3032
8.0003 3.8277 0.5646 0.2625 8.1003 3.8239 0.5461 0.2496 8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758	7.8003	3.8346	0.6017	0.2898
8.1003 3.8239 0.5461 0.2496 8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758	7.9003	3.8305	0.5829	0.2767
8.2003 3.8204 0.5280 0.2358 8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758	8.0003	3.8277	0.5646	0.2625
8.3003 3.8167 0.5096 0.2226 8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758	8.1003	3.8239	0.5461	0.2496
8.3679 3.8159 0.4996 0.2109 8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758	8.2003	3.8204	0.5280	0.2358
8.4001 3.8134 0.4919 0.2186 8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758	8.3003		0.5096	0.2226
8.5001 3.8112 0.4734 0.1940 8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758	8.3679		0.4996	0.2109
8.6001 3.8082 0.4562 0.1795 8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758			0.4919	0.2186
8.7001 3.8059 0.4409 0.1625 8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758			0.4734	0.1940
8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758			0.4562	0.1795
8.8001 3.8043 0.4259 0.1456 8.9001 3.8018 0.4097 0.1293 9.0001 3.7993 0.3932 0.1142 9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758	8.7001		0.4409	0.1625
9.0001 3.7993 0.3932 0.1142 9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758		3.8043	0.4259	
9.1001 3.7968 0.3760 0.0093 9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758		3.8018		0.1293
9.2001 3.7841 0.3594 0.0845 9.3001 3.7849 0.3368 0.0758			0.3932	0.1142
9.3001 3.7849 0.3368 0.0758		3.7968	0.3760	0.0093
0.0730		3.7841		0.0845
0.2055			0.3368	0.0758
9.3955 3.7814 0.3194 0.0721	9.3955	3.7814	0.3194	0.0721

Table 1. Continued

(c) Nozzle 7

х	y_R	^z R	R
1.0004	4.0138	1.5030	0.9858
1.1004	4.0135	1.5034	0.9861
1.2004	4.0143	1.5036	0.9858
1.3004	4.0146	1.5045	0.9852
1,4004	4.0139	1.5021	0.9874
1.5004	4.0157	1.5039	0.9851
1.6004	4.0153	1.5029	0.9861
1.7004	4.0154	1.5031	0.9859
1.8004	4.0147	1.5033	0.9861
1.9004	4.0147	1.5028	0.9865
2.0004	4.0159	1.5042	0.9846
2.1004	4.0150	1.5031	0.9859
2.2004	4.0133	1.5020	0.9878
2.3004	4.0139	1.5033	0.9862
2.4004	4.0140	1.5024	0.9873
2.5004	4.0141	1.5026	0.9868
2.6004	4.0136	1.5034	0.9860
2.7004	4.0102	1.5028	0.9850
2.7500	4.0120	1.5061	0.9782
2.8001	4.0086	1.5038	0.9742
2.9001	4.0046	1.4998	0.9576
3.0001	3.9999	1.4938	0.9338
3.1001	3.9888	1.4827	0.9152
3.2001	3.9732	1.4688	0.9002
3.3001	3.9598	1.4541	0.8847
3.4001	3.9446	1.4403	0.8691
3.5001	3.9305	1.4266	0.8533
3.6001	3.9134	1.4098	0.8410
3.7001	3.8954	1.3921	0.8298
3.8001	3.8792	1.3765	0.8168
3.9001	3.8619	1.3588	0.8052
4.0001	3.8470	1.3441	0.7907
4.1001	3.8292	1.3259	0.7802
4.2001	3.8131	1.3104	0.7664
4.3001	3.7958	1.2931	0.7551
4.4001	3.7783	1.2753	0.7437
4.5001	3.7623	1.2605	0.7292
4.6001	3.7446	1.2424	0.7188
4.7001	3.7284	1.2263	0.7063
4.8001	3.7080	1.2064	0.6983
4.9001	3.6985	1.1959	0.6770

5.0001 3.6728 1.1716 0.6760 5.1001 3.6602 1.1581 0.6588 5.2001 3.6016 1.1005 0.7032 5.3001 3.6397 1.1397 0.6141 5.4001 3.6294 1.1290 0.5933 5.4501 3.6122 1.1084 0.6022 5.6501 3.5824 1.0791 0.5720 5.7501 3.5651 1.0622 0.5€3 5.8501 3.5483 1.0453 0.5477 5.9501 3.5359 1.0331 0.5297 6.0501 3.5179 1.0155 0.5184 6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4352 0.9352 0.4540 6.5501 3.4136 0.9139 0.4479 6.7501 3.3738 0.8971 0.4355 6.8501 3.3732 0.8688				
5.1001 3.6602 1.1581 0.6588 5.2001 3.6016 1.1005 0.7032 5.3001 3.6397 1.1397 0.6141 5.4001 3.6294 1.1290 0.5933 5.4501 3.6122 1.1084 0.6022 5.6501 3.5824 1.0791 0.5720 5.7501 3.5651 1.0622 0.5€ J3 5.8501 3.5483 1.0453 0.5477 5.9501 3.5359 1.0331 0.5297 6.0501 3.5179 1.0155 0.5184 6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4352 0.9352 0.4540 6.5501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434	x	y_R	z_R	R
5.1001 3.6602 1.1581 0.6588 5.2001 3.6016 1.1005 0.7032 5.3001 3.6397 1.1397 0.6141 5.4001 3.6294 1.1290 0.5933 5.4501 3.6122 1.1084 0.6022 5.6501 3.5824 1.0791 0.5720 5.7501 3.5651 1.0622 0.5633 5.8501 3.5483 1.0453 0.5477 5.9501 3.5359 1.0331 0.5297 6.0501 3.5179 1.0155 0.5184 6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3742 0.8742 0.3969 7.0501 3.3738 0.8742	5.0001	3.6728		
5.2001 3.6016 1.1005 0.7032 5.3001 3.6397 1.1397 0.6141 5.4001 3.6294 1.1290 0.5933 5.4501 3.6122 1.1084 0.6022 5.6501 3.5824 1.0791 0.5720 5.7501 3.5651 1.0622 0.563 5.8501 3.5483 1.0453 0.5477 5.9501 3.5359 1.0331 0.5297 6.0501 3.5179 1.0155 0.5184 6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4599 0.9530 0.4640 6.4501 3.4539 0.9530 0.4640 6.5501 3.4352 0.9352 0.4540 6.7501 3.3973 0.8971 0.4355 6.8501 3.3732 0.8742 0.3969 7.0501 3.3738 0.8742 0.3969 7.5501 3.3273 0.8265 <		3.6602		
5.3001 3.6397 1.1397 0.6141 5.4001 3.6294 1.1290 0.5933 5.4501 3.6122 1.1084 0.6022 5.6501 3.5824 1.0791 0.5720 5.7501 3.5651 1.0622 0.5633 5.8501 3.5483 1.0453 0.5477 5.9501 3.5359 1.0331 0.5297 6.0501 3.5179 1.0155 0.5184 6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4352 0.9352 0.4540 6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3738 0.8742 0.3969 7.0501 3.3738 0.8742 0.3969 7.501 3.3273 0.8265 <		3.6016		0.7032
5.4501 3.6122 1.1084 0.6022 5.6501 3.5824 1.0791 0.5720 5.7501 3.5651 1.0622 0.56 J3 5.8501 3.5483 1.0453 0.5477 5.9501 3.5359 1.0331 0.5297 6.0501 3.5179 1.0155 0.5184 6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4352 0.9352 0.4540 6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3738 0.8742 0.3969 7.0501 3.3738 0.8742 0.3969 7.0501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930		3.6397	1.1397	
5.6501 3.5824 1.0791 0.5720 5.7501 3.5651 1.0622 0.56 J3 5.8501 3.5483 1.0453 0.5477 5.9501 3.5359 1.0331 0.5297 6.0501 3.5179 1.0155 0.5184 6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4352 0.9352 0.4540 6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3738 0.8742 0.3969 7.0501 3.3738 0.8742 0.3969 7.0501 3.3738 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930	5.4001	3.6294	1.1290	0.5933
5.7501 3.5651 1.0622 0.56 J3 5.8501 3.5483 1.0453 0.5477 5.9501 3.5359 1.0331 0.5297 6.0501 3.5179 1.0155 0.5184 6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4352 0.9352 0.4540 6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641	5.4501	3.6122		
5.8501 3.5483 1.0453 0.5477 5.9501 3.5359 1.0331 0.5297 6.0501 3.5179 1.0155 0.5184 6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4352 0.9352 0.4540 6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.218 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2516 0.7526 <	5.6501	3.5824	1.0791	
5.9501 3.5359 1.0331 0.5297 6.0501 3.5179 1.0155 0.5184 6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363	5.7501	3.5651	1.0622	
6.0501 3.5179 1.0155 0.5184 6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4352 0.9352 0.4540 6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363	5.8501	3.5483		0.5477
6.1501 3.5028 1.0009 0.5037 6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4352 0.9352 0.4540 6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209	5.9501	3.5359		
6.2501 3.4862 0.9842 0.4910 6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4352 0.9352 0.4540 6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209	6.0501	3.5179	1.0155	
6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4352 0.9352 0.4540 6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1546 0.6542	6.1501	3.5028	1.0009	
6.3501 3.4696 0.9682 0.4778 6.4501 3.4539 0.9530 0.4640 6.5501 3.4352 0.9352 0.4540 6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1546 0.6542		3.4862	0.9842	
6.5501 3.4352 0.9352 0.4540 6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389	6.3501	3.4696	0.9682	
6.6501 3.4136 0.9139 0.4479 6.7501 3.3973 0.8971 0.4355 6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220	6.4501	3.4539	0.9530	
6.7501 3.3973 0.8971 0.4355 6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160	6.5501	3.4352	0.9352	0.4540
6.8501 3.3862 0.8868 0.4149 6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	6.6501	3.4136	0.9139	
6.9501 3.3738 0.8742 0.3969 7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	6.7501	3.3973	0.8971	
7.0501 3.3742 0.8749 0.3607 7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	6.8501	3.3862	0.8868	
7.1501 3.3438 0.8434 0.3675 7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	6.9501	3.3738	0.8742	0.3969
7.2501 3.3273 0.8265 0.3551 7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	7.0501	3.3742	0.8749	0.3607
7.3501 3.3118 0.8115 0.3411 7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	7.1501	3.3438		
7.4501 3.2946 0.7930 0.3299 7.5501 3.2793 0.7785 0.3153 7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	7.2501	3.3273	0.8265	
7.4501 3.2793 0.7785 0.3153 7.5501 3.2793 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	7.3501	3.3118	0.8115	
7.6501 3.2647 0.7641 0.2992 7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	7.4501	3.2946	0.7930	
7.7501 3.2516 0.7526 0.2811 7.8501 3.2350 0.7363 0.2679 7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	7.5501	3.2793	0.7785	
7.8501 3.2350 0.7363 0.2679 7.8501 3.2350 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	7.6501	3.2647	0.7641	
7.9501 3.2200 0.7209 0.2536 8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	7.7501	3.2516		
8.0501 3.2085 0.7089 0.2363 8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	7.8501	3.2350	0.7363	
8.1996 3.1720 0.6713 0.2327 8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	7.9501			
8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	8.0501			
8.2996 3.1546 0.6542 0.2210 8.3996 3.1389 0.6389 0.2067 8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688	8.1996			
8.4996 3.1224 0.6220 0.1947 8.5996 3.1154 0.6160 0.1688		3.1546	0.6542	
8.5996 3.1154 0.6160 0.1688	8.3996			
8.5770	8.4996		0.6220	
	8.5996			
0.0770	8.6996	3.0975	0.5978	0.1585
8.7996 3.0816 0.5816 0.1451	8.7996	3.0816	0.5816	
8.8996 3.0604 0.5648 0.1357	8.8996	3.0604		
8.9996 3.0332 0.5392 0.1367	8.9996	3.0332		
9.0193 3.0414 0.5405 0.1226	9.0193	3.0414	0.5405	0.1226

Table 1. Continued

(d) Nozzle 8

1		T	·	
	x	y_R	z_R	R
	0.9991	4.0159	1.5147	0.9825
ı	1.0991	4.0148	1.5131	0.9841
ı	1.1991	4.0147	1.5129	0.9845
ı	1.2991	4.0156	1.5134	0.9833
ı	1.3991	4.0128	1.5112	0.9867
l	1.4991	4.0145	1.5133	0.9838
L	1.5991	4.0126	1.5114	0.9862
L	1.6991	4.0139	1.5142	0.9832
L	1.7991	4.0155	1.5168	0.9801
Ĺ	1.8991	4.0162	1.5181	0.9790
L	1.9991	4.0173	1.5202	0.9767
Ĺ	2.0991	4.0201	1.5240	0.9722
L	2.1991	4.0208	1.5257	0.9703
L	2.2991	4.0243	1.5307	0.9644
L	2.3991	4.0236	1.5312	0.9642
L	2.4991	4.0234	1.5321	0.9630
L	2.5991	4.0253	1.5341	0.9589
L	2.6991	4.0210	1.5289	0.9613
L	2.7503	4.0233	1.5266	0.9574
L	2.8007	4.0165	1.5153	0.9625
L	2.9007	4.0085	1.5008	0.9589
L	3.0007	3.9947	1.4835	0.9511
L	3.1007	3.9727	1.4678	0.9398
L	3.2007	3.9497	1.4556	0.9249
L	3.3007	3.9256	1.4453	0.9074
L	3.4007	3.9008	1.4339	0.8914
L	3.5007	3.8761	1.4237	0.8739
L	3.6007	3.8480	1.4092	0.8619
L	3.7007	3.8208	1.3966	0.8482
L	3.8007	3.7920	1.3823	0.8359
L	3.9007	3.7642	1.3695	0.8226
L	4.0007	3.7361	1.3564	0.8088
L	4.1007	3.7078	1.3431	0.7962
L	4.2007	3.6792	1.3292	0.7835
L	4.3007	3.6517	1.3168	0.7694
L	4.4007	3.6248	1.3046	0.7553
L	4.5007	3.5975	1.2926	0.7407
_	4.6007	3.5691	1.2780	0.7291
L	4.7007	3.5409	1.2649	0.7164
_	4.8007	3.5132	1.2516	0.7029
_	4.9007	3.4862	1.2390	0.6889
	5.0007	3.4577	1.2250	0.6764

х	y_R	z _R	R
5.1007	3.4312	1.2128	0.6617
5.2007	3.4026	1.1984	0.6495
5.3007	3.3757	1.1861	0.6353
5.4007	3.3486	1.1734	0.6207
5.5007	3.3210	1.1601	0.6074
5.6007	3.2941	1.1476	0.5926
5.7007	3.2660	1.1345	0.5792
5.8007	3.2398	1.1225	0.5645
5.9007	3.2119	1.1096	0.5515
6.0007	3.1835	1.0957	0.5387
6.1007	3.1570	1.0844	0.5233
6.2007	3.1292	1.0706	0.5107
6.3007	3.1008	1.0569	0.4980
6.4007	3.0724	1.0434	0.4856
6.5007	3.0456	1.0306	0.4719
6.6007	3.0175	1.0172	0.4586
6.7007	2.9907	1.0047	0.4443
6.8007	2.9629	0.9918	0.4305
6.9007	2.9356	0.9783	0.4172
7.0007	2.9082	0.9652	0.4032
7.1007	2.8808	0.9528	0.3886
7.2007	2.8533	0.9396	0.3755
7.3007	2.8262	0.9278	0.3604
7.4007	2.7984	0.9139	0.3481
7.5007	2.7712	0.9009	0.3349
7.6007	2.7435	0.8882	0.3208
7.7007	2.7169	0.8766	0.3061
7.8007	2.6894	0.8636	0.2921
7.9007	2.6625	0.8515	0.2772
8.0007	2.6355	0.8388	0.2633
8.1007	2.6090	0.8268	0.2481
8.2007	2.5818	0.8143	0.2341
8.3007	2.5548	0.8012	0.2204
8.4007	2.5267	0.7877	0.2069
8.5007	2.5010	0.7753	0.1918
8.6007	2.4721	0.7611	0.1792
8.7007	2.4454	0.7486	0.1646
8.8007	2.4166	0.7341	0.1521
8.9007	2.3882	0.7201	0.1391
9.0007	2.3597	0.7053	0.1270
9.0164	2.3384	0.6834	0.1501

Table 1. Continued

(e) Nozzle 9

x	y_R	^Z R	R
1.0000	3.0064	0.4965	1.9971
1.1000	3.0075	0.4985	1.9952
1.2000	3.0052	0.4960	1.9987
1.3000	3.0007	0.4922	2.0048
1.4000	3.0008	0.4929	2.0039
1.5000	3.0028	0.4945	2.0018
1.6000	3.0046	0.4971	1.9985
1.7000	3.0005	0.4927	2.0048
1.8000	3.0035	0.4961	2.0001
1.9000	3.0039	0.4961	1.9999
2.0000	3.0029	0.4952	2.0010
2.1000	3.0172	0.5094	1.9813
2.2000	3.0193	0.5115	1.9781
2.3000	3.0086	0.4994	1.9933
2.4000	3.0126	0.5037	1.9870
2.5000	3.0043	0.4956	1.9977
2.6000	3.0166	0.5078	1.9797
2.7000	3.0315	0.5268	1.9546
2.8000	3.0276	0.5251	1.9566
2.8645	3.0377	0.5346	1.9409
2.9000	2.9494	0.4537	2.0580
3.0000	3.0491	0.5281	1.9301
3.1000	3.0874	0.5367	1.8884
3.2000	3.1240	0.5406	1.8501
3.3000	3.1762	0.5587	1.7908
3.4000	3.2066	0.5560	1.7611
3.5000	3.2330	0.5475	1.7375
3.6000	3.2603	0.5425	1.7109
3.7000	3.2910	0.5403	1.6797
3.8000	3.3249	0.5406	1.6450
3.9000	3.3565	0.5399	1.6121
4.0000	3.3837	0.5338	1.5860
4.1000	3.4219	0.5388	1.5448
4.2000	3.4452	0.5306	1.5229
4.3000	3.4810	0.5339	1.4846
4.4000	3.5179	0.5381	1.4448
4.5000	3.5516	0.5382	1.4100
4.6000	3.5890	0.5431	1.3695
4.7000	3.6115	0.5324	1.3496

x y _R z _R R 4.8000 3.6591 0.5471 1.2952 4.9000 3.6884 0.5444 1.2654 4.9489 3.6750 0.5121 1.2913 4.9996 3.6189 0.4554 1.3644 5.1003 3.7024 0.4857 1.2692 5.2003 3.7777 0.5331 1.1726 5.3003 3.8184 0.5403 1.1279 5.4003 3.8426 0.5315 1.1057 5.5003 3.8796 0.5366 1.0650 5.6003 3.9139 0.5378 1.0289 5.7003 3.9366 0.5259 1.0098 5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1667 0.4906 0.7834 <th></th> <th></th> <th></th> <th></th>				
4.9000 3.6884 0.5444 1.2654 4.9489 3.6750 0.5121 1.2913 4.9996 3.6189 0.4554 1.3644 5.1003 3.7024 0.4857 1.2692 5.2003 3.7777 0.5331 1.1726 5.3003 3.8184 0.5403 1.1279 5.4003 3.8426 0.5315 1.1057 5.5003 3.8796 0.5366 1.0650 5.6003 3.9139 0.5378 1.0289 5.7003 3.9366 0.5259 1.0098 5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906	x	y_R		R
4.9489 3.6750 0.5121 1.2913 4.9996 3.6189 0.4554 1.3644 5.1003 3.7024 0.4857 1.2692 5.2003 3.7777 0.5331 1.1726 5.3003 3.8184 0.5403 1.1279 5.4003 3.8426 0.5315 1.1057 5.5003 3.8796 0.5366 1.0650 5.6003 3.9139 0.5378 1.0289 5.7003 3.9366 0.5259 1.0098 5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.2178 0.4745	4.8000	3.6591	0.5471	1.2952
4.9996 3.6189 0.4554 1.3644 5.1003 3.7024 0.4857 1.2692 5.2003 3.7777 0.5331 1.1726 5.3003 3.8184 0.5403 1.1279 5.4003 3.8426 0.5315 1.1057 5.5003 3.8796 0.5366 1.0650 5.6003 3.9139 0.5378 1.0289 5.7003 3.9366 0.5259 1.0098 5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689	4.9000	3.6884	0.5444	1.2654
5.1003 3.7024 0.4857 1.2692 5.2003 3.7777 0.5331 1.1726 5.3003 3.8184 0.5403 1.1279 5.4003 3.8426 0.5315 1.1057 5.5003 3.8796 0.5366 1.0650 5.6003 3.9139 0.5378 1.0289 5.7003 3.9366 0.5259 1.0098 5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.237 0.4641 <	4.9489	3.6750	0.5121	1.2913
5.2003 3.7777 0.5331 1.1726 5.3003 3.8184 0.5403 1.1279 5.4003 3.8426 0.5315 1.1057 5.5003 3.8796 0.5366 1.0650 5.6003 3.9139 0.5378 1.0289 5.7003 3.9366 0.5259 1.0098 5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641	4.9996	3.6189	0.4554	1.3644
5.3003 3.8184 0.5403 1.1279 5.4003 3.8426 0.5315 1.1057 5.5003 3.8796 0.5366 1.0650 5.6003 3.9139 0.5378 1.0289 5.7003 3.9366 0.5259 1.0098 5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0904 4.3234 0.4436	5.1003	3.7024	0.4857	
5.4003 3.8426 0.5315 1.1057 5.5003 3.8796 0.5366 1.0650 5.6003 3.9139 0.5378 1.0289 5.7003 3.9366 0.5259 1.0098 5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892	5.2003	3.7777	0.5331	1.1726
5.5003 3.8796 0.5366 1.0650 5.6003 3.9139 0.5378 1.0289 5.7003 3.9366 0.5259 1.0098 5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892	5.3003	3.8184	0.5403	1.1279
5.6003 3.9139 0.5378 1.0289 5.7003 3.9366 0.5259 1.0098 5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332	5.4003	3.8426	***	
5.7003 3.9366 0.5259 1.0098 5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.3996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028	5.5003	3.8796		1.0650
5.8003 3.9678 0.5249 0.9775 5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.5996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028	5.6003	3.9139	0.5378	1.0289
5.9003 3.9957 0.5191 0.9506 6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028	5.7003	3.9366	0.5259	1.0098
6.0003 4.0230 0.5134 0.9244 6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.5028 0.3851	5.8003	3.9678	0.5249	0.9775
6.1003 4.0468 0.5040 0.9030 6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817	5.9003	3.9957		
6.2003 4.0793 0.5039 0.8692 6.3003 4.1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817	6.0003	4.0230	0.5134	0.9244
6.3003 4,1037 0.4950 0.8470 6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817	6.1003	4.0468	0.5040	0.9030
6.4003 4.1355 0.4928 0.8150 6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680	6.2003	4.0793	0.5039	0.8692
6.5003 4.1667 0.4906 0.7834 6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5532 0.3665 0.3964 8.0996 4.5852 0.3665	6.3003	4.1037	0.4950	
6.6003 4.1908 0.4817 0.7614 6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552	6.4003	4.1355		0.8150
6.7003 4.2178 0.4745 0.7362 6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441	6.5003		0.4906	
6.8003 4.2467 0.4689 0.7085 6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587	6.6003			
6.9003 4.2757 0.4641 0.6802 7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587	6.7003		0.4745	0.7362
7.0003 4.3053 0.4596 0.6514 7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587	6.8003		0.4689	0.7085
7.1003 4.3234 0.4436 0.6383 7.1681 4.2838 0.3892 0.6968 7.1996 4.2027 0.3346 0.7915 7.2996 4.3786 0.4332 0.5845 7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587	6.9003			
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7.2996 4.3786 0.4332 0.5845 7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587				
7.3996 4.4025 0.4222 0.5638 7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587				
7.4996 4.4267 0.4127 0.5421 7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587		4.3786	•	
7.5996 4.4516 0.4028 0.5202 7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587	7.3996			
7.6996 4.4784 0.3948 0.4959 7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587		····		
7.7996 4.5028 0.3851 0.4742 7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587				
7.8996 4.5328 0.3817 0.4447 7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587	7.6996	4.4784		
7.9996 4.5534 0.3680 0.4285 8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587				
8.0996 4.5852 0.3665 0.3964 8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587				
8.1996 4.6078 0.3552 0.3773 8.2996 4.6299 0.3441 0.3587	7.9996			-
8.2996 4.6299 0.3441 0.3587				
		4.6078	0.3552	
8.3618 4.6363 0.3293 0.3572	8.2996			0.3587
	8.3618	4.6363	0.3293	0.3572

Table 1. Continued

(f) Nozzle 10

х	y_R	z_R	R
0.9992	3.0016	0.4936	2.0013
1.0992	3.0007	0.4935	2.0020
1.1992	3.0016	0.4937	2.0013
1.2992	3.0034	0.4953	1.9990
1.3992	3.0022	0.4938	2.0008
1.4992	3.0038	0.4950	1.9992
1.5992	3.0042	0.4957	1.9986
1.6992	3.0040	0.4952	1.9991
1.7992	3.0034	0.4946	2.0000
1.8992	3.0011	0.4922	2.0032
1.9992	3.0077	0.4995	1.9941
2.0992	3.0065	0.4967	1.9969
2.1992	3.0096	0.4998	1.9930
2.2992	3.0102	0.5007	1.9920
2.3992	3.0099	0.4996	1.9928
2.4992	3.0163	0.5063	1.9834
2.5992	3.0288	0.5189	1.9657
2.6001	3.0286	0.5186	1.9656
2.6497	3.0363	0.5263	1.9544
2.7497	3.0539	0.5492	1.9226
2.8497	3.0638	0.5667	1.8945
2.9497	3.0636	0.5688	1.8769
3.0497	3.0713	0.5682	1.8511
3.1497	3.0806	0.5646	1.8252
3.2497	3.0901	0.5606	1.7986
3.3497	3.1009	0.5577	1.7711
3.4497	3.1100	0.5526	1.7454
3.5497	3.1241	0.5520	1.7136
3.6497	3.1308	0.5455	1.6907
3.7497	3.1443	0.5437	1.6599
3.8497	3.1536	0.5399	1.6338
3.9497	3.1647	0.5360	1.6065
4.0497	3.1775	0.5340	1.5761
4.1497	3.1859	0.5287	1.5513
4.2497	3.1972	0.5254	1.5229
4.3497	3.2094	0.5233	1.4930
4.4497	3.2194	0.5197	1.4661
4.5497	3.2333	0.5191	1.4344
4.6497	3.2431	0.5141	1.4084
4.7497	3.2540	0.5115	1.3800
4.8497	3.2647	0.5071	1.3528
4.9497	3.2747	0.5021	1.3264

х	y_R	z_R	R
5.0497	3.2866	0.5002	1.2970
5.1497	3.2976	0.4971	1.2688
5.2497	3.3092	0.4945	1.2402
5.3497	3.3205	0.4912	1.2121
5.4497	3.3313	0.4875	1.1846
5.5497	3.3431	0.4855	1.1556
5.6497	3.3536	0.4812	1.1285
5.7497	3.3650	0.4783	1.0999
5.8497	3.3760	0.4747	1.0724
5.9497	3.3863	0.4717	1.0448
6.0497	3.3957	0.4661	1.0193
6.1497	3.4058	0.4611	0.9928
6.2497	3.4193	0.4606	0.9616
6.3497	3.4299	0.4569	0.9343
6.4497	3.4404	0.4530	0.9069
6.5497	3.4491	0.4475	0.8817
6.6497	3.4608	0.4447	0.8531
6.7497	3.4730	0.4422	0.8241
6.8497	3.4831	0.4382	0.7968
6.9497	3.4932	0.4339	0.7702
7.0497	3.5046	0.4306	0.7418
7.1497	3.5141	0.4261	0.7158
7.2497	3.5261	0.4237	0.6863
7.3497	3.5365	0.4195	0.6592
7.4497	3.5451	0.4140	0.6344
7.5497	3.5560	0.4110	0.6064
7.6497	3.5682	0.4088	0.5769
7.7497	3.5799	0.4058	0.5485
7.8497	3.5877	0.3992	0.5245
7.9497	3.5985	0.3961	0.4967
8.0497	3.6122	0.3950	0.4655
8.1497	3.6198	0.3883	0.4415
8.2497	3.6309	0.3852	0.4135
8.3497	3.6416	0.3817	0.3859
8.4497	3.6545	0.3801	0.3553
8.5497	3.6649	0.3757	0.3281
8.6497	3.6779	0.3738	0.2978
8.7497	3.6925	0.3758	0.2637
8.8497	3.7065	0.3760	0.2307
8.9497	3.7220	0.3782	0.1960
9.0497	3.7374	0.3788	0.1623
9.0732	3.7226	0.3580	0.1820

Table 1. Continued

(g) Nozzle 11

$\overline{}$	y_R	z _R	R
1.0002	3.0021	0.5133	1.9942
	3.0071	0.5177	1.9875
1.1002	3.0071	0.5140	1.9925
1.2002	3.0029	0.5130	1.9928
1.3002	3.0029	0.5136	1.9918
1.4002	3.0039	0.5133	1.9915
1.5002	3.0025	0.5117	1.9935
1.6002	3.0023	0.5143	1.9902
1.7002	3.0036	0.5138	1.9911
1.8002	3.0030	0.5138	1.9834
1.9002		0.5197	1.9826
2.0002	3.0101	0.5197	1.9825
2.1002	3.0103	0.5236	1.9767
2.2002	3.0145		1.9750
2.3002	3.0153	0.5246	1.9736
2.4002	3.0158	0.5253	1.9681
2.5002	3.0197	0.5283	1.9624
2.6002	3.0229	0.5317	1.9493
2.7002	3.0304	0.5382	1.9595
2.7498	3.0234	0.5259	1.9393
2.8000	3.0290	0.5326	
2.9000	3.0545	0.5651	1.8907
3.0000	3.0634	0.5769	1.8535
3.1000	3.0606	0.5759	1.8286
3.2000	3.0563	0.5725	1.8043
3.3000	3.0557	0.5728	1.7749
3.4000	3.0534	0.5719	1.7471
3.5000	3.0533	0.5721	1.7174
3.6000	3.0529	0.5718	1.6881
3.7000	3.0526	0.5721	1.6585
3.8000	3.0479	0.5674	1.6351
3.9000	3.0472	0.5664	1.6066
4.0000	3.0456	0.5653	1.5785
4.1000	3.0428	0.5632	1.5522
4.2000	3.0441	0.5642	1.5205
4.3000	3.0418	0.5620	1.4941
4.4000	3.0402	0.5601	1.4663
4.5000	3.0398	0.5592	1.4376
4.6000	3.0379	0.5577	1.4097
4.7000	3.0355	0.5548	1.3836
4.8000	3.0330	0.5520	1.3571
4.9000	3.0334	0.5523	1.3271
5.0000	3.0300	0.5488	1.3016
5.1000	3.0275	0.5465	1.2754

х	y _R	z_R	R
5.2000	3.0261	0.5447	1.2475
5.3000	3.0224	0.5417	1.2226
5.4000	3.0222	0.5411	1.1931
5.5000	3.0217	0.5407	1.1641
5.6000	3.0185	0.5376	1.1383
5.7000	3.0175	0.5369	1.1099
5.8000	3.0159	0.5353	1.0820
5.9000	3.0146	0.5339	1.0543
6.0000	3.0146	0.5341	1.0241
6.1000	3.0125	0.5317	0.9977
6.2000	3.0119	0.5305	0.9687
6.3000	3.0097	0.5287	0.9417
6.4000	3.0088	0.5280	0.9127
6.5000	3.0077	0.5269	0.8845
6.6000	3.0050	0.5238	0.8584
6.7000	3.0035	0.5229	0.8303
6.8000	3.0022	0.5215	0.8021
6.9000	3.0016	0.5213	0.7733
7.0000	3.0004	0.5207	0.7444
7.1000	2.9984	0.5189	0.7174
7.2000	2.9986	0.5183	0.6878
7.3000	2.9985	0.5186	0.6579
7.4000	2.9967	0.5166	0.6306
7.5000	2.9940	0.5137	0.6047
7.6000	2.9931	0.5127	0.5761
7.7000	2.9920	0.5115	0.5482
7.8000	2.9919	0.5111	0.5185
7.9000	2.9909	0.5102	0.4905
8.0000	2.9887	0.5080	0.4632
8.1000	2.9877	0.5073	0.4349
8.2000	2.9871	0.5065	0.4058
8.3000	2.9868	0.5057	0.3771
8.4000	2.9851	0.5031	0.3500
8.5000	2.9813	0.4991	0.3257
8.6000	2.9795	0.4969	0.2983
8.7000	2.9772	0.4938	0.2724
8.8000	2.9742	0.4911	0.2461
8.9000	2.9708	0.4869	0.2214
9.0000	2.9688	0.4847	0.1941
9.1000	2.9654	0.4815	0.1684
9.2000	2.9615	0.4772	0.1433
9.2410	2.9583	0.4734	0.1356

Table 1. Concluded

(h) Nozzle 12

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				
1.0000 3.0007 0.4884 2.0069 1.1000 3.0025 0.4909 2.0041 1.2000 3.0031 0.4918 2.0035 1.3000 3.0037 0.4922 2.0028 1.4000 3.0034 0.4925 2.0033 1.5000 3.0032 0.4926 2.0036 1.6000 3.0035 0.4930 2.0031 1.7000 3.0048 0.4946 2.0014 1.8000 3.0043 0.4949 2.0008 1.9000 3.0043 0.4942 2.0020 2.0000 3.0043 0.4942 2.0020 2.0000 3.0043 0.4942 2.0041 2.1000 3.0043 0.4942 2.0041 2.2000 3.0073 0.4971 1.9974 2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114	х	y_R	z_R	R
1.1000 3.0025 0.4909 2.0041 1.2000 3.0031 0.4918 2.0035 1.3000 3.0037 0.4922 2.0028 1.4000 3.0034 0.4925 2.0036 1.5000 3.0032 0.4926 2.0036 1.6000 3.0035 0.4930 2.0031 1.7000 3.0048 0.4946 2.0014 1.8000 3.0043 0.4949 2.0008 1.9000 3.0043 0.4942 2.0020 2.0000 3.0043 0.4942 2.0041 2.1000 3.0043 0.4942 2.0041 2.2000 3.0073 0.4971 1.9974 2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0033 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5162 1.9618 2.8000 3.0362 0.5159	1.0000			2.0069
1.3000 3.0037 0.4922 2.0028 1.4000 3.0034 0.4925 2.0033 1.5000 3.0032 0.4926 2.0036 1.6000 3.0035 0.4930 2.0031 1.7000 3.0048 0.4946 2.0014 1.8000 3.0054 0.4949 2.0008 1.9000 3.0043 0.4942 2.0020 2.0000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0144 0.5047	1.1000	3.0025	0.4909	
1.3000 3.0037 0.4922 2.0028 1.4000 3.0034 0.4925 2.0033 1.5000 3.0032 0.4926 2.0036 1.6000 3.0035 0.4930 2.0031 1.7000 3.0048 0.4946 2.0014 1.8000 3.0054 0.4949 2.0008 1.9000 3.0043 0.4942 2.0020 2.0000 3.0043 0.4942 2.0016 2.1000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0073 0.4971 1.9974 2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162	1.2000	3.0031	0.4918	
1.4000 3.0034 0.4925 2.0036 1.5000 3.0032 0.4926 2.0036 1.6000 3.0035 0.4930 2.0031 1.7000 3.0048 0.4946 2.0014 1.8000 3.0054 0.4949 2.0008 1.9000 3.0043 0.4942 2.0020 2.0000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0043 0.4942 2.0016 2.2000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0413 0.5102	1.3000	3.0037		
1.5000 3.0032 0.4926 2.0036 1.6000 3.0035 0.4930 2.0031 1.7000 3.0048 0.4946 2.0014 1.8000 3.0054 0.4949 2.0008 1.9000 3.0043 0.4942 2.0020 2.0000 3.0043 0.4926 2.0041 2.1000 3.0043 0.4942 2.0016 2.2000 3.0073 0.4971 1.9974 2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998	1.4000	3.0034		
1.6000 3.0035 0.4930 2.0031 1.7000 3.0048 0.4946 2.0014 1.8000 3.0054 0.4949 2.0008 1.9000 3.0043 0.4942 2.0020 2.0000 3.0043 0.4926 2.0041 2.1000 3.0043 0.4942 2.0016 2.2000 3.0073 0.4971 1.9974 2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076	1.5000	3.0032		
1.7000 3.0048 0.4946 2.0014 1.8000 3.0054 0.4949 2.0008 1.9000 3.0043 0.4942 2.0020 2.0000 3.0024 0.4926 2.0041 2.1000 3.0043 0.4942 2.0016 2.2000 3.0073 0.4971 1.9974 2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0362 0.5159 1.9555 2.9000 3.0447 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076	1.6000	3.0035	0.4930	
1.8000 3.0054 0.4949 2.0008 1.9000 3.0043 0.4942 2.0020 2.0000 3.0024 0.4926 2.0041 2.1000 3.0043 0.4942 2.0016 2.2000 3.0073 0.4971 1.9974 2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0362 0.5159 1.9555 2.9000 3.0477 0.5182 1.9277 3.0000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086	1.7000	3.0048	0.4946	
2.0000 3.0024 0.4926 2.0041 2.1000 3.0043 0.4942 2.0016 2.2000 3.0073 0.4971 1.9974 2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0362 0.5159 1.9555 2.9000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121	1.8000	3.0054	0.4949	
2.0000 3.0024 0.4926 2.0041 2.1000 3.0043 0.4942 2.0016 2.2000 3.0073 0.4971 1.9974 2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0362 0.5159 1.9555 2.9000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121	1.9000	3.0043	0.4942	2.0020
2.1000 3.0043 0.4942 2.0016 2.2000 3.0073 0.4971 1.9974 2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0362 0.5159 1.9555 2.9000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140	2.0000	3.0024	0.4926	
2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0362 0.5159 1.9555 2.9000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382	2.1000	3.0043	0.4942	
2.3000 3.0064 0.4965 1.9980 2.4000 3.0065 0.4969 1.9976 2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0362 0.5159 1.9555 2.9000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9167 0.5197	2.2000	3.0073	0.4971	1.9974
2.4000 3.0065 0.4969 1.9976 2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0362 0.5159 1.9555 2.9000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216	2.3000	3.0064	0.4965	
2.5000 3.0093 0.4999 1.9935 2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0362 0.5159 1.9555 2.9000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244	2.4000	3.0065	0.4969	
2.6000 3.0144 0.5047 1.9865 2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0362 0.5159 1.9555 2.9000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8691 0.5315	2.5000	3.0093	0.4999	
2.7000 3.0234 0.5114 1.9744 2.7496 3.0326 0.5162 1.9618 2.8000 3.0362 0.5159 1.9555 2.9000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8691 0.5315 1.5424 4.4000 2.8558 0.5327	2.6000	3.0144	0.5047	
2.8000 3.0362 0.5159 1.9555 2.9000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329	2.7000	3.0234	0.5114	
2.9000 3.0477 0.5182 1.9277 3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8691 0.5315 1.5424 4.4000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372	2.7496	3.0326	0.5162	1.9618
3.0000 3.0413 0.5102 1.9090 3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372	2.8000	3.0362	0.5159	1.9555
3.1000 3.0268 0.5033 1.8889 3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409	2.9000	3.0477	0.5182	1.9277
3.2000 3.0119 0.4998 1.8656 3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409	3.0000	3.0413	0.5102	1.9090
3.3000 3.0072 0.5076 1.8274 3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692	3.1000	3.0268	0.5033	1.8889
3.4000 2.9935 0.5082 1.7998 3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692	3.2000	3.0119	0.4998	1.8656
3.5000 2.9793 0.5086 1.7728 3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692	3.3000	3.0072	0.5076	1.8274
3.6000 2.9681 0.5121 1.7425 3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692	3.4000	2.9935	0.5082	1.7998
3.7000 2.9550 0.5140 1.7139 3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692	3.5000	2.9793	0.5086	1.7728
3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692	3.6000	2.9681	0.5121	1.7425
3.8000 2.9420 0.5159 1.6859 3.9000 2.9421 0.5382 1.6346 4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692	3.7000	2.9550	0.5140	1.7139
4.0000 2.9167 0.5197 1.6292 4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692		2.9420	0.5159	
4.1000 2.9039 0.5216 1.6013 4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692		2.9421	0.5382	1.6346
4.2000 2.8917 0.5244 1.5717 4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692		2.9167	0.5197	1.6292
4.3000 2.8801 0.5271 1.5424 4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692		2.9039		1.6013
4.4000 2.8691 0.5315 1.5108 4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692		2.8917	0.5244	1.5717
4.5000 2.8558 0.5327 1.4836 4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692		2.8801	0.5271	1.5424
4.6000 2.8414 0.5329 1.4574 4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692				1.5108
4.7000 2.8308 0.5372 1.4263 4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692		2.8558	0.5327	1.4836
4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692		2.8414		1.4574
4.8000 2.8161 0.5368 1.4004 4.9000 2.8059 0.5409 1.3692	4.7000	2.8308	0.5372	1.4263
3.0.107		2.8161	0.5368	
5.0000 2.7916 0.5411 1.3426				1.3692
0.5/11 1.5420	5.0000	2.7916	0.5411	1.3426

х	УR	^z R	R
5.1000	2.7799	0.5445	1.3120
5.2000	2.7655	0.5443	1.2864
5.3000	2.7546	0.5481	1.2556
5.4000	2.7418	0.5505	1.2267
5.5000	2.7304	0.5542	1.1957
5.6000	2.7172	0.5555	1.1684
5.7000	2.7047	0.5575	1.1402
5.8000	2.6927	0.5610	1.1099
5.9000	2.6815	0.5642	1.0800
6.0000	2.6666	0.5644	1.0541
6.1000	2.6537	0.5659	1.0260
6.2000	2.6416	0.5690	0.9966
6.3000	2.6288	0.5710	0.9681
6.4000	2.6168	0.5741	0.9386
6.5000	2.6049	0.5767	0.9089
6.6000	2.5915	0.5778	0.8818
6.7000	2.5801	0.5807	0.8521
6.8000	2.5664	0.5821	0.8242
6.9000	2.5523	0.5826	0.7973
7.0000	2.5393	0.5839	0.7697
7.1000	2.5275	0.5871	0.7393
7.2000	2.5143	0.5886	0.7117
7.3000	2.5013	0.5902	0.6839
7.4000	2.4888	0.5925	0.6549
7.5000	2.4761	0.5942	0.6268
7.6000	2.4630	0.5963	0.5983
7.7000	2.4498	0.5969	0.5709
7.8000	2.4369	0.5991	0.5427
7.9000	2.4252	0.6019	0.5132
8.0000	2.4122	0.6039	0.4848
8.1000	2.3999	0.6062	0.4555
8.2000	2.3869	0.6082	0.4275
8.3000	2.3739	0.6099	0.3997
8.4000	2.3625	0.6133	0.3691
8.5000	2.3479	0.6125	0.3437
8.6000	2.3359	0.6158	0.3135
8.7000	2.3224	0.6163	0.2867
8.8000	2.3092	0.6181	0.2581
8.9000	2.2983	0.6215	0.2278
9.0000	2.2848	0.6221	0.2001
9.1000	2.2737	0.6252	0.1701
9.1511	2.2648	0.6219	0.1599

Table 2. Pressure Orifice Locations for Each Nozzle

[All dimensions are given in inches]

(a) Nozzle 2

To	D	Left	side	Bottom	
<i>x</i>	у	х	Z	x	<u>y</u>
1.446	-0.004	1.450	-2.191	1.449	-0.007
1.444	-2.606	1.452	0.000	2.143	-0.004
1.447	-3.905	1.451	1.463	2.844	-0.006
1.441	-4.562	1.452	2.194	3.195	-0.004
2.148	-4.454	2.148	2.033	3.895	-0.004
2.147	-3.813	2.148	1.354	5.295	-0.004
2.146	-2.546	2.148	0.002	6.696	-0.004
2.142	-0.002	2.148	-2.027	8.794	-0.007
2.846	-0.002	2.843	-1.861	1.446	-2.609
2.841	-2.486	2.846	0.003	1.444	-4.566
2.847	-3.725	2.844	1.244	2.142	-4.142
2.843	-4.350	2.844	1.865	2.143	-2.550
3.194	-4.300	3.198	1.789	2.843	-2.489
3.195	-3.683	3.195	1.195	2.843	-4.357
3.195	-2.454	3.197	0.003	3.191	-4.303
3.194	0.001	3.199	-1.781	3.191	-2.462
3.898	-0.001	3.896	-1.619	3.891	-2.398
3.894	-2.393	3.896	0.002	3.890	-4.199
3.896	-3.593	3.895	1.080	5.293	-3.988
3.893	-4.192	3.893	1.624	5.291	-2.283
4.595	-0.001	4.597	0.002	6.691	-2.161
5.296	-0.002	5.299	0.006	6.693	-3.777
5.295	-2.275	5.298	0.865	7.292	-3.672
5.296	-3.413	5.296	1.296	7.389	-2.100
5.293	-3.982	5.295	-1.291	8.094	-2.043
5.997	-0.002	5.996	-0.002	8.093	-3.574
6.694	-0.001	6.698	-0.964	8.794	-3.467
6.695	-2.155	6.696	0.002	8.792	-1.983
6.694	-3.234	6.698	0.647		
6.691	-3.771	6.695	0.964		
7.392	-3.672	7.395	0.535		
7.395	-3.141	7.395	0.802		
7.397	-2.097	7.398	0.002		
7.394	-0.002	8.099	0.003		
8.096	-0.002	8.098	0.430		
8.096	-2.034	8.099	0.636		
8.093	-3.051	8.799	0.479		
8.091	-3.566	8.795	0.318		
8.795	-3.458	8.795	0.003	1	
8.795	-2.966	8.798	-0.469	_1	
8.792	-1.976			_	
8.795 8.795	-0.001	ı			

Table 2. Continued

(b) Nozzle 3

7	Top Left side		t side	Bot	tom
<u> </u>	у	X	Z	х	у
1.444	0.005	1.450	-2.171	1.444	-0.011
1.446	-2.694	1.449	0.001	1.446	-2.707
1.444	-4.044	1.450	1.448	1.444	-4.729
1.443	-4.717	1.447	2.169	2.145	-4.550
2.148	-4.532	2.148	2.018	2.148	-2.600
2.139	-3.888	2.146	1.350	2.148	-0.008
2.145	-2.591	2.148	0.004	2.847	-0.002
2.145	-0.003	2.150	-2.017	2.846	-2.501
2.849	0.000	2.850	-1.856	2.846	-4.367
2.844	-2.482	2.850	0.009	3.192	-4.293
2.844	-3.729	2.850	1.246	3.194	-2.443
2.841	-4.358	2.847	1.865	3.195	-0.005
3.195	-4.263	3.195	1.790	3.894	-0.003
3.198	-3.657	3.195	1.191	3.893	-2.343
3.198	-2.439	3.202	0.009	3.893	-4.098
3.197	0.000	3.198	-1.779	5.293	-3.734
3.894	0.010	3.899	-1.621	5.294	-2.139
3.895	-2.335	3.895	0.009	5.290	-0.006
3.898	-3.496	3.896	1.091	6.699	-0.010
3.895	-4.088	3.895	1.632	6.693	-1.932
4.595	0.005	4.599	0.002	6.694	-3.373
5.298	0.006	5.301	0.007	7.392	-3.195
5.298	-2.126	5.299	-1.317	7.394	-1.833
5.301	-3.194	5.295	0.886	8.098	-1.743
5.298	-3.729	5.295	1.321	8.094	-3.017
5.998	0.002	5.999	0.012	8.795	-2.836
6.695	-0.002	6.698	0.010	8.794	-1.624
6.696	-1.923	6.699	0.680	8.795	-0.006
6.698	-2.887	6.696	1.015		
6.699	-3.370	6.704	-1.002		
7.400	-3.184	7.397	0.013		
7.392	-2.724	7.395	0.579		
7.398	-1.814	7.392	0.854		
7.395	0.000	8.099	0.711		
8.098	0.000	8.101	0.481		
8.095	-1.713	8.102	0.009		
8.091	-2.580	8.800	0.010		
8.098	-3.006	8.799	0.373		
8.797	-2.819	8.800	0.558		
8.794	-2.414	8.798	-0.535		
8.798	-1.608				
8.785	0.000				

Table 2. Continued

(c) Nozzle 5

Top	, [Left	side	Bott	
$\frac{10}{x}$	у	x	<u>z</u>	X	<u>y</u>
1.443	0.003	1.450	-1.472	1.448	0.001
1.446	-2.499	1.447	-0.003	2.150	0.001
1.447	-3.745	1.447	1.469	2.843	-0.001
1.443	-4.376	1.447	2.167	3.195	0.001
2.145	-4.373	2.149	2.169	3.897	-0.002
2.147	-3.747	2.152	1.358	5.295	0.001
2.143	-2.499	2.152	-0.002	6.698	-0.001
2.150	0.002	2.152	-1.359	8.796	-0.001
2.841	0.000	2.847	-1.246	1.450	-2.500
2.843	-2.499	2.851	0.002	2.147	-2.499
2.843	-3.750	2.850	1.246	2.848	-2.502
2.843	-4.375	2.847	2.143	3.196	-2.500
3.192	-4.373	3.196	2.050	3.895	-2.499
3.194	-3.750	3.201	1.187	5.297	-2.500
3.192	-2.499	3.201	0.000	6.698	-2.500
3.191	-0.000	3.198	-1.189	7.396	-2.500
3.890	-0.000	3.899	-1.079	8.097	-2.501
3.894	-2.501	3.895	-0.002	8.795	-2.499
3.894	-3.748	3.897	1.072	1.447	-4.371
3.890	-4.378	3.899	1.863	2.144	-4.369 4.373
4.589	0.001	4.601	-0.003	2.845	-4.373
5.291	-0.000	5.300	0.000	3.198	-4.369
5.295	-2.499	5.302	-0.852	3.895	-4.373
5.294	-3.751	5.300	0.849	5.297	-4.374 -4.374
5.293	-4.376	5.297	1.477	6.697	-4.376
5.991	0.000	6.002	-0.001	7.396	-4.370 -4.370
6.691	-0.002	6.700	-0.001	8.095	-4.374
6.696	2.501	6.701	-0.627	8.796	<u> </u>
6.696	-3.750	6.700	0.624		
6.694	-4.377	6.699	1.098	1	
7.391	-4.376	7.395	0.906		
7.389	-3.750	7.399	0.507		
7.389	-2.501	7.399	-0.002		
7.391	0.002	8.100	-0.004		
8.093	0.002	8.100	0.394		
8.098	-2.502	8.097	0.715	}	
8.095	-3.746	8.799	0.524	1	
8.093	-4.378	8.799	0.285		
8.795	-4.379	8.801	-0.001	1	
8.794	-3.750	8.802	-0.284		
8.792	-2.498	Į.			
8.791	-0.002				

Table 2. Continued
(d) Nozzle 6

	Гор	Le	ft side	T Bo	ottom
	у	х	Z	x	
1.446	-0.002	1.460	-1.456	1.444	y 0.016
1.449	-2.605	1.449	0.004	1.444	-0.016
1.444	-3.910	1.439	1.467	1.444	-2.605
1.449	-4.561	1.436	2.206	2.138	-4.553
2.148	-4.459	2.137	2.209	2.136	-4.452
2.145	-3.822	2.142	1.362	2.143	-2.547
2.148	-2.548	2.148	0.010	2.148	-0.002
2.148	-0.015	2.157	-1.344	2.846	0.002
2.847	-0.007	2.855	-1.229	2.839	-2.485
2.844	-2.488	2.854	0.018	3.189	-4.348
2.849	-3.734	2.841	1.264	3.189	-4.294
2.844	-4.353	2.836	2.202	3.192	-2.454
3.197	-4.299	3.184	2.114	3.891	0.002
3.194	-3.688	3.190	1.204	3.893	0.003
3.195	-2.460	3.197	0.015	3.890	-2.397
3.195	-0.005	3.206	-1.174	5.288	-4.187
3.896	-0.003	3.907	-1.059	5.294	-3.976
3.899	-2.399	3.898	0.021	5.296	-2.277
3.893	-3.594	3.896	1.099	6.699	0.000
3.894	-4.195	3.890	1.930	6.696	0.002
4.600	-0.002	4.601	0.024	6.694	-2.166
5.296	0.000	5.296	0.029	7.392	-3.776
5.293	-2.279	5.293	0.889	7.392	-3.668
5.299	-3.419	5.292	1.565	8.094	-2.101
5.298	-3.980	5.304	-0.834	8.094 8.094	-2.038
5.994	0.000	6.003	0.031	8.795	-3.557
6.698	-3.772	6.699	-0.612	8.794 8.794	−3.457 −1.976
6.698	-3.233	6.699	0.040	8.792	
6.696	-2.154	6.693	0.680	0.192	0.002
6.698	-0.002	6.691	1.196		
7.397	-0.005	7.392	1.014		
7.397	-2.098	7.395	0.576		
7.397	-3.140	7.400	0.042		
7.397	-3.673	8.102	0.042		
8.090	-3.562	8.094	0.470		
8.096	-3.054	8.094	0.826		
8.098	-2.041	8.795	0.650		
8.099	0.000	8.795	0.363		
8.795	-0.005	8.798	0.051		
8.798	-1.975	8.800	-0.269		
8.794	-2.961		0.207		
8.794	-3.458				

Table 2. Continued

(e) Nozzle 7

To	op	Left	side	Bott	tom
x	y	x	z	х	у
1.452	0.003	1.457	-1.445	1.450	0.003
1.451	-2.697	1.457	-0.001	1.453	-2.695
1.454	-4.047	1.457	1.448	1.450	-4.710
1.453	-4.715	1.452	2.204	2.150	-4.537
2.149	-4.536	2.156	2.205	2.148	-2.593
2.155	-3.891	2.157	1.341	2.152	0.006
2.154	-2.592	2.153	-0.001	2.847	-0.002
2.154	0.002	2.157	-1.345	2.845	-2.491
2.852	0.003	2.853	-1.240	2.846	-4.357
2.850	-2.487	2.854	-0.001	3.198	-4.268
2.849	-3.734	2.853	1.240	3.198	-2.435
2.848	-4.355	2.856	2.194	3.198	0.000
3.200	-4.263	3.208	2.114	3.902	-0.002
3.198	-3.655	3.203	1.187	3.899	-2.334
3.198	-2.436	3.206	0.001	3.899	-4.087
3.198	0.001	3.203	-1.194	5.300	-3.724
3.901	0.003	3.903	-1.089	5.302	-2.133
3.898	-2.336	3.903	-0.003	5.301	-0.003
3.900	-3.502	3.905	1.084	6.699	-0.001
3.901	-4.086	3.906	1.937	6.701	-1.921
4.603	0.002	4.604	-0.002	6.698	-3.362
5.301	0.001	5.302	-0.004	7.400	-3.184
5.304	-2.130	5.306	-0.885	7.402	-1.820
5.300	-3.194	5.305	0.878	8.102	-1.720
5.299	-3.728	5.306	1.582	8.102	-3.006
6.002	0.001	6.003	-0.001	8.801	-2.820
6.702	0.003	6.705	-0.002	8.802	-1.612
6.699	-1.922	6.703	-0.675	8.798	-0.001
6.699	-2.880	6.704	0.668		
6.697	-3.365	6.702	1.226		
7.403	-3.185	7.404	1.051		
7.399	-2.727	7.407	0.567		
7.400	-1.817	7.405	-0.003		
7.398	0.003	8.103	-0.002		
8.102	0.003	8.102	0.468		
8.099	-1.713	8.106	0.870		
8.103	-2.576	8.809	0.687		
8.099	-3.002	8.803	0.366		
8.797	-2.820	8.805	0.000		
8.800	-2.422	8.804	-0.371	J	
8.800	-1.615				
8.802	0.004				

Table 2. Continued

(f) Nozzle 8

Te	op	Left	side	Bot	tom
x	y	X	z	x	у
1.447	-0.002	1.452	-1.421	1.450	0.006
1.447	-2.796	1.453	0.004	1.450	-2.795
1.450	-4.193	1.452	1.431	1.450	-4.888
1.451	-4.895	1.448	2.206	2.150	-4.638
2.146	-4.637	2.146	2.206	2.148	-2.654
2.147	-3.980	2.152	1.335	2.146	0.006
2.144	-2.650	2.151	0.009	2.853	0.000
2.147	0.003	2.152	-1.330	2.851	-2.507
2.850	-0.001	2.850	-1.240	2.853	-4.391
2.850	-2.502	2.850	0.004	3.199	-4.265
2.850	-3.765	2.853	1.240	3.199	-2.438
2.850	-4.387	2.852	2.196	3.199	0.000
3.196	-4.259	3.201	2.132	3.902	0.005
3.198	-3.648	3.201	1.191	3.902	-2.291
3.196	-2.434	3.201	-0.001	3.895	-4.009
3.198	0.002	3.200	-1.191	5.299	-3.504
3.897	0.004	3.900	-1.100	5.302	-2.005
3.898	-2.286	3.904	0.001	5.295	0.005
3.898	-3.437	3.900	1.095	6.698	0.005
3.895	-4.007	3.905	1.969	6.702	-1.713
4.597	0.004	4.601	0.001	6.698	-3.009
5.295	0.001	5.297	-0.008	7.401	-2.758
5.297	-1.999	5.300	-0.917	7.398	-1.575
5.294	-3.004	5.297	0.904	8.099	-1.429
5.297	-3.502	5.302	1.642	8.100	-2.504
6.000	0.006	5.999	-0.005	8.802	-2.250
6.697	0.004	6.703	1.310	8.799	-1.284
6.698	-1.711	6.699	0.723	8.799	-0.003
6.697	-2.568	6.702	-0.008		
6.695 7.396	-3.004 2.740	6.700	-0.729		
7.396	-2.749	7.401	-0.006		
7.396	-2.355 -1.565	7.404	0.625		
7.398	0.002	7.406 8.106	1.150		
8.098	-0.002 -0.001	8.100 8.103	0.997		
8.100	-0.001 -1.424	8.105 8.105	0.532 0.003		
8.097	-1.424 -2.144	8.801	-0.003 -0.010		
8.097	-2.1 44 -2.499	8.803	-0.010 -0.444		
8.798	-2.242	8.798	0.439		
8.793	-1.923	8.799	0.439		
8.798	-1.281	0.177	0.050		
8.798	-0.001				
0.770	-0.001				

Table 2. Continued

(g) Nozzle 9

To	<u> </u>	Left	side	Botte	om
$\frac{10}{x}$	у	x	Z	х	у
1.447	-0.005	1.450	-1.472	1.442	0.003
1.447	-1.250	1.450	-0.002	1.442	-2.501
1.443	-2.499	1.448	1.469	1.446	-3.754
1.447	-3.750	1.451	1.921	2.144	-3.751
2.149	-3.750 -3.750	2.144	1.921	2.143	-2.500
	-3.750 -2.505	2.148	1.356	2.144	-0.002
2.144	-2.303 -1.250	2.147	-0.002	2.843	-0.003
2.144 2.144	-0.001	2.147	-1.357	2.843	-2.499
	-0.001 -0.004	2.850	-1.251	2.847	-3.759
2.843	-0.004 -1.250	2.850	-0.001	3.199	-3.756
2.843 2.845	-2.502	2.851	1.242	3.194	-2.501
2.843	-3.762	2.851	1.867	3.191	-0.003
3.202	-3.752 -3.752	3.196	1.801	3.892	-0.002
3.196	-2.510	3.201	1.190	3.892	-2.501
3.194	-1.251	3.196	-0.002	3.898	-3.753
3.196	-0.001	3.201	-1.194	5.294	-3.751
3.895	-0.001 -0.004	3.903	-1.087	5.292	-2.501
3.895	-1.245	3.895	-0.005	5.292	-0.000
3.897	-2.497	3.898	1.078	6.692	0.003
3.905	-3.746	3.897	1.631	6.695	-2.496
4.593	0.001	4.599	-0.006	6.692	-3.751
5.297	-0.001	5.298	-0.004	7.391	-3.748
5.295	-1.253	5.298	-0.856	7.398	-2.499
5.297	-2.500	5.302	0.846	8.092	-2.498
5.294	3.749	5.297	1.303	8.091	-3.750
5.993	0.001	5.999	-0.005	8.793	-3.756
6.693	-0.001	6.698	-0.002	8.791	-2.496
6.695	-1.251	6.697	-0.628	8.791	0.003
6.697	-2.506	6.697	0.626		
6.695	-3.750	6.702	0.974		
7.401	-3.746	7.401	0.801		
7.398	-2.503	7.396	0.512		
7.396	-1.250	7.398	-0.001		
7.398	-0.001	8.100	0.003		
8.095	-0.001	8.102	0.399		
8.097	-1.250	8.102	0.637		
8.092	-2.497	8.795	0.483		
8.097	-3.750	8.799	0.286		
8.799	-3.749	8.798	0.002		
8.794	-2.505	8.801	-0.294		
8.796	-1.248				
8.793	0.001				

Table 2. Continued

(h) Nozzle 10

Т	ор	Lef	t side	Во	ttom
x	у	x	Z	x	V
1.443	-0.006	1.449	-1.454	1,443	0.000
1.443	-1.302	1.449	0.003	1.441	-2.605
1.442	-2.607	1.448	1.465	1.445	-3.904
1.446	-3.906	1.443	2.289	2.143	-3.815
2.147	-3.819	2.145	1.910	2.145	-2.546
2.146	-2.549	2.146	1.354	2.143	0.000
2.149	-1.276	2.146	0.001	2.843	0.002
2.143	-0.003	2.150	-1.346	2.843	-2.484
2.847	-0.004	2.850	-1.238	2.844	-3.724
2.847	-1.243	2.847	0.001	3.193	-3.679
2.848	-2.491	2.846	1.245	3.191	-2.456
2.845	-3.724	2.850	1.904	3.192	0.002
3.193	-3.681	3.192	1.827	3.893	0.002
3.195	-2.461	3.197	1.192	3.893	-2.396
3.198	-1.234	3.195	0.004	3.892	-3.589
3.195	-0.003	3.198	-1.188	5.289	-3.408
3.895	-0.007	3.895	-1.077	5.291	-2.273
3.896	-1.201	3.896	0.005	5.290	0.006
3.896	-2.395	3.897	1.083	6.695	0.004
3.897	-3.597	3.892	1.677	6.692	-2.153
4.595	-0.006	4.594	0.004	6.691	-3.231
5.295	-0.008	5.295	0.006	7.391	-3.141
5.298	-1.139	5.298	-0.861	7.391	-2.094
5.297	-2.279	5.298	0.867	8.089	-2.035
5.295	-3.413	5.291	1.355	8.086	-3.050
5.995	-0.006	5.996	0.008	8.790	-2.962
6.697	-0.004	6.697	0.003	8.791	-1.974
6.697	-1.077	6.695	-0.642	8.791	0.000
6.696	-2.156	6.695	0.648		
6.697	-3.235	6.695	1.039		
7.396	-3.143	7.395	0.878		
7.396	-2.098	7.391	0.539		
7.397	-1.050	7.393	0.004		
7.395	-0.002	8.096	0.009		
8.096	-0.002	8.095	0.428		
8.095	-1.021	8.095	0.720		
8.095	-2.037	8.795	0.562		
8.098	-3.054	8.793	0.322		
8.801	-2.965	8.793	0.010		
8.799	-1.978	8.795	-0.310		
8.801	-0.991				
8.795	-0.001				

Table 2. Continued

(i) Nozzle 11

То	р	Left	side	Bott	
x	у	Х	Z	X	у
1.444	-0.006	1.446	-1.446	1.448	-0.005
1.443	-1.354	1.447	-0.008	1.447	-2.699
1.443	-2.702	1.447	1.437	1.445	-4.043
1.391	-4.048	1.451	1.904	2.143	-3.894
2.143	-3.890	2.149	1.904	2.143	-2.598
2.142	-2.596	2.147	1.340	2.145	-0.005
2.143	-1.298	2.147	-0.005	2.844	-0.002
2.143	-0.003	2.147	-1.344	2.841	-2.495
2.844	-0.004	2.847	-1.241	2.842	-3.737
2.842	-1.250	2.847	-0.008	3.194	-3.661
2.839	-2.495	2.846	1.237	3.192	-2.442
2.842	-3.737	2.846	1.893	3.194	-0.002
3.188	-3.665	3.197	1.812	3.894	-0.006
3.191	-2.445	3.194	1.182	3.895	-2.343
3.191	-1.224	3.194	-0.005	3.893	-3.509
3.193	-0.006	3.193	-1.191	5.294	-3.199
3.890	-0.005	3.898	-1.089	5.294	-2.135
3.892	-1.169	3.891	-0.007	5.291	-0.007
3.894	-2.339	3.895	1.078	6.692	-0.003
3.891	-3.509	3.898	1.654	6.695	-1.931
4.593	0.000	4.588	0.000	6.691	-2.891
5.287	-0.003	5.295	-0.004	7.394	-2.736
5.292	-1.069	5.295	-0.881	7.391	-1.823
5.293	-2.131	5.297	0.874	8.097	-1.721
5.295	-3.199	5.295	1.389	8.095	-2.562
5.990	0.004	5.990	-0.006	8.796	-2.428
6.689	-0.001	6.687	-0.004	8.798	-1.620
6.690	-0.965	6.691	-0.674	8.797	-0.005
6.690	-1.928	6.691	0.672		
6.692	-2.888	6.695	1.098		
7.390	-2.734	7.395	0.949		
7.390	-1.821	7.391	0.567		
7.393	-0.911	7.390	-0.007		
7.391	0.002	8.086	-0.006	Ì	
8.091	-0.002	8.092	0.464		
8.091	-0.862	8.095	0.802		
8.089	-1.720	8.791	-0.368		
8.092	-2.581	8.786	-0.011		
8.791	-2.443	8.789	0.360		
8.791	-1.616	8.792	0.654		
8.791	-0.808				
8.790	0.000]			

Table 2. Concluded

(j) Nozzle 12

7	Гор	Lef	t side	Bo	ttom
x	у	x	Z	X	y
1.443	-0.003	1.445	-1.426	1.440	-0.003
1.444	-1.399	1.447	-0.001	1.440	-2.799
1.447	-2.799	1.443	1.423	1.440	-4.196
1.443	-4.197	1.444	1.916	2.139	-3.980
2.143	-3.977	2.143	1.917	2.135	-2.657
2.144	-2.652	2.142	1.330	2.139	-0.004
2.143	-1.328	2.147	-0.001	2.837	-0.003
2.143	-0.003	2.147	-1.329	2.838	-2.511
2.843	-0.006	2.846	-1.233	2.837	-3.761
2.839	-1.256	2.842	0.004	3.189	-3.656
2.839	-2.507	2.845	1.238	3.189	-2.442
2.843	-3.763	2.842	1.913	3.187	-0.002
3.191	-3.657	3.193	1.857	3.886	-0.003
3.193	-2.436	3.195	1.192	3.889	-2.296
3.192	-1.221	3.192	0.002	3.888	-3.441
3.190	-0.005	3.194	-1.181	5.288	-3.009
3.889	-0.005	3.895	-1.097	5.287	-2.010
3.890	-1.150	3.893	-0.002	5.290	-0.001
3.891	-2.292	3.891	1.096	6.691	-0.001
3.892	-3.442	3.891	1.724	6.688	-1.719
4.589	-0.007	4.588	0.002	6.688	-2.580
5.288	-0.004	5.293	-0.910	7.391	-2.363
5.289	-0.999	5.291	0.001	7.388	-1.573
5.291	-2.004	5.293	0.910	8.091	-1.432
5.293	-3.006	5.291	1.459	8.087	-2.144
5.991	-0.003	5.991	-0.001	8.791	-1.931
6.688	-0.003	6.694	-0.723	8.790	-1.287
6.691	-0.859	6.693	-0.002	8.790	-0.003
6.695	-1.717	6.691	0.720		0.000
6.692	-2.578	6.688	1.200		
7.395	-2.356	7.390	1.067		
7.396	-1.574	7.398	0.633		
7.395	-0.787	7.394	0.001		
7.398	-0.002	8.092	0.936		
8.092	-0.002	8.101	0.535		
8.095	-0.713	8.091	-0.002		
8.095	-1.428	8.793	-0.446		
8.091	-2.140	8.790	0.000		
8.792	-1.927	8.795	0.442		
8.795	-1.284	8.789	0.807		
8.794	-0.643				
8.793	-0.004				

Table 3. Index of Configurations(a) Nozzle configurations tested

Nozzle		$\beta_{t,\text{top/bot}}/\beta_t$,side, deg		1	Corner radius	
(a)	17.9/0	17.3/9.7	16.4/16.4	15.0/22.4	Sharp	1 in.	2 in.
(1)	X			· 	Х	'	
2	*	x			Х		
3			x		X		
(4)				X	X		İ
5	x					X	
6		x			Ì	Х	ļ
7			x			Х	
8				x		Х	
9	X						У
10		x					X
11			x				Х
12				x			X

a Nozzle number in parentheses indicates data not presented.

(b) Data tables and figures

Nozzle	Solid plume	Table	Figures
2	On	4	7(a)-7(c), 8(a), 10, 14
3	On	5	7(d)-7(f), 8(b), 11, 14
3	Off	6	7(d)-7(f), 13(b)
5	On	7	7(g)-7(i), 8(c), 9, 15
5	Off	8	7(g)-7(i), 13(a), 17(a)
6	Off	9	7(j)-7(1)
7	On	10	7(m)-7(o), 8(d), 11, 15
7	Off	11	7(m)-7(o), 13(b), 17(a)
8	On	12	7(p), 7(q), 8(e), 12, 15
8	Off	13	7(p), 7(q), 13(c), 17(a)
9	On	14	7(r)-7(t), $8(f)$, 9 , 16
9	Off	15	7(r)-7(t), $13(a)$, $17(b)$
10	On	16	7(u)-7(w), $8(g)$, 10 , 16 ,
10	Off	17	7(u)-7(w), $17(b)$
11	On	18	7(x)-7(z), $8(h)$, 11, 16
11	Off	19	7(x)-7(z), 13(b), 17(b)
12	On	20	7(aa)-7(cc), 8(i), 12, 16
12	Off	21	7(aa)-7(cc), 13(c), 17(b)

Table 4. Pressure and Force Data for Nozzle 2 With $\beta_{t,top/bot} = 17.3^{\circ}/\beta_{t,side} = 9.7^{\circ}$, Plume On, and $\alpha = 0^{\circ}$

(a) Static pressure coefficients on nozzle top flap

			.926	0.219	0.189	0.042	0000	0,70	-0.112	-0.126	0.125	57	-0.093	0.050) 20	07070	-0.008	0.030	5	0.182	0.213	
		+	_		_	\vdash	F	\dagger	1		H	1		-	\dagger	+	_	H	\dagger	-	_	ł
			833	0.193	0.168	0.00	-0.117		-0:17p	-0.1 <u>4</u>	J 156		-0.125	960'0-	0.000	3	-0.042	000		0.163	0.188	0010
		0.00	6//:	0.159	0.145	-0.018	-0.131	1.73	77.7	-0.158	-0.173		-0.151	-0.123	0000	0.000	-0.073	-0.020		0.141	0.156	0110
	line	202	SO/:	0.115	0.111	-0.048	-0.143	0.150	0.1.0	-0.173	-0.190		1/10	-0.147	-0 116	000	-U.098	0.047	0110	0.110	0.115	0.103
	lap at center	633	260.	0.064	0.068	-0.075	-0.156	891 0	001.00	ص 190	-0.205	100	-0.185	-0.166	-0.140	2010	-0.120	-0.074	0 0 0	0.009	0.066	0.056
	with values of v// of—	\$58	0000	-0.001	0.00	-0.110	-0.184	-0.193		117.0	-0.219	0000	-0.202	-0.188	-0.168	0.152	0.1.0	601.0	1100	0.011	0.001	010
1000	ocificients o with values	484		-	-		_	1		'	1			ı	1			1	-		1	1
o de constante de la constante	Static pressure coefficients on nozzle top flap at centerline with values of v/l of—	411	3000	0.22.2	0.211	-0.212	-0.500	-0.542	0,604	0.00	-0.289	J 240	25.0	-0.23U	-0.221	0220-		-0.211	-0.207	3000	22.0	-0.220
Sta	Sid	.337	0.547	0.570	635	-0.324	-0.521	-0.569	0690	20.0	-0.409	0 332	2000	-0.293	-0.283	-0.292	01.0	415.0	-0.564	0 540	200	54.7
		.300	-1 096	1 383	1.000	70.00	10.5//	-0.416	-0.473	002.0	60/02	0.663	0,640	25.5	-0.638	-0.670	0.00	27.7	-1.340	-1 084	0.070	7.0.7
		.226	-0.459	-0.447	0.330	0.017	/10:01	-0.024	-0.048	7710	001.00	-0.197	200	2500	0.230	-0.277	230	13.50	-0.444	-0.457	0.412	7.41.7
		.153	-0.304	-0.294	20,00	0100	010.0	0.010	-0.031	51 5	101.0	-0.1.26	-0.153	1210		-0.188	1660-		767.0-	-0.304	580	707.0
	1	N _∞	0.599	0.700	0.801	1 250	2021	1.701	1.149	0.950	2000	0.920	0.899	t	t	0.852	0.801	107.0	0.701	0.603	0.400	1

Static pressure coefficients on nozzle top flap at $y/Y = 0.50$ with values of y/I of—	705 770 853	C.O. (1); CO.O. (2000 OLOO OCS O	0.220 -0.210 -0.000	-0.359 -0.204 0.005 0.107 0.143 0.168 0.188	-0.353 -0.223 -0.112 -0.047 -0.018 0.008 0.028	0.124 0.116	011.0 421.0 61.0	0.500 0.500 0.133 -0.137	+	-0.438 -0.306 -0.228 -0.201 -0.180 0.162 0.130	201.00 0.100	0.212	-0.344 -0.257 -0.194 -0.149 -0.125 -0.096 -0.065	t	0100	01.00	+	-0.551 -0.201 0.007 0.106 0.140 0.145 0.105	0.100	0.00 0.000 0.109	-0.50 -0.203 -0.009 0.095 0.141 0.179 0.10
e coefficients on nozz	.411 55	\dagger	+	\dashv			H	\dagger	1		t	+			H	\dagger	1	_	H	t	_
Static pressur	300 337	-1 086 -0 520	\dagger	7	-0.843 -0.353	-0.365 -0.523	-0.407 -0.570	t	\dagger	-0.724 -0.438	-0.718 -0.381	\dagger	1	-0.697 -0.326	-0.719 -0.323	0.835 0.353	\dagger	-1.345 -0.551	-1.075 -0.516	7280 6780	\exists
	. 226	-0.4261	\dagger	+		-0.011	0.018	5043	+	-0.155	-0.185	l	1	-0.240	-0.265 -0.	0.312	\dagger	-0.413	-0.423 -1.	J 381	1
	.153	-0.274	796.0	0.200	-0.208	-0.005	-0.005	-0.024	200	21	-0.118	171	ш	וח	-0.176	-0.205	3700	-0.203	-0.271	-0.253	
	M _∞	0.599	0.700	1000	0.901	1.250	1.201	1.149	0000	0.230	0.926	0 800	0.072	0.0/2	0.852	0.801	0.701	7.70	0.603	0.400	

Table 4. Continued

(a) Concluded

			Stat	lic pressure c	Static pressure coefficients on nozzle top flap at $y/Y = 0.75$	nozzle top	$\int \int dx dx = \int \int dx dx$	0.75		
					with values of x/l of-	—Jo <i>I/X</i> Jo				
×	153	226	300	.337	114.	.558	.705	6 <i>LL</i>	.853	.926
0050	0.240	928 0-	-0.972	-0.465	-0.187	1	0.090	0.132	0.176	0.213
0.00	0.243	-0.379	-1.274	-0.486	-0.188		0.097	0.134	0.165	0.193
1080	001 0	-0 299	-0.923	-0.412	-0.223		-0.034	-0.010	0.024	0.068
0.001	9000	1109	-0.369	-0.516	-0.454	1	-0.127	-0.116	-0.108	-0.083
1.230	0000	0100	-0410	-0.564	-0.491		-0.145	-0.133	-0.120	-0.098
1.201	0.00	0.048	-0.461	-0.626	-0.546	1	-0.165	-0.151	-0.134	-0.111
1.149	0.020	0.00	-0.747	-0.484	-0.323		-0.199	-0.184	-0.163	-0.131
0.930	20.07	0.130	0.748	0.417	-0.797	ı	-0.173	-0.151	-0.122	-0.085
0.920	-0.113	0.0.0	0.775	0.277	0 273		-0 146	-0.119	-0.082	440.0
0.899	-0.139	-0.210	0.733	0.250	0.750		0 115	-0.087	-0.051	-0.007
0.873	-0.156	-0.234	-0.730	0.538	0.2.30		2000	0.065	0.031	0.014
0.852	-0.170	-0.258	-0.762	-0.559	-0.248	'	-0.07	COO.O	500	9000
0.801	901.0	-0.302	006:0-	-0.411	-0.222	1	-0.036	-0.010	0.023	0.003
102.0		-0.379	-1.236	-0.479	-0.185	ı	0.094	0.131	0.160	0.187
0.701	0770	0.375	-0.963	-0.460	-0.186	1	0.091	0.132	0.173	0.209
0.003	0.240	-0.339	-0.790	-0.412	-0.174	1	0.079	0.119	0.162	0.203
201.0										

				_	_	_	_			_	_	_	Τ	_	_		_	_			1
	926	0.197	0.187	0.085	7200	7.0.7	-0.089	-0.097	0 120	77.1	-0.077	_0.035	200	0.002	0.026	0.084	104	0.104	0.195	0.184	
	.853	0.154	0.152	0.044	101	-0.102	-0.114	-0.128	0710	7.143	-0.107	2200	200	-0.036	-0.014	0.045	1210	0.131	0.152	0.142	
875	<i>6LL</i> :	0.113	0.116	0.014	20.0	-0.122	-0.134	-0.149	2210	-0.1/0	-0.140	0.106	9.100	-0.073	-0.048	0.013	200	0.116	0.113	0 101	
p at $y/Y = 0$.	705	0.072	0.079	0.014	10:0	-0.140	-0.156	171 0		-0.195	-0.167	0.125	33	-0.103	-0.079	0.015	0.0.0	0.080	0.072	0.064	150.0
nozzle top fla	.558	-0.024	20017	7800	-0.004	-0.303	-0.325	-0 345	2	-0.233	-0.216	0 105	0.130	-0.167	-0.144	0.083	00.0	-0.015	-0.022	2000	10.02.7
fficients on nozzle top with values of x/l of—	.411	-0 183	0810	2000	-0.200	-0.342	-0.375	9670	27.7	-0.326	-0.294	0200	20.7/8	-0.264	-0.255	0000	20.200	-0.187	181.0	9910	001.7
Static pressure coefficients on nozzle top flap at $y/Y = 0.875$ with values of x/I of—	.337	0.412	0.440	15.0	-0.433	-0.502	-0.550	0070	0.000	-0.507	-0.442		-U.401	-0.382	-0.389	0.433	-0.433	-0.433	0410	0300	705.0
Static	300	0.850	170	-1.001	-0.980	-0.355	193	1370	10.431	-0.728	97.0	0:130	-0.771	-0.778	008.07	2000	-0.960	-1.037	0.842	700	45/5
	326	2300	0.275	-0.345	-0.289	9000	0.014	10.0	-U.044	-0.143	177	7.1.7	-0.202	922.0-	0.250	0.530	-0.288	-0.343	0 331	1000	-0.297
	153	5100	-0.213	-0.220	-0.188	-0.003	7000	13.0	-0.028	980 0-	0110	0.110	-0.133	-0.148	0.163	-0.103	-0.186	0160	0.213	217.0-	961
	*	8000	0.599	0.700	0.801	1 250	T	Т	1.149	0.050	Т		0.899	0.873	C/0.0	0.832	0.801	107.0	0.701	0.003	0.400

Table 4. Continued

(b) Static pressure coefficients on nozzle sidewall

	\neg	$\overline{}$		_	_	_	_	_	•	_	_	_	ш,	_	_	_	_	_	_
	926	2	1	-	•	-	_	1					-	1			1	1	ı
	853	0.122	0.133	0.137	0.037	51.13	-0.112	-0.120	-0.105	0200	0.000	0.0-0	-0.010	0.010	0.056	0.135	0.133	0.133	0.118
.75	977	0000	0.003	0.005	0.023	0.169	07.70	-0.173	-0.125	-0.093	0.055	0.000	-0.03/	-0.019	0.025	200	0.000	0.000	0.0//
vall at $z/Z = 0$	705	0.043	0.048	0.00	0.00	0.722	0.233	-0.238	-0.142	0110	2000	6,000	00.0	-0.042	-0.003	0.051	7700	0.0	0.03/
nozzle sidev	.558	50.048	-0.045	990	986 0	0.200	7220	-0.33/	-0.191	-0.158	961.0-	201.0	31.7	0.000	-0.065	5083	0.045	1500	-0.041
efficients on nozzle side with values of v/l of	114.	-0.180	-0.193	181 9	0 300	0.338	2000	0.200	-0.414	-0.351	-0.285	0.217	717.0	-0.189	-0.182	-0.188	0819	0,100	201.7
Static pressure coefficients on nozzle sidewall at $z/Z = 0.75$ with values of z/l of	.337	-0.313	-0.350	-0.349	-0 333	-0.364	0.416	914	-0.645	089.0	-0.686	0.650	0.000	-0.563	-0.351	-0.346	-0.315	1200	1/7.0
Stat	.300	-0.501	-0.579	-0.918	-0.322	-0.361	5116	C11.7	-0.677	-0.722	-0.778	P 828	20.0	-0.877	-0.897	-0.574	-0.498	3070	0.74
	.226	-0.285	-0.313	-0.293	-0.004	-0.014	-D 047	10.0	-0.148	-0.175	-0.206	-0.231	2000	-0.252	-0.289	-0.307	-0.284	-0.757	7.77
	.153	-0.197	-0.210	-0.191	-0.003	-0.006	-0.032	2000	-0.087	-0.112	-0.134	-0.150	0.167	70.10	-0.189	-0.206	-0.195	-0.176	2
	M∞	0.599	0.700	0.801	1.250	1.201	1.149		0.950	0.926	0.899	0.873	0.000	0.032	0.801	0.701	0.603	0.400	

\Box	_	Т	Т	Т	_	Г	1	Т	7		Г	Т	Т		_	Т	T	_		Т	
	926	1010	0.181	0.182	0.108	-0.049	-0.053	1200	100.7	-0.029	7007	0.00	0.012	0.041	0.061	021.00		0.181	0.180	0 169	``
	853	124	0.134	0.137	0.004	-0.123	-0113	0 1 20	-0.120	-0.091	0900	0000	0.027	0.000	0.020	0.065	25.00	0.13/	0.133	0.122	
Static pressure coefficients on nozzle sidewall at $z/Z = 0.50$ with values of z/I of	779	7600	0.000	0.091	0.028	-0.187	-0.183	0 183	0.103	-0.111	-0.081	0.054	1000	-0.029		0.031	2000	260.0	0.087	080.0	1
	705	0.043	0.00	0.030	-0.002	-0.230	-0.244	0.250	0.230	-0.128	-0.100	9200	2,500	-0.033	-0.036	000	0000	0.00	0.044	0.037	
nozzle sidev	.558				1	I	1			,	ı			'	1	ı			-	ı	
efficients on nozzle side with values of v/l of	.411	-0.176	2010	167	701.07	-0.326	-0.359	-0.414	200	-0.220	-0.435	-0.305	0100	20.219	-0.190	-0.183	7819	101.0	-0.178	-0.158	
ic pressure co	.337	-0.313	-0 347	9366	2005	-0.342	-0.382	-0.436	0.503	7.09.5	-0.744	-0.795	0.831	170.0	-0.729	-0.364	-D 343		-0.312	-0.273	
Stati	.300					1	ı	1		1	-	ı			-	ı	1			ı	
	.226	-0.306	-0.334	10321	1000	-0.009	-0.029	-0.063	167	/01.0	-0.197	-0.227	-0.253		-0.2/4	-0.319	-0.330	7020	\$	-0.265	
	.153	-0.200	-0.216	0.199	200	0.000	-0.008	-0.040	790,0		√.II./	-0.141	-0.157	12.0	471.74	-0.198	-0.213	1000	0.401	-0.180	
	M	0.599	0.700	0.801	030	1.230	1.201	1.149	0.950	200	0.920	0.899	0.873	0.000	0.632	0.801	0.701	0,603	COOLO	0.400	

Table 4. Continued

(b) Concluded

				Sta	tic pressure c	oefficients of	Static pressure coefficients on nozzle sidewall at centerline	wall at center	line			
					L	with values	with values of x/l of-					
7	153	966	300	.337	.411	.484	.558	.632	.705	622.	.853	.926
0 700	2000	0120	0 480	0.310	-0.177	-0.099	-0.045	-0.002	0.043	0.085	0.131	0.181
0.599	-0.207	0.243	0.467	0.340	0.185	104	-0.045	0.002	0.049	0.091	0.135	0.183
0.700	-0.222	0.343	-0.300	0.375	0.187	1119	10.054	-0.031	0.003	0.033	0.071	0.114
0.801	-0.20/	-0.330	-0.934	275.0	0.107	0 320	0.087	-0.254	-0.236	-0.208	-0.135	-0.044
1.250	0.006	-0.015	-0.328	-0.341	0.225	0.354	0.311	182 07	-0.255	-0.197	-0.120	-0.052
1.201	-0.010	-0.032	-0.372	9/5/0	C/C:0	10.50	0.300	200	7500	0010	0.10	-0.056
1 149	170.07	0.070	-0.427	-0.438	-0.429	-0.392	-0.322	767.0-	0.270	27.17	0.120	20.0
0200	0000	177	0 690	-0 695	-0.664	-0.278	0.157	-0.130	-0.113	-0.101	-0.0/9	-0.033
0.930	-0.070	1,1,0	2000	77.0	0.657	0 188	-0.117	-0.097	-0.086	-0.074	-0.050	-0.017
0.926	-0.123	-0.204	-0.73	7.7	1000	001.0		1000	0.066	0.048	-0.001	0.017
0 800	-0.145	-0.233	-0.801	-0.796	-0.331	-0.140	-0.0y4	-0.001	-0.000	010.0	170.0	2700
0.073	0 163	6960	-0.855	-0.844	-0.230	-0.113	-0.085	-0.066	-0.045	-0.024	0.010	0.047
0.073	0.100	707.0	0000	20807	-0 192	-0.113	-0.080	-0.056	-0.032	-0.003	0.027	0.068
0.852	11.17	-0.207	0.004	200.0	7010	0 113	-0 0K4	-0.030	0.003	0.033	0.071	0.114
0.801	-0.208	-0.332	-0.938	0.270	70.10	C11.0		2000	0700	0.00	0.137	0.179
0.701	-0.218	-0.339	-0.557	-0.336	-0.182	-0.102	-C-C-C-C-C-C-C-C-C-C-C-C-C-C-C-C-C-C-C	0.00	0.01	0.071	12.0	01.10
0,603	0000	0 310	-0.488	-0.307	-0.173	-0.101	-0.045	-0.001	0.044	0.086	0.132	0.1/8
0.00	0.187	0.270	-0.422	-0.268	-0.155	-0.092	-0.043	-0.001	0.038	0.076	0.119	0.165
0.400	701.7	7.4.7		22.0								

	Γ	7	٦		П	Т		Ī	٦	Ī			\neg	T		T	
	700	076:	1	1	1	'	ı	'	l	1	1	١	1	1	ı	_	'
0.75	305	c0/.	0.047	0.051	0.005	-0.261	-0.260	-0.251	-0.125	-0.101	-0.077	-0.051	-0.035	0.007	0.054	0.047	0.041
/all at <i>z/Z</i> = -	22.5	.558	-0.049	-0.047	690.0-	-0.289	-0.324	-0.344	-0.183	-0.154	-0.119	-0.100	-0.091	890:0-	-0.045	-0.047	-0.046
Static pressure coefficients on nozzle sidewall at $z/Z = -0.75$ with values of x/I of—		.411	-	ļ	_	_		1	1	1		1	1	ı	1	1	-
efficients on with values		.337	1	-	1	1	1	1	1	1	1	1	1		1		1
c pressure co		.300	-0.493	-0.572	-0.948	-0.336	-0.382	-0.436	-0.696	-0.750	-0.806	-0.860	-0.908	-0.937	-0.567	-0.493	-0.421
Stati		.226	-0.288	-0.317	-0.301	-0.004	-0.029	-0.059	-0.158	-0.184	-0.214	-0.239	-0.262	-0.303	-0.313	-0.287	-0.254
		.153	70107	900	-0.193	0.008	1100	140.04	-0.092	-0.117	0.136	0.155	691.0	-0 103	-0.206	194	168
		M	005 0	0.00	0.801	1 250	1 201	1 140	0800	9000	0.000	0.623	0.852	0.801	0.00	0.603	0.400

Table 4. Continued

(c) Static pressure coefficients on nozzle bottom flap

		.926	0.203	0 202	0.122	-0.062	-0.079	-0.085	0.070	0.00	0.040	010.0	0.031	0.059	0.123	0 100	0.201	0.192	- /
		.853	0.159	0.164	0.081	-0.103	-0.112	-0.119	6113	7800	0.000	00.0-	-0.012	0.015	0.082	2910	0 150	0.146	,
0.875		622		i	1	,	ı	,	 -						1	1	†- 		
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.875$.705	0.076	0.086	0.018	-0.218	-0.184	-0.184	0.170	0 154	0.122	771.0	-0.0e3	-0.054	0.021	0.088	0.076	0.069	-
zzle bottom	—Jo <i>I/x</i> Jo	.558	-0.020	-0.016	-0.068	-0.312	-0.340	-0.353	-0.229	1170	181	0 163	70.105	-0.137	-0.064	-0.012	-0.018	-0.018	
icients on no	with values of x/l of-	.411	1	ı	1	ı	1	ı						-	_	1		1	
ressure coeff		.337	1	ı	ı	1	1	-	1	1	† 			'	ı	ı	1	1	
Static p		.300	-0.766	-0.940	-1.050	-0.357	-0.398	-0.456	-0.732	-0.774	-0.807	-0.842	0.00	-0.063	-1.036	-0.922	-0.764	-0.647	
		.226	I	I	ł		-	1	1	ı	,	,		1	-	1	1	ı	
		.133	-0.210	-0.221	-0.192	0.008	-0.010	-0.035	-0.088	-0.112	-0.134	-0.150	5 166	201.00	-0.193	-0.219	-0.210	-0.189	
	•	M_{∞}	0.599	0.700	0.801	1.250	1.201	1.149	0.950	0.926	668'0	0.873	0.852	70.00	0.801	0.701	0.603	0.400	

	_	_	_	_	_	_			_	_			_	_					
	.926									-	ı					'		 	ı
	.853								-	1	1	1				1	1	!	1
= 0.50	677.		0 140	0 150	9000	0.020	0.150	201.0	24.100	14.14.	-0.124	-0.098	500	080	0.032	0110	0.140	00.130	U.139
i flap at y/Y =	.705		0 106	0.112	000	0310	51.74	0.10	0 176	27.0	-0.133	-0.130	880	-0.077	7000	0 111	18	200	0.097
ozzle botton of x/l of—	.558		-0.007	0.002	2010	-0.408	20.258	25.0	0.247	0.010	-0.213	-0.197	-0.177	-0.157	50102	0000	2005	2100	20.01
fficients on nozzle botto with values of x/l of—	.411		-0.208	-0.199	-0.257	-0.498	-0.545	10,604	0.351	700.0	10.27	-0.266	-0.264	-0.261	-0.260	961 0-	2020	0 107	7,71
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.50$ with values of x/l of—	.337		-0.517	-0.533	-0.411	-0.515	-0.570	-0.633	-0 572	0.415	CI+:O	-0.356	-0.350	-0.351	-0.423	-0.520	-0.505	J 458	OCT.O
Static	.300		-0.962	-1.323	-0.921	-0.371	-0.415	-0.473	-0.749	-0.753	55.0	-0.729	-0.745	-0.771	-0.920	-1.264	-0.947	-0.786	22/12
	.226		-0.433	-0.440	-0.342	-0.012	-0.032	-0.064	-0.177	-0.207		-0.237	-0.265	-0.291	-0.341	-0.439	-0.431	-0.391	
	.153		-0.279	-0.279	-0.224	-0.002	-0.020	-0.043	-0.107	-0.132	7.0	-0.154	-0.173	-0.191	-0.222	-0.278	-0.276	-0.255	
,	M∞		0.599	0.700	0.801	1.250	1.201	1.149	0.950	0.926	0000	0.899	0.873	0.852	0.801	0.701	0.603	0.400	

Table 4. Concluded

(c) Concluded

		Static	pressure coe	efficients on 1	Static pressure coefficients on nozzle bottom flap at centerline	flap at cente	erline	
				with values of x/l of-	—IO 1/X IO			
M	.153	.226	.300	.337	.411	.558	.705	.926
005 0	7070	_0 443	-0.958	-0.531	-0.235	-0.016	0.103	0.235
0.700	797	-0.454	-1.287	-0.556	-0.227	-0.005	0.110	0.223
0.700	-0.232	-0.352	-1.000	-0.438	-0.235	-0.095	-0.005	0.094
1 250	5001	-0.021	-0.371	-0.502	-0.491	-0.269	-0.172	-0.095
1 201	1000	-0.043	-0.418	-0.558	-0.538	-0.251	-0.185	-0.107
1.140	0.047	-0.074	-0.472	-0.616	-0.598	-0.256	-0.207	-0.118
0.050	2117	-0.194	-0.744	-0.490	-0.326	-0.245	-0.190	-0.098
9000	-0.130	-0.219	-0.735	-0.395	-0.281	-0.210	-0.158	-0.063
0.220	0 160	-0.246	-0.736	-0.358	-0.262	-0.193	-0.130	-0.030
0.623	0.180	0770	-0.754	-0.352	-0.252	-0.169	-0.101	900.0
0.852	2 2	-0.294	-0.796	-0.362	-0.254	-0.153	-0.077	0.031
0.00	0 230	-0.350	-0.959	-0.429	-0.242	860.0-	-0.008	0.091
102.0	0 204	-0.450	-1.287	-0.553	-0.224	-0.003	0.110	0.218
0.00	-0.202	-0 442	-0.975	-0.531	-0.232	-0.015	0.103	0.228
0.00	-0.272	-0.398	-0.815	-0.476	-0.221	-0.025	0.091	0.221

(d) Force data

C_{Df}	0.0128	0.0125	0.0122	0.0114	0.0115	0.0116	0.0120	0.0120	0.0121	0.0122	0.0122	0.0123	0.0126	0.0129	0.0137
$C_{D,p}$	0.0449	0.0564	0.1110	0.2204	0.2403	0.2666	0.2247	0.1965	0.1726	0.1516	0.1401	0.1100	0.0546	0.0444	0.0383
$a_{\mathcal{O}}$	0.0383	0.0496	0.1052	0.2298	0.2473	0.2676	0.2232	0.1945	0.1717	0.1497	0.1350	9660'0	0.0488	0.0382	0.0321
М∞	0.599	0.700	0.801	1.250	1.201	1.149	0.950	0.926	0.899	0.873	0.852	0.801	0.701	0.603	0.400

Table 5. Pressure and Force Data for Nozzle 3 With $\beta_{t,top/bot} = \beta_{t,side} = 16.4^{\circ}$, Plume On, and $\alpha = 0^{\circ}$

(a) Static pressure coefficients on nozzle top flap

	_	_	_	_	_	~	_	_	_	_			
	926	7,00	0 196	0.082	-0.089	-0.052	-0.024	0.005	0.034	0.075	0 180	0 2 2 0	0.218
	853	0.201	0.177	0.049	-0.129	-0.093	-0.063	-0.032	-0.003	0.042	0.172	0.195	0.189
	97.1	0.166	0.153	0.022	-0.155	-0.126	-0.098	-0.065	-0.036	0.013	0.148	0.164	0.155
line	705	0.123	0.120	-0.007	-0.181	-0.153	-0.130	-0.100	-0.069	-0.016	0.116	0.123	0.111
Static pressure coefficients on nozzle top flap at centerline	.632	0.075	0.078	-0.037	-0.198	-0.174	-0.156	-0.128	-0.098	-0.046	0.075	0.073	0.063
n nozzle top	.484 .558	0.010	0.022	-0.075	-0.213	-0.192	-0.182	-0.160	-0.133	-0.083	0.019	0.009	0.002
coefficients	.484	-0.076	-0.062	-0.120	-0.240	-0.212	-0.206	-0.191	-0.171	-0.131	-0.063	-0.078	-0.083
itic pressure	114.	-0.208	-0.196	-0.198	-0.289	-0.251	-0.239	-0.230	-0.220	-0.204	-0.197	-0.211	-0.204
Stz	.337	-0.507	-0.529	-0.361	-0.447	-0.351	-0.329	-0.313	-0.314	-0.352	-0.520	-0.505	-0.456
	.300	-1.065	-1.342	-0.873	-0.737	869:0-	-0.677	089.0-	-0.717	-0.850	-1.317	-1.048	-0.864
	.226	-0.424	-0.420	-0.316	-0.154	-0.181	-0.210	-0.242	-0.269	-0.318	-0.418	-0.426	-0.383
	.153	-0.281	-0.273	-0.211	-0.093	-0.116	-0.138	-0.160	-0.180	-0.213	-0.276	-0.282	-0.258
	M	0.602	0.703	0.797	0.952	0.926	0.904	0.875	0.847	0.800	0.702	0.600	0.403

	_	_	_	_	_	_	_	_	_	_		_	
	.926	0.225	0.198	0.080	-0.095	-0.057	-0 028	0000	0.033	0.074	0.192	0.220	0.218
	.853	0.198	0.178	0.048	-0.138	-0.101	-0.071	-0.036	-0.005	0.042	0.174	0.194	0.191
0.50	<i>ett</i> .	0.165	0.154	0.020	-0.165	-0.133	-0.104	-0.071	-0.038	0.012	0.149	0.162	0.156
Static pressure coefficients on nozzle top flap at $y/Y = 0.50$ with values of x/l of—	.705	0.123	0.118	-0.009	-0.191	-0.163	-0.137	-0.106	-0.072	-0.015	0.118	0.121	0.113
fficients on nozzle top with values of x/l of—	.558	0.012	0.021	-0.079	-0.234	-0.211	-0.194	-0.169	-0.140	-0.087	0.019	0.014	0.008
oefficients o	.411	-0.192	-0.186	-0.215	-0.336	-0.294	-0.275	-0.258	-0.247	-0.222	-0.187	-0.193	-0.187
ic pressure c	.337	1	-	ı	-	1		1	1	1	1	ļ	
Stat	.300	-1.050	-1.350	-0.892	-0.748	-0.770	-0.762	-0.754	-0.777	-0.877	-1.329	-1.036	-0.850
	.226	-0.398	-0.393	-0.300	-0.146	-0.173	-0.202	-0.229	-0.257	-0.303	-0.396	-0.398	-0.356
	.153	-0.258	-0.253	-0.199	-0.088	-0.114	-0.134	-0.155	-0.174	-0.202	-0.257	-0.259	-0.237
	M∞	0.602	0.703	0.797	0.952	0.926	0.904	0.875	0.847	0.800	0.702	0.600	0.403

Table 5. Continued

(a) Concluded

			Stat	ic pressure c	Static pressure coefficients on nozzle top flap at $y/Y = 0.75$	n nozzle top f	$\int a dx = \int dx dx = \int dx dx$	0.75		
					with values	with values of 377 of—				
M	.153	.226	.300	.337	.411	.558	.705	.779	.853	.926
0,602	-0.229	-0.351	-0.969	-0.438	-0.167	0.020	0.120	0.155	0.192	0.223
0.203	-0.233	-0.360	-1.298	-0.460	-0.167	0.025	0.118	0.149	0.178	0.200
0.707	1010	-0.287	-0.977	-0.425	-0.219	-0.073	-0.003	0.024	0.058	0.093
0.057	9800	0 138	0.750	-0.682	-0.360	-0.237	-0.193	-0.168	-0.129	-0.084
0.006	0.000	001.0	-0.792	-0.491	-0.321	-0.222	-0.163	-0.131	-0.087	-0.040
0.220	0.10	0 104	518	-0.432	-0.295	-0.200	-0.138	-0.100	-0.060	-0.016
0.30	0 140	0.220	5180	-0 303	-0.272	-0.171	-0.100	-0.064	-0.024	0.014
0.073	0.147	0.220	0.010	306	10.258	-0.142	-0.068	-0.030	0.00	0.047
0.847	-0.10/	0.240	2000	0.272	7000	1800	1100	0.018	0.052	0.089
0.800	7.174	-0.209	0.240	0.450	177.0	0.003	0 116	0.145	0.172	0.194
0.705	-0.234	-0.363	7/7:1-	-0.439	70.10	0.023	0.110	C+1.0		
0.600	-0.229	-0.354	-0.962	-0.438	-0.168	0.019	0.116	0.153	0.188	0.217
0.403	-0.206	-0.316	-0.790	-0.391	-0.155	0.021	0.109	0.143	0.179	0.210
201.00	20112									

				_		_			_					
	.926	0.217	0.200	0.100	-0.085	-0.039	-0.014	0.020	0.052	0.094	0.195	0.212	0.204	
	.853	0.187	0.178	0.070	-0.119	-0.078	-0.049	-0.013	0.019	0.065	0.173	0.184	0.177	
875	622	0.153	0.150	0.037	-0.159	-0.117	-0.089	-0.053	-0.019	0.032	0.147	0.151	0.143	
up at y/Y = 0.	705	0.116	0.117	0.007	-0.188	-0.157	-0.126	-0.091	-0.055	0.001	0.114	0.112	0.106	
nozzle top fla of x/l of—	.558	0.019	0.023	990:0-	-0.240	-0.226	-0.199	-0.168	-0.136	-0.072	0.021	0.019	0.015	
fficients on nozzle top with values of x/l of—	.411	-0.152	-0.156	-0.215	-0.367	-0.331	-0.303	-0.281	-0.265	-0.222	-0.159	-0.153	-0.138	
Static pressure coefficients on nozzle top flap at $y/Y = 0.875$ with values of x/I of—	.337	-0.402	-0.426	-0.457	-0.731	-0.536	-0.462	-0.426	-0.427	-0.456	-0.428	-0.402	-0.356	
Static	300	-0.884	-1.143	-1.047	-0.736	-0.789	9830	C98 0	668 0	-1 024	-1 126	-0.878 -0.878	-0.730	
	.226	-0315	-0.333	-0.276	-0.129	1910	0.185	0.13	0.210	0.276	-0 335	7150	-0.281	- 32
	153	902.07	-0.218	9810	280	20107	0.106	0.145	161	184	0120	0.210	188	221.0
	<u> </u>	2090	0.703	0.707	T	T	0.720	0.304	0.6/3	10.0	0.900	0.702	0.000	32.5

Table 5. Continued

(b) Static pressure coefficients on nozzle sidewall

		_		_	_	_		_	_	_	_	-	
	.926	0.204	0.199	0.127	-0.015	0.013	0.028	0.054	0.082	0.121	0.193	0.197	0.194
	.853	0.180	0.177	0.102	-0.058	-0.024	900'0-	610'0	0.051	0.094	0.172	0.175	0.170
0.75	671.	0.150	0.152	0.078	-0.097	-0.059	-0.040	-0.012	0.021	690'0	0.147	0.146	0.140
wall at $z/Z = 0$.705	0.116	0.120	0.049	-0.140	-0.095	-0.075	-0.047	-0.012	0.041	0.117	0.115	0.106
fficients on nozzle sidewith values of x/l of—	.558	0.028	0.031	-0.028	-0.218	-0.193	-0.170	-0.138	-0.102	-0.032	0.030	0.026	0.029
Static pressure coefficients on nozzle sidewall at $z/Z = 0.75$ with values of x/I of—	.411	-0.142	-0.143	-0.186	-0.513	-0.368	-0.330	-0.294	-0.260	-0.192	-0.147	-0.142	-0.129
tic pressure c	.337	-0.383	-0.405	-0.501	-0.874	-0.900	-0.751	-0.578	-0.537	-0.506	-0.407	-0.381	-0.336
Sta	.300	-0.740	-0.894	-1.071	-0.734	-0.784	-0.838	-0.899	-0.964	-1.062	-0.894	-0.735	-0.623
	.226	-0.321	-0.342	-0.289	-0.138	-0.166	-0.193	-0.220	-0.249	-0.290	-0.342	-0.321	-0.284
	.153	-0.207	-0.217	-0.188	-0.084	-0.109	-0.128	-0.147	-0.165	-0.189	-0.219	-0.210	-0.186
	M_{∞}	0.602	0.703	0.797	0.952	0.926	0.904	0.875	0.847	0.800	0.702	0.600	0.403

			_	_			_	,	_	_			_
	926	0.203	0.199	0.131	0.007	0.026	0.034	0.058	0.087	0.124	0.195	0.199	0.197
	.853	0.180	0.179	0.104	-0.036	-0.013	-0.001	0.024	0.054	960'0	0.174	0.177	0.172
.50	677.			ŀ	ı	ı	ı	1	1	ı	ı	1	1
vall at $z/Z = 0$.705	0.116	0.123	0.049	-0.106	-0.079	-0.072	-0.050	-0.016	0.041	0.115	0.116	0.108
nozzle sidev of x/I of—	.558	1	_	-	-	-	_	_	1	ı			1
Static pressure coefficients on nozzle sidewall at $z/Z = 0.50$ with values of x/l of—	.411	-0.149	-0.149	-0.210	-0.639	-0.419	-0.360	-0.310	-0.282	-0.217	-0.151	-0.149	-0.141
tic pressure co	.337	-0.408	-0.427	-0.523	-0.924	-0.941	-0.697	-0.546	-0.515	-0.521	-0.427	-0.406	-0.363
Stat	.300	-0.783	-0.956	-1.077	-0.747	-0.800	-0.852	-0.904	-0.956	-1.049	-0.950	-0.777	-0.656
	.226	-0.351	-0.369	-0.307	-0.150	-0.179	-0.204	-0.233	-0.265	-0.308	-0.373	-0.351	-0.315
	.153	-0.220	-0.228	-0.192	-0.088	-0.111	-0.131	-0.149	-0.170	-0.195	-0.230	-0.221	-0.201
	M∞	0.602	0.703	0.797	0.952	0.926	0.904	0.875	0.847	0.800	0.702	0.600	0.403

Table 5. Continued

(b) Concluded

							-	11 - 11				
				Stat	ic pressure c	oefficients on nozzle sid	Static pressure coefficients on nozzle sidewall at centerline static pressure coefficients of v/l of—	vail at center	2			
						Will value	10 1/4 10	3	205	770	853	926
74	153	226	300	.337	.411	.484	.558	.032	co/.		CCO.	
<i>∞</i> ′′′			000	0170	0.153	0.043	0.030	0.079	0.120	0.152	0.178	0.200
0.602	-0.233	-0.371	-0.820	-0.410	0.155	6500	0.035	0.084	0 124	0.152	0.177	0.199
0.703	-0.241	-0.388	-1.020	-0.430	-0.133	-0.03/	0.033	100.0	0700	8200	0.105	0.132
707.0	0 203	-0.316	-1.015	-0.481	-0.234	-0.116	-0.043	0.007	0.049	0.070	0.100	7100
0.77	603.0	73.0	0.760	0.005	70,668	-0.320	-0.211	-0.140	-0.094	-0.001	-0.023	0.014
0.952	-0.092	-0:130	-0.703	0.22	2000	9000	0010	-0 128	-0.081	-0.045	-0.011	0.032
0.926	-0.117	-0.185	-0.820	-0.903	10.434	-0.270		1010	0000	0.030	7001	0.035
. 60	261.0	0.213	70.866	592	-0.365	-0.274	-0.197	-0.131	70.00	, (CO:)	200	
0.904	-0.133	-0.413	0.000	027	0 2 10	0.223	0 161	2010	-0.053	-0.015	0.022	0.057
0.875	-0.156	-0.239	-0.871	-0.478	-0.519	2.600		0 00	0.018	0.018	0.055	0.087
0.847	-0 176	-0.273	-0.883	-0.450	-0.294	-0.200	-0.124	-0.000	010.0	0.00	1010	0 1 20
0.01	200		000	0.477	070 0-	-0.124	-0.052	0.005	0.040	0.072	0.101	0.127
0.800	-0.204	-0.317	-0.330	11.0	21.7		0000	6000	0110	0.150	0.175	0.194
0.707	-0 242	-0.392	-1.007	-0.431	-0.152	-0.038	0.032	7000	211.0		01.10	0 107
70/-0		0.770	0.013	0.417	-0 154	-0.043	0.028	0.078	0.117	0.149	0.170	0.17
0.000	-0.730	-0.372	C10.0-	1		1700	\$00.0	0.074	0110	0.142	0.170	0.194
0 403	0.214	-0.336	9890	-0.373	-0.145	-0.041	0.023	10.0	211:5			
1	1.1.1	, ,										

.153 .226 .300 -0.209 -0.3150.217 -0.3380.191 -0.2890.086 -0.1420.110 -0.1700.127 -0.1950.146 -0.2230.167 -0.2290.195 -0.2900.205 -0.315 -			Statio	c pressure co	Static pressure coefficients on nozzle sidewall at $z/z = -0.13$ with values of x/l of—	nozzie sidew of <i>x/l</i> of—	/aii at 2/2 = -	0.13	
-0.209 -0.315 - -0.372 - 0.024 -0.217 -0.338 - -0.398 - 0.029 -0.191 -0.289 - -0.041 -0.086 -0.142 - -0.909 - -0.043 -0.110 -0.170 - -0.914 - -0.189 -0.127 -0.195 - -0.702 - -0.189 -0.146 -0.233 - -0.538 - -0.146 -0.167 -0.249 - -0.146 - -0.146 -0.167 -0.299 - -0.496 - -0.146 -0.167 -0.299 - -0.497 - -0.047 -0.299 - -0.394 - -0.027 -0.205 - -0.315 - -0.373 - -0.024 -0.205 - -0.377 - - -0.024 - -	*	153	226	300	.337	.411	.558	.705	.926
-0.209 -0.315 - -0.372 - 0.024 -0.217 -0.338 - -0.398 - 0.029 -0.191 -0.289 - -0.504 - -0.041 -0.086 -0.142 - -0.909 - -0.203 -0.110 -0.170 - -0.914 - -0.189 -0.127 -0.195 - -0.702 - -0.146 -0.146 -0.223 - -0.538 - -0.146 -0.167 -0.249 - -0.146 - -0.146 -0.167 -0.249 - -0.146 - -0.146 -0.167 -0.299 - -0.496 - -0.047 -0.195 -0.290 - -0.047 - -0.047 -0.219 -0.315 - -0.373 - -0.023 -0.205 -0.315 - -0.327 - -0.024	<i>∞ INI</i> ∞	551.	2				7000	0.116	0.204
-0.217 -0.338 - -0.398 - 0.029 -0.191 -0.289 - -0.504 - -0.041 -0.086 -0.142 - -0.909 - -0.203 -0.110 -0.170 - -0.914 - -0.189 -0.127 -0.195 - -0.702 - -0.189 -0.146 -0.223 - -0.146 - -0.167 -0.249 - -0.146 - -0.167 -0.299 - -0.146 - -0.167 -0.249 - -0.146 - -0.155 -0.299 - -0.146 - -0.195 -0.299 - -0.047 - -0.047 -0.219 -0.315 - -0.373 - -0.024 -0.183 - -0.377 - -0.024 -	0.602	-0.209	-0.315	1	-0.372	ı	0.024	0.110	0.50
-0.191 -0.289 - -0.504 - -0.041 -0.086 -0.142 - -0.909 - -0.203 - -0.110 -0.170 - -0.914 - -0.189 - -0.127 -0.195 - -0.702 - -0.189 - -0.146 -0.223 - -0.146 - -0.146 - -0.167 -0.249 - -0.496 - -0.146 -0.195 -0.290 - -0.497 - -0.047 -0.195 -0.399 - -0.047 - -0.047 -0.219 -0.339 - -0.394 - -0.027 -0.255 -0.315 - -0.373 - -0.024 -0.373 - -0.327 - - -0.024	0.703	-0.217	-0.338	1	-0.398	ı	0.029	0.120	0.199
-0.086 -0.142 -0.909 -0.203 -0.203 -0.108 -0.170 -0.914 -0.189 -0.189 -0.127 -0.195 -0.702 -0.189 -0.176 -0.146 -0.223 -0.146 -0.146 -0.146 -0.167 -0.249 -0.146 -0.117 -0.117 -0.195 -0.290 -0.497 -0.047 -0.195 -0.339 -0.394 -0.027 -0.205 -0.315 -0.373 -0.023 -0.205 -0.315 -0.327 -0.024	0.70	1010	0 280		40.504	ı	-0.041	0.050	0.136
-0.100 -0.132 -0.189 -0.189 -0.110 -0.170 -0.914 -0.189 -0.127 -0.195 -0.702 -0.176 -0.146 -0.223 -0.146 -0.146 -0.167 -0.249 -0.146 -0.117 -0.195 -0.290 -0.497 -0.047 -0.195 -0.339 -0.394 -0.0027 -0.205 -0.315 -0.373 -0.023 -0.183 -0.373 -0.024	0.797	0.002	0.142		606 0	1	-0.203	-0.106	900.0
-0.110 -0.170 - -0.127 -0.195 - -0.702 - -0.146 -0.223 - -0.538 - -0.146 -0.167 -0.249 - -0.496 - -0.117 -0.195 -0.290 - -0.497 - -0.047 -0.219 -0.339 - -0.394 - 0.027 -0.205 -0.315 - -0.373 - 0.023 -0.318 - -0.327 - 0.024	0.952	0.000	-0.142		0.017		-0.189	-0.098	0.020
-0.127 -0.195 - -0.702 - -0.170 -0.146 -0.223 - -0.538 - -0.146 -0.167 -0.249 - -0.496 - -0.117 -0.195 -0.290 - -0.497 - -0.047 -0.219 -0.339 - -0.394 - 0.027 -0.205 -0.315 - -0.373 - 0.023 0.183 - -0.373 - 0.024	0.926	-0.110	-0.170	_	11,7.7		2610	7200	0.031
-0.146 -0.223 - -0.538 - -0.146 - -0.167 -0.249 - -0.496 - -0.117 - -0.195 -0.290 - -0.497 - -0.047 -0.219 -0.339 - -0.394 - 0.027 -0.205 -0.315 - -0.373 - 0.023 0.183 - -0.377 - 0.024	0 000	7010	-0.195	ı	-0.702	ı	-U.1/0	-0.077	10.0
-0.167 -0.249 - -0.496 - -0.117 - -0.195 -0.290 - -0.497 - -0.047 -0.19 -0.290 - -0.497 - -0.047 -0.219 -0.339 - -0.394 - 0.027 -0.205 -0.315 - -0.373 - 0.023 -0.183 - -0.327 - 0.024	250	0 146	0.223		-0.538	1	-0.146	-0.051	0.055
-0.16/ -0.249 - -0.497 - -0.047 -0.195 -0.290 - -0.497 - -0.047 -0.219 -0.339 - -0.394 - 0.027 -0.205 -0.315 - -0.373 - 0.023 -0.183 - -0.377 - 0.024	0.875	0.140	0.245		7070		-0.117	-0.016	0.087
-0.195 -0.290 - -0.497 - -0.047 -0.219 -0.339 - -0.394 - 0.027 -0.205 -0.315 - -0.373 - 0.023 0.183 - 0.779 - -0.327 - 0.024	0.847	-0.10/	-0.243	<u>'</u>	201.0		7700	7700	0 1 1 0
-0.219 -0.339 - -0.394 - 0.027 -0.205 -0.315 - -0.373 - 0.023 0.183 - 0.779 - -0.327 - 0.024	0 800	-0.195	-0.290	1	-0.49/	_	15.5	5	(21.5)
-0.205 -0.3150.373 - 0.023 0.183 -0.3790.327 - 0.024	202.0	0.210	0330		-0.394	1	0.027	0.116	0.192
0.183 -0.3790.327 - 0.024	0.702	-0.417	7:00		0 273		0.003	0.115	0.198
0.183 -0.790.327 - 0.024	0.00	-0.205	-0.515		C/C:D			20.0	701.0
	0.403	-0.183	-0.279	I	-0.327	ı	0.024	0.10/	0.154

Table 5. Continued

(c) Static pressure coefficients on nozzle bottom flap

		200	076.	0160	17.5	0.217	0.140		-0.027	7000	0.020	-0.003	0000	0.029	0.069	25.0	0.133	0 212	7,7	0.215	0000	7.507
		050	cco.	0 188		0.190	0.114	2500	7/0.0	7900	1	- 0.042	900	-U.U08	0.034	301.0	0.100	0.186		0.184	0.175	
= 0.875		770	(11:	0.152	0 150	0.1.70	0.084	0 113	7117	-0.107		-0.081	0.045	-0.0 1	0000	0.075	2,0,0	0.155	0.5	0.150	0.146	
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.875$		705		0.116	0 131	171.5	0.050	5710	1	-0.146		١٠.١٠/	20.02	700.0	-0.036	0.044		0.117	2110	0.113	0.107	
nozzle botton	with values of x/l of—	.558		0.020	0.005	2010	-0.037	10.217	12.5	707.0	0 100	70.103	951.0		-0.119	-0.046		0.023	0.017	7.0.0	0.016	
fficients on	with value	4.		-0.144	-0.146	2000	-0.203	-0.405	202.0	4.303	0000	707.0	-0.263	0.000	-0.22 <i>t</i>	-0.211	9710	-0.149	D 144		-0.129	
pressure coe	1	.337	0.363	-0.303	-0.390	0.502	2000	-0.799	2750	0.7+0	-0.472		-0.442	0.466	-0.403	-0.507	0 300	-0.300	-0.362	1000	-0.321	
Static	300	ر ان	0 733	0.733	-0.888	-1 085		-0.774	618 0	710.0	-0.838		-0.85/	0100	0.717	-1.059	0880	0.000	-0.730	0.510	10.019	
	700	077	-0 340	2 3	-0.365	-0.309		-0.133	-0.183		-0.211	0,00	-0.238	7920	200	-0.309	-0.367	1000	-0.340	0 200	0000	
	153	CCI.	-0.214		-0.223	0.194	0.007	10.00	-0-		-0.132	0 150	20.1.50	-0.168	701.0	77.170	-0.227	200	-0.213	001 0		
	¥	8	0.602	201.0	0.703	0.797	0.050	202.0	0.926	300	0.904	0.875	2/0.0	0.847	0.800	0000	0.702	000	0.00	0.403		

Г	_	Τ	٦		Τ	٦	_	Τ		Γ	Т	_	T	7	_	T		Т	٦	-	Т
		700	076.	1			ı		1	i		ı		1	1		1			ı	
		852	cco.	0.196	2010	0.130	0.107	5.50	-0.072	7900		0.043		10.01	0.029		0.096	0 100	0.192	0.194	
= 0.50		779		0.162	7710	5 5	0.075	0110	27.11.0	-0.102		080.7	7700	0.01	-0004	1,00	0.00	0.161	0.101	0.159	0.150
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.50$.705		0.121	0 127	127.0	0.039	J 146	2	-0.139	2	ر ا	780 0	0.00	-0.049	0000	0.029	0 124	171.0	0.118	0.110
nozzle bottor	with values of x/l of—	.558	2100	0.015	0.02	0000	-0.009	0.230		-0.202	0 107	6.19	166		-0.140	\$600	0.07	0.010	100	0.011	0.00
efficients on	with value	.411	0.170	0.1/0	-0.171	0.360	7.67.6	-0.375	0000	797.0-	0770	2/7:2	-0.256	6,200	-0.203	-0.250		-0.173	100	70.100	-0.167
pressure co		.337	-0.437	10.10	0.447	-0.466		-0.729	0.417	14.7	-0.373		-0.350	0.360	2000	-0.459		-44.0	-0.435		-0.391
Static	333	.300	-0.853		-1.121	-0.954	000	-0.792	0 740	2	1 -0.712		-0.694	-0.741		-0.930	1 305	-1.05	-0.849		-0.709
	75%	077:	-0.432	37.0	-0.400	-0.355	191	70.19	0170		-0.238	1000	1/7.0-	-0.303		-0.333	0.452	20.4.0	-0.433	2000	-0.383
	153	cci.	-0.269	27.0	C/7:0	-0.220	0 103	701.0	-0.125		_U.149	0 1 60	67.70	061.00	550	-0.223	-0.275	2.7.7	-0.271	0.242	-0.243
	2	8	0.602	0.703		0.797	0.952	77.75	0.926	200	0.904	0.875	C/0.0	0.847	2000	0.00	0.702		0.600	0.402	CO.+CO

Table 5. Concluded

(c) Concluded

		Static	pressure coe	fficients on nozzle botto with values of x/l of—	ozzle botton	Static pressure coefficients on nozzle bottom flap at centerline with values of x/l of—	rline	
	152	300	300	337	411	.558	.705	.926
Μ∞	661.	077.	Socie			0000	9	0,000
0 602	-0.284	-0.436	-0.872	-0.454	_	-0.002	0.112	0.242
0.703	0.00	-0.460	-1.109	-0.479	1	0.011	0.122	0.237
707.0	0.27	0 366	-1 021	-0.492	1	-0.056	0.040	0.135
0.797	0.113	0.106	922.0	-0.534		-0.230	-0.176	-0.056
0.932	-0.112	0.170	0.750	0.423		-0 107	-0.132	-0.018
0.926	-0.129	-0.222	-0.733	-0.423				1000
0 004	-0.156	-0.246	-0.740	-0.395	į	-0.175	-0.105	0.004
2000	0.177	9200	765	-0.395		-0.155	-0.073	0.031
6,00	0.1.0	0.270	0.832	0.417		-0.126	-0.036	0.065
0.84/	-0.200	210.0-	2000	10,0		0.066	0.031	0.124
0.800	-0.237	-0.369	-0.990	-0.485	_	-0.000	150.0	121.0
0.707	-0 293	-0.464	-1.094	-0.479	ı	0.007	0.119	0.230
70/0	200.0	0.430	0 860	-0.455	1	-0.004	0.110	0.234
0.000	-0.200	10.430	00.0				1010	0000
0.403	10.258	-0.388	-0.742	-0.403	1	-0.011	0.101	0.229
֚֚֚֝֝֟֝֜֜֝֜֝֜֜֝֜֜֜֝֓֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֜֜֜֜		1						

(d) Force data

											_	_
c_{Df}	0.0122	0.0119	0.0117	0.0114	0.0115	0.0115	0.0116	0.0116	0.0117	0.0120	0.0123	0.0130
$C_{D,p}$	0.0429	0.0576	0.1126	0.2512	0.2139	0.1911	0.1655	0.1457	0.1171	0.0589	0.0441	0.0352
a_{2}	0.0378	0.0454	0.1068	0.2529	0.2185	0.1895	0.1655	0.1432	0.1111	0.0473	0.0368	0.0307
M _∞	0.602	0.703	0.797	0.952	0.926	0.904	0.875	0.847	0.800	0.702	0.600	0.403
			-	_								

Table 6. Pressure and Force Data for Nozzle 3 With $\beta_{t,top/bot} = \beta_{t,side} = 16.4^{\circ}$ and Plume Off

(a) Static pressure coefficients on nozzle top flap

	200	976	0.094	161	101.0	0.150	0.161	0.159	0.154	-0.108	-0.085	-0.054	-0.070	-0.051	-0.031	-0.012	0.005	-0.022	0.003	0.048	0.165	0.141	2112	-0.102	001.09	0.116	0.130	9119
1	650	650.	2117	0.120	0.120	0.124	0.131	0.126	0.119	-0.132	-0.115	-0.087	0.108	-0.085	-0.070	-0.058	-0.050	-0.058	-0.029	0.022	0.142	0.112	-0.128	97.18	-0.127	-0.134	-0.146	51.33
	07.1	6110	7 7 7	0.103	080	0.103	0.105	0.100	0.091	-0.152	-0.142	-0.119	-0.139	-0.114	9.10	-0.097	-0.098	-0.089	-0.060	0.000	0.115	0.082	-0.141	-0.132	-0.140	-0.146	-0.158	-0 147
ine	302	0.135	51.5	0.069	0.051	0.071	0.077	0.071	0.062	-0.168	-0.162	-0.143	-0.158	-0.143	-0.139	-0.140	-0.145	-0.119	-0.090	-0.026	0.082	0.044	-0.156	-0.145	-0.160	-0.167	-0.177	-0.157
Static pressure coefficients on nozzle top flap at centerline	633	260.	0.73	0.020	-0.005	0.020	0.027	0.020	0.010	-0.180	-0.176	-0.165	-0.178	-0.163	-0.166	-0.176	-0.187	-0.142	-0.116	-0.052	0.038	0.002	-0.184	-0.166	-0.204	-0.209	-0.212	-0.178
nozzle top f	—Jo //x. Jo	70.318	-0.289	0.042	-0.071	-0.042	-0.032	-0.038	-0.051	-0.192	-0.188	-0.182	-0.196	-0.181	-0.190	-0.210	-0.226	-0.166	-0.147	-0.088	-0.021	-0.057	-0.382	-0.249	-0.378	-0.409	-0.438	-0.210
oefficients or	with values of 1/1 of-	-0.446	-0.494	-0.126	-0.162	-0.129	-0.117	-0.123	-0.139	-0.214	-0.203	-0.203	-0.215	-0.201	-0.214	-0.242	-0.263	-0.195	-0.181	-0.131	-0.106	-0.135	-0.490	-0.481	-0.492	-0.494	-0.518	-0.454
tic pressure c	411	-0.499	-0.543	-0.257	-0.299	-0.261	-0.244	-0.250	-0.270	-0.257	-0.237	-0.234	-0.249	-0.228	-0.241	-0.275	-0.300	-0.233	-0.227	-0.200	-0.241	-0.252	-0.522	-0.530	-0.537	-0.538	-0.551	-0.595
Sta	337	-0.504	-0.551	-0.550	-0.607	-0.551	-0.522	-0.527	-0.561	-0.378	-0.325	-0.314	-0.334	-0.309	-0.323	-0.366	-0.390	-0.309	-0.316	-0.342	-0.582	-0.504	-0.536	-0.536	-0.542	-0.540	-0.550	-0.594
<u>.</u>	300	-0.393	-0.433	-1.101	-1.220	-1.102	-1.034	-1.041	-1.122	-0.697	-0.662	-0.658	-0.687	-0.649	-0.664	-0.715	-0.746	-0.663	-0.698	-0.838	-1.359	-0.913	-0.420	-0.423	-0.432	-0.429	-0.430	-0.475
	.226	-0.033	-0.036	-0.458	-0.485	-0.460	-0.442	-0.436	-0.442	-0.166	-0.196	-0.223	-0.208	-0.226	-0.235	-0.238	-0.233	-0.249	-0.273	-0.327	-0.440	-0.422	-0.022	-0.024	-0.026	-0.030	-0.046	-0.039
	.153	-0.028	-0.027	-0.307	-0.320	-0.307	-0.295	-0.288	-0.288	-0.106	-0.130	-0.151	-0.139	-0.152	-0.159	-0.165	-0.169	-0.171	-0.188	-0.223	-0.293	-0.297	-0.016	-0.015	-0.011	-0.017	-0.035	-0.023
	α, deg	-0.007	0.017	-0.026	-3.007	0.030	2.997	5.992	9.003	0.036	-0.011	-0.012	-3.024	0.002	3.002	9.000	9.018	0.025	0.021	-0.018	0.002	-0.012	-3.030	0.004	2.942	6.007	9.002	0.020
	M	1.249	1.201	0.598	0.599	0.600	0.601	0.601	0.601	0.948	0.925	0.901	0.900	0.898	0.898	0.897	0.899	0.875	0.850	0.798	0.700	0.401	1.201	1.202	1.199	1.200	1.198	1.153

Table 6. Continued

(a) Continued

	9	95	5	59	19	58	62	62	8	8)	986	53	9/(151)33	117	302)24	0.002	0.046	0.164	0.141	112	102	109	-0.116	-0.132	-0.116	
!	.926	-0.095	0.113	0.159	0.161	0.158	0.162	0.162	0.160	-0.109	-0.086	-0.053	-0.076	-0.051	-0.033	-0.017	-0.002	-0.024	0.0	0.0	ö	0	-0.112	-0.102	-0.109	9	9	٩	;
	.853	-0.110	-0.129	0.134	0.130	0.134	0.138	0.137	0.134	-0.142	-0.122	-0.091	-0.117	-0.088	-0.072	-0.062	-0.053	-0.062	-0.032	0.021	0.142	0.115	-0.128	-0.118	-0.126	-0.131	-0.145	J 134	
.50	6LL:	-0.123	-0.142	0.104	0.092	0.101	0.105	0.102	0.101	-0.163	-0.151	-0.124	-0.148	-0.119	-0.109	-0.106	-0.106	-0.092	-0.063	-0.001	0.115	0.085	-0.144	-0.133	-0.141	-0.146	-0.159	0.147	7
ap at y/Y = 0	.705	-0.137	-0.159	0.068	0.051	0.067	0.072	0.070	0.070	-0.181	-0.175	-0.153	-0.173	-0.148	-0.142	-0.146	-0.151	-0.124	-0.093	-0.026	0.079	0.048	-0.162	-0.150	-0.164	-0.168	-0.176	1410	1
nozzle top f	.558	-0.390	-0.383	-0.031	-0.058	-0.030	-0.022	-0.023	-0.023	-0.213	-0.211	-0.204	-0.216	-0.199	-0.203	-0.220	-0.235	-0.177	-0.157	-0.090	-0.018	-0.048	-0.445	-0.324	-0.435	-0.477	-0.455	2220	
Static pressure coefficients on nozzle top flap at $y/Y = 0.50$ with values of y/I of—	.411	-0.484	-0.540	-0.232	-0.272	-0.235	-0.220	-0.227	-0.232	-0.290	-0.285	-0.274	-0.291	0220	-0.281	-0.315	755 0	0920	-0.254	-0.218	-0.228	-0.234	-0.514	-0.526	-0 535	955 0-	795 0-	102:0	5
c pressure co	.337		1						1	,												1		 					
Stati	300	-0 379	0.410	1086	1.00	1 003	1 047	-1 067	-1 144	-0.738	757	-0.753	787 0	0.745	0.750	0.708	0.775	0.771	0.750	-0.870	-1.367	-0.893	-0.405	0.400	0.114	0070	00,00	77.7	V77 V
	226	9000	0.020	0.02	0.454	0.434	0.416	0.400	0.420	0.150	0.187	0.15	0.00	-0.202	20.00	0.225	0.233	0.240	0.240	-0.204	-0415	70307	0000	0.020	0.021	0.027	40.050	-V.V.20	200
	153	0.003	20.0	-0.024	-0.204	0.250	0.376	0.273	0.783	0010	0.100	0.146	10.140	-0.134	0.140	0.133	0,1,0	-0.184	-0.103	0.160	-0.274	0.770	0.270	1000	-0.011	0.013	0.020	-U.U.7	
	ماده	u, uce	10.00	0.017	3.002	-3.007	0.030	2.997	3.992	9.003	0.030	10.01	2.002	-3.024	0.002	3.002	0.000	9.018	20.0	0.021	0.018	0.002	20012	-5.050	0.004	2.942	6.007	9.002	0000
	7		1.249	1.201	0.398	0.599	0.600	0.001	0.001	0.001	0.948	0.923	0.901	0.900	0.898	968.0	0.897	0.899	0.875	0.850	0.790	0.700	0.401	1.201	1.202	1.199	1.200	1.198	

Table 6. Continued

(a) Continued

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| 926 | 2000 | -0.067 | 0.100 | 0.133 | 0.133 | 0.149 | 0.155 | 0.133 | 9110 | 1800

 | 0.047 | -0.070 | 5000 | 1000

 | 0000 | 0.028 | 8100
 | 0000
 | 0.050 | 0.159
 | 0 134 | 51.0 | -0.005 | 800 0 | 0.070 | 0.120
 | |
| 853 | 201.0 | 0 175 | 0.127 | 0.127 | 0.123 | 0.123 | 0.120 | 0.123 | -0.148 | -0.122

 | -0.087 | -0.115 | -0.083 | 2900

 | -0.043 | -0.020 | -0.055
 | -0.025
 | 0.025 | 0.138
 | 0.107 | -0 122 | 1119 | -0.115 | 0710 | -0.133
 | -0.128 |
| 922 | 9110 | 0.110 | 0000 | 0.00 | 0.00 | 0.050 | 0.103 | 0.104 | -0.175 | -0.153

 | -0.122 | -0.149 | -0.117 | -0.102

 | -0.092 | -0.080 | -0.089
 | -0.061
 | 0.000 | 0.110
 | 0.078 | -0.139 | -0.126 | -0.137 | -0 139 | -0.149
 | -0.144 |
| 705 | -0.136 | 0.158 | 0.064 | 0.050 | 0000 | 0.000 | 0.00 | 0.068 | -0.194 | -0.177

 | -0.153 | -0.177 | -0.146 | -0.137

 | -0.139 | -0.142 | -0.120
 | -0.089
 | -0.024 | 0.079
 | 0.050 | -0.157 | -0.143 | -0.171 | -0.166 | -0.166
 | -0.158 |
| .558 | -0 353 | -0.382 | 2000 | -5 044 | 5000 | -0.014 | 000 | 0.004 | -0.226 | -0.226

 | -0.207 | -0.225 | -0.205 | -0.207

 | -0.226 | -0.245 | -0.180
 | -0.155
 | -0.086 | -0.013
 | -0.027 | -0.393 | -0.358 | -0.364 | -0.375 | -0.363
 | -0.288 |
| .411 | -0.470 | -0.530 | -0.205 | -0.242 | 0000 | -0.195 | -0.181 | -0.162 | -0.317 | -0.313

 | -0.297 | -0.324 | -0.295 | -0.314

 | -0.345 | -0.347 | -0.278
 | -0.264
 | -0.226 | -0.203
 | 661.0- | -0.503 | -0.512 | -0.534 | -0.545 | -0.573
 | -0.583 |
| .337 | -0.498 | -0.549 | -0.476 | -0.533 | -0.483 | -0.467 | -0.453 | -0.424 | -0.524 | -0.465

 | -0.427 | -0.480 | -0.425 | -0.448

 | -0.465 | -0.449 | -0.397
 | -0.392
 | -0.425 | -0.498
 | -0.433 | -0.541 | -0.537 | -0.556 | -0.566 | -0.580
 | -0.596 |
| .300 | -0.372 | -0.418 | -1.005 | -1.126 | -1.012 | -1.021 | -1.023 | -0.945 | -0.754 | -0.793

 | -0.813 | -0.839 | -0.810 | -0.836

 | -0.851 | -0.826 | -0.812
 | -0.822
 | -0.941 | -1.319
 | -0.836 | -0.397 | -0.402 | -0.409 | -0.420 | -0.430
 | -0.454 |
| .226 | -0.022 | -0.035 | -0.385 | -0.409 | -0.394 | -0.374 | -0.384 | -0.393 | -0.150 | -0.180

 | -0.209 | -0.196 | -0.207 | -0.222

 | -0.245 | -0.254 | -0.233
 | -0.254
 | -0.301 | -0.382
 | -0.355 | -0.019 | -0.020 | -0.029 | -0.051 | -0.072
 | -0.040 |
| .153 | -0.020 | -0.025 | -0.255 | -0.266 | -0.258 | -0.255 | -0.267 | -0.272 | -0.097 | -0.121

 | -0.141 | -0.133 | -0.141 | -0.158

 | -0.180 | -0.187 | -0.161
 | -0.175
 | -0.203 | -0.253
 | -0.240 | -0.016 | -0.013 | -0.023 | -0.045 | -0.057
 | -0.025 |
| α, deg | -0.007 | 0.017 | -0.026 | -3.007 | 0.030 | 2.997 | 5.992 | 9.003 | 0.036 | -0.011

 | -0.012 | -3.024 | 0.002 | 3.002

 | 9.000 | 9.018 | 0.025
 | 0.021
 | -0.018 | 0.002
 | -0.012 | -3.030 | 0.004 | 2.942 | 6.007 | 9.002
 | 0.020 |
| M _∞ | 1.249 | 1.201 | 0.598 | 0.599 | 0.600 | 0.601 | 0.601 | 0.601 | 0.948 | 0.925

 | 0.901 | 0.900 | 0.898 | 0.898

 | 0.897 | 0.899 | 0.875
 | 0.850
 | 0.798 | 0.700
 | 0.401 | 1.201 | 1.202 | 1.199 | 1.200 | 1.198
 | 1.153 |
| | α, deg .153 .226 .300 .337 .411 .558 .705 .779 853 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 -0.007 -0.020 -0.022 -0.372 -0.498 -0.470 -0.353 -0.116 0.116 0.106 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 -0.007 -0.020 -0.0372 -0.498 -0.470 -0.353 -0.116 -0.116 -0.100 0.017 -0.025 -0.035 -0.418 -0.549 -0.530 -0.382 -0.158 -0.116 -0.100 | α, deg .153 .226 .300 .337 411 .558 .705 .779 .853 -0.007 -0.020 -0.0372 -0.498 -0.470 -0.353 -0.136 -0.116 -0.100 -0.100 -0.017 -0.025 -0.035 -0.418 -0.539 -0.530 -0.138 -0.137 -0.125 -0.125 -0.026 -0.255 -0.385 -1.005 -0.476 -0.205 -0.02 0.064 0.000 0.137 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 -0.007 -0.002 -0.0372 -0.498 -0.470 -0.353 -0.136 -0.116 -0.100 0.017 -0.025 -0.035 -0.418 -0.549 -0.530 -0.382 -0.136 -0.116 -0.105 -0.026 -0.255 -0.385 -1.005 -0.476 -0.205 -0.022 0.064 0.099 0.127 -3.007 -0.266 -0.409 -1.126 -0.533 -0.247 -0.044 0.050 0.050 0.027 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 -0.007 -0.020 -0.0322 -0.498 -0.470 -0.353 -0.136 -0.116 -0.100 -0.017 -0.025 -0.035 -0.418 -0.549 -0.530 -0.382 -0.136 -0.116 -0.105 -0.026 -0.255 -0.385 -1.005 -0.476 -0.205 -0.022 0.064 0.099 0.127 -3.007 -0.266 -0.409 -1.126 -0.533 -0.242 -0.044 0.050 0.091 0.123 0.030 -0.258 -0.394 -1.012 -0.483 -0.704 -0.050 0.090 0.023 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 -0.007 -0.020 -0.022 -0.372 -0.498 -0.470 -0.353 -0.136 -0.116 -0.100 -0.026 -0.025 -0.035 -0.418 -0.549 -0.530 -0.382 -0.158 -0.115 -0.125 -0.026 -0.255 -0.385 -1.005 -0.476 -0.205 -0.022 0.064 0.099 0.127 -3.007 -0.266 -0.409 -1.126 -0.533 -0.242 -0.044 0.050 0.091 0.123 0.030 -0.258 -0.394 -1.012 -0.483 -0.209 -0.023 0.060 0.098 0.123 2.997 -0.255 -0.374 -1.021 -0.467 -0.195 -0.014 0.067 0.108 0.123 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 -0.007 -0.020 -0.022 -0.372 -0.498 -0.470 -0.353 -0.136 -0.116 -0.100 0.017 -0.025 -0.035 -0.418 -0.549 -0.530 -0.382 -0.158 -0.137 -0.125 -0.026 -0.255 -0.248 -0.205 -0.022 0.064 0.099 0.127 -3.007 -0.266 -0.409 -1.126 -0.533 -0.242 -0.044 0.050 0.091 0.123 0.030 -0.258 -0.394 -1.012 -0.483 -0.209 -0.023 0.060 0.098 0.123 2.997 -0.255 -0.374 -1.021 -0.467 -0.195 -0.014 0.067 0.105 0.129 5.992 -0.267 -0.384 -1.023 -0.483 -0.181 -0.064 0.069 0.106 0.129 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 -0.007 -0.020 -0.022 -0.372 -0.498 -0.470 -0.353 -0.136 -0.116 -0.100 0.017 -0.025 -0.035 -0.418 -0.549 -0.530 -0.382 -0.137 -0.125 -0.026 -0.255 -0.385 -1.005 -0.476 -0.205 -0.022 0.064 0.099 0.127 -3.007 -0.266 -0.409 -1.126 -0.533 -0.242 -0.044 0.050 0.091 0.123 0.030 -0.258 -0.394 -1.012 -0.483 -0.209 -0.023 0.060 0.098 0.123 2.997 -0.257 -0.384 -1.021 -0.467 -0.195 -0.004 0.069 0.106 0.129 9.003 -0.272 -0.393 -0.424 -0.162 0.004 0.069 0.104 0.123 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 -0.007 -0.020 -0.022 -0.372 -0.498 -0.470 -0.353 -0.136 -0.116 -0.100 0.017 -0.025 -0.035 -0.418 -0.549 -0.430 -0.136 -0.137 -0.125 -0.026 -0.255 -0.385 -1.005 -0.476 -0.205 -0.022 0.064 0.099 0.127 -3.007 -0.266 -0.409 -1.126 -0.533 -0.242 -0.044 0.050 0.091 0.123 -3.007 -0.258 -0.394 -1.012 -0.483 -0.209 -0.023 0.060 0.098 0.123 -0.297 -0.257 -0.384 -1.021 -0.467 -0.195 -0.014 0.069 0.105 0.129 -0.036 -0.272 -0.393 -0.424 -0.162 0.004 0.069 0.104 0.129 -0.036 -0.057 <td>α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 -0.007 -0.020 -0.022 -0.372 -0.498 -0.470 -0.353 -0.136 -0.116 -0.100 0.017 -0.025 -0.035 -0.418 -0.549 -0.530 -0.382 -0.137 -0.125 -0.026 -0.255 -0.385 -1.005 -0.476 -0.205 -0.022 0.064 0.099 0.127 -3.007 -0.266 -0.409 -1.126 -0.533 -0.242 -0.044 0.050 0.091 0.123 0.030 -0.258 -0.394 -1.012 -0.483 -0.209 -0.023 0.060 0.098 0.123 2.997 -0.255 -0.374 -1.021 -0.467 -0.195 -0.014 0.067 0.105 0.129 5.992 -0.267 -0.384 -1.023 -0.453 -0.181 -0.004 0.069 0.106 0.129 0.036</td> <td>α, deg.153.226.300.337.411.558.705.779.853$-0.007$$-0.020$$-0.022$$-0.372$$-0.498$$-0.470$$-0.353$$-0.136$$-0.116$$-0.100$$0.017$$-0.025$$-0.025$$-0.025$$-0.418$$-0.549$$-0.530$$-0.382$$-0.137$$-0.125$$-0.026$$-0.255$$-0.385$$-1.005$$-0.476$$-0.205$$-0.022$$-0.064$$0.099$$0.127$$-0.026$$-0.256$$-0.409$$-1.126$$-0.533$$-0.242$$-0.044$$0.050$$0.091$$0.123$$0.030$$-0.258$$-0.394$$-1.012$$-0.483$$-0.209$$-0.023$$0.060$$0.098$$0.123$$2.997$$-0.255$$-0.374$$-1.021$$-0.467$$-0.195$$-0.014$$0.067$$0.105$$0.129$$2.997$$-0.257$$-0.384$$-1.023$$-0.453$$-0.181$$-0.004$$0.069$$0.106$$0.106$$9.003$$-0.272$$-0.393$$-0.945$$-0.424$$-0.162$$0.004$$0.068$$0.104$$0.123$$-0.011$$-0.121$$-0.180$$-0.793$$-0.425$$-0.313$$-0.226$$-0.194$$-0.155$$-0.182$$-0.012$$-0.012$$-0.141$$-0.190$$-0.192$$-0.192$$-0.192$$-0.192$$-0.192$$-0.192$$-0.012$$-0.012$$-0.012$$-0.029$$-0.177$$-0.127$$-0.127$</td> <td>α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 -0.007 -0.020 -0.022 -0.372 -0.498 -0.470 -0.353 -0.136 -0.116 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color705.779.8530.007-0.020-0.022-0.438-0.470-0.353-0.136-0.116-0.1000.017-0.025-0.035-0.418-0.549-0.530-0.382-0.137-0.125-0.026-0.255-0.035-0.418-0.205-0.205-0.158-0.137-0.125-0.026-0.256-0.409-1.126-0.205-0.0240.0640.0990.127-0.030-0.258-0.394-1.126-0.483-0.209-0.0230.0990.1032.997-0.255-0.374-1.012-0.483-0.209-0.0230.0600.0980.1232.997-0.255-0.374-1.023-0.483-0.181-0.0040.0660.1050.1292.997-0.257-0.384-1.023-0.454-0.181-0.0040.0680.1060.1292.011-0.180-0.754-0.524-0.1620.0040.0680.1040.125-0.012-0.141-0.209-0.754-0.524-0.137-0.135-0.135-0.135-0.012-0.141-0.209-0.813-0.425-0.205-0.194-0.153-0.125-0.012-0.141-0.209-0.813-0.226-0.194-0.153-0.125-0.012-0.141-0.209-0.819-0.425-0.205-0.104-0.105-0.02-</td><td>α, deg .153 .226 .300 .337 411 .558 .705 .779 .853 -0.007 -0.020 -0.022 -0.372 -0.498 -0.470 -0.353 -0.136 -0.116 -0.100 0.017 -0.025 -0.037 -0.498 -0.470 -0.382 -0.158 -0.137 -0.105 0.017 -0.025 -0.035 -0.418 -0.549 -0.549 -0.250 -0.022 -0.137 -0.105 -0.004 0.015 0.017 0.030 -0.256 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/td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>a, deg .153 .226 .300 .337 will values of 150 of 170 of</td><td>a. deg .153 .226 .300 .337 .411 Values 0.710 ol. .715 .779 .853 9 -0.007 -0.020 -0.022 -0.478 -0.470 -0.335 -0.136 -0.116 -0.100 1 0.017 -0.025 -0.035 -0.418 -0.476 -0.235 -0.136 -0.137 -0.125 8 -0.026 -0.026 -0.409 -1.126 -0.439 -0.204 -0.024 -0.139 -0.139 -0.139 -0.125 -0.136 -0.137 -0.125 -0.136 -0.137 -0.125 -0.137 -0.125 -0.136 -0.137 -0.125 -0.136 -0.136 -0.137 -0.125 -0.136 -0.137 -0.125 -0.136 -0.137 -0.137 -0.125 -0.136 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.139 -0.144 -0.137 -0.144
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color705.779.8530.007-0.020-0.022-0.438-0.470-0.353-0.136-0.116-0.1000.017-0.025-0.035-0.418-0.549-0.530-0.382-0.137-0.125-0.026-0.255-0.035-0.418-0.205-0.205-0.158-0.137-0.125-0.026-0.256-0.409-1.126-0.205-0.0240.0640.0990.127-0.030-0.258-0.394-1.126-0.483-0.209-0.0230.0990.1032.997-0.255-0.374-1.012-0.483-0.209-0.0230.0600.0980.1232.997-0.255-0.374-1.023-0.483-0.181-0.0040.0660.1050.1292.997-0.257-0.384-1.023-0.454-0.181-0.0040.0680.1060.1292.011-0.180-0.754-0.524-0.1620.0040.0680.1040.125-0.012-0.141-0.209-0.754-0.524-0.137-0.135-0.135-0.135-0.012-0.141-0.209-0.813-0.425-0.205-0.194-0.153-0.125-0.012-0.141-0.209-0.813-0.226-0.194-0.153-0.125-0.012-0.141-0.209-0.819-0.425-0.205-0.104-0.105-0.02-</td> <td>α, deg .153 .226 .300 .337 411 .558 .705 .779 .853 -0.007 -0.020 -0.022 -0.372 -0.498 -0.470 -0.353 -0.136 -0.116 -0.100 0.017 -0.025 -0.037 -0.498 -0.470 -0.382 -0.158 -0.137 -0.105 0.017 -0.025 -0.035 -0.418 -0.549 -0.549 -0.250 -0.022 -0.137 -0.105 -0.004 0.015 0.017 0.030 -0.256 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-0.209 -0.024 0.060 0.098 0.123 2.997 -0.257 -0.254 -0.181 -0.044 0.060 0.096 0.106 2.997 -0.267 -0.384 -1.023 | α , deg.153.226.300.337will values of the color705.779.8530.007-0.020-0.022-0.438-0.470-0.353-0.136-0.116-0.1000.017-0.025-0.035-0.418-0.549-0.530-0.382-0.137-0.125-0.026-0.255-0.035-0.418-0.205-0.205-0.158-0.137-0.125-0.026-0.256-0.409-1.126-0.205-0.0240.0640.0990.127-0.030-0.258-0.394-1.126-0.483-0.209-0.0230.0990.1032.997-0.255-0.374-1.012-0.483-0.209-0.0230.0600.0980.1232.997-0.255-0.374-1.023-0.483-0.181-0.0040.0660.1050.1292.997-0.257-0.384-1.023-0.454-0.181-0.0040.0680.1060.1292.011-0.180-0.754-0.524-0.1620.0040.0680.1040.125-0.012-0.141-0.209-0.754-0.524-0.137-0.135-0.135-0.135-0.012-0.141-0.209-0.813-0.425-0.205-0.194-0.153-0.125-0.012-0.141-0.209-0.813-0.226-0.194-0.153-0.125-0.012-0.141-0.209-0.819-0.425-0.205-0.104-0.105-0.02- | α, deg .153 .226 .300 .337 411 .558 .705 .779 .853 -0.007 -0.020 -0.022 -0.372 -0.498 -0.470 -0.353 -0.136 -0.116 -0.100 0.017 -0.025 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-0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.139 -0.144 -0.137 -0.144 -0.144 -0.144 -0.144 -0.144</td> <td>a. deg .153 .226 .300 .337 .4111 Annes of LATO .705 .779 .853 9 -0.007 -0.022 -0.372 -0.470 -0.353 -0.156 -0.116 -0.100 9 -0.007 -0.025 -0.035 -0.418 -0.249 -0.530 -0.156 -0.116 -0.107 -0.105 9 -0.026 -0.255 -0.035 -0.476 -0.253 -0.156 -0.197 -0.125 9 -3.007 -0.266 -0.499 -1.102 -0.476 -0.249 -0.156 -0.194 -0.125 1 -0.25 -0.394 -1.012 -0.424 -0.104 0.069 0.105 0.127 1 2.997 -0.255 -0.344 -1.021 -0.447 -0.195 -0.044 0.105 0.009 0.125 1 2.997 -0.255 -0.344 -0.105 -0.141 -0.102 -0.449 -0.150 0.004 0.105 0.112 <td< td=""><td>a. deg .153 .226 .300 .337 ATILITATIONS OF ALTO OF</td></td<></td> | a. deg .153 .226 .300 .337 will falles of 1701 .705 .779 .853 9 -0.007 -0.020 -0.022 -0.348 -0.470 -0.53 -0.136 -0.116 -0.100 1 0.017 -0.025 -0.035 -0.418 -0.549 -0.470 -0.382 -0.138 -0.116 -0.110 -0.100 8 -0.026 -0.255 -0.385 -1.005 -0.476 -0.205 -0.026 -0.116 -0.116 -0.110 9 -0.026 -0.268 -0.499 -1.126 -0.539 -0.029 -0.023 -0.044 0.069 0.019 0.127 1 2.997 -0.256 -0.384 -1.023 -0.453 -0.181 0.069 0.108 0.123 2.997 -0.257 -0.393 -0.454 -0.162 0.004 0.069 0.108 0.123 1 2.997 -0.212 -0.195 -0.184 -0.154 -0.184 0.019 | a, deg .153 .226 .300 .337 Attivates of | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | a, deg .153 .226 .300 .337 will values of 150 of 170 of | a. deg .153 .226 .300 .337 .411 Values 0.710 ol. .715 .779 .853 9 -0.007 -0.020 -0.022 -0.478 -0.470 -0.335 -0.136 -0.116 -0.100 1 0.017 -0.025 -0.035 -0.418 -0.476 -0.235 -0.136 -0.137 -0.125 8 -0.026 -0.026 -0.409 -1.126 -0.439 -0.204 -0.024 -0.139 -0.139 -0.139 -0.125 -0.136 -0.137 -0.125 -0.136 -0.137 -0.125 -0.137 -0.125 -0.136 -0.137 -0.125 -0.136 -0.136 -0.137 -0.125 -0.136 -0.137 -0.125 -0.136 -0.137 -0.137 -0.125 -0.136 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.137 -0.139 -0.144 -0.137 -0.144 -0.144 -0.144 -0.144 -0.144 | a. deg .153 .226 .300 .337 .4111 Annes of LATO .705 .779 .853 9 -0.007 -0.022 -0.372 -0.470 -0.353 -0.156 -0.116 -0.100 9 -0.007 -0.025 -0.035 -0.418 -0.249 -0.530 -0.156 -0.116 -0.107 -0.105 9 -0.026 -0.255 -0.035 -0.476 -0.253 -0.156 -0.197 -0.125 9 -3.007 -0.266 -0.499 -1.102 -0.476 -0.249 -0.156 -0.194 -0.125 1 -0.25 -0.394 -1.012 -0.424 -0.104 0.069 0.105 0.127 1 2.997 -0.255 -0.344 -1.021 -0.447 -0.195 -0.044 0.105 0.009 0.125 1 2.997 -0.255 -0.344 -0.105 -0.141 -0.102 -0.449 -0.150 0.004 0.105 0.112 <td< td=""><td>a. deg .153 .226 .300 .337 ATILITATIONS OF ALTO OF</td></td<> | a. deg .153 .226 .300 .337 ATILITATIONS OF ALTO OF |

Table 6. Continued

(a) Concluded

									_	_	_	_			_,	_		_	_	_	_	-т	_	_	-	_	т-	т	1
	.926	-0.081	-0.098	0.150	0.152	0.146	0.153	0.150	0.141	-0.115	-0.079	-0.045	-0.069	-0.042	-0.016	0.004	900.0	-0.014	0.014	0.054	0.156	0.130	-0.098	-0.087	060'0-	-0.094	-0.109	-0 103	-2.0.0
	.853	-0.092	-0.112	0.128	0.126	0.127	0.134	0.133	0.126	-0.149	-0.112	-0.078	-0.107	-0.075	-0.049	-0.029	-0.025	-0.045	-0.019	0.032	0.138	0.107	-0.115	-0.102	-0.106	-0.111	121	9118	2117
875	<i>6LL</i> :	-0.113	-0.130	0.099	0.093	0.099	0.107	0.109	0.105	-0.177	-0.145	-0.113	-0.143	-0.109	-0.086	-0.071	-0.061	-0.080	-0.052	0.008	0.110	0.082	-0.133	-0.120	-0.131	-0.134	0.137	0.135	0.11.0
Static pressure coefficients on nozzle top flap at $y/Y = 0.875$ with values of x/I of—	.705	-0.160	-0.169	0.066	0.055	0.064	0.074	0.078	0.077	-0.198	-0.176	-0.147	-0.173	-0.140	-0.124	-0.120	-0.111	-0.110	-0.081	-0.016	0.078	0.046	-0.175	-0.149	-0.186	-0 178	0.163	0.10	101.0
nozzle top fla of x/l of—	.558	-0.327	-0.362	-0.023	-0.040	-0.023	600.0-	0.002	0.010	-0.235	-0.233	-0.209	-0.230	-0.206	-0.206	-0.222	-0.247	-0.178	-0.151	-0.081	-0.014	-0.030	-0.361	-0.348	-0.342	0 343	0.227	0.347	-0.347
fficients on nozzle top with values of x/l of-	.411	-0.372	-0.421	-0.190	-0.220	-0.194	-0.168	-0.145	-0.132	-0.331	-0.326	-0.308	-0.336	-0.308	-0.326	-0.341	-0.344	-0.290	-0 274	-0.226	-0.190	-0.183	-0.414	-0.403	-0.424	0 305	202.0	-0.390	-0.458
pressure coe	.337	-0.499	-0.546	-0.436	-0.488	-0.439	-0.395	-0.361	-0.337	-0.572	-0.512	-0.462	-0.522	-0.461	-0.451	-0.450	-0.451	-0.434	-0.424	-0.455	-0.459	-0.397	-0.538	-0.535	895.0	0.554	-0.334	-0.538	-0.592
Static	300	-0.361	-0.407	-0.918	-1.047	-0.927	-0.874	-0.816	-0.741	-0.752	-0.800	-0.843	-0.848	-0.842	-0.841	78.0	0830	0.861	0.001	1 017	1176	277.0	0.387	0.303	0.233	11.0	-0.429	-0.435	-0.447
	.226	-0.013	-0.028	0.344	-0.362	-0.348	-0.339	-0.341	-0 340	-0.146	-0.174	50 198	187	100	0220	0.238	0.270	1000	777	0.250	0.353	0.318	0.010	0.017	200	-0.027	-0.043	-0.059	-0.033
	.153	9100	72007	-0.237	-0.246	-0.240	-0.244	-0.250	10.254	-000	-0.119	0710	0.137	0170	0.156	0.1.0	-0.172	0.160	-0.130	-0.109	0.337	0.777	0.010	0.010	-0.011	-0.024	-0.038	-0.050	-0.024
	a, deg	2000	0.017	9000	3 007	0.030	2 007	\$ 907	0.003	0.036	110.6	0.010	2,007	-3.05-	2,002	3.002	0.000	9.018	0.023	0.021	-0.010	0.002	2.020	-3.030	10.00	2.942	6.007	9.002	0.020
	M	1 240	1 201	107.1	0.500	0.500	0,000	0.001	0.00	0.00	0.240	0.00	0.901	0.900	0.898	0.090	0.897	0.899	0.875	0.850	0.798	0.700	0.401	1.201	1.202	1.199	1.200	1.198	1.153

Table 6. Continued

(b) Static pressure coefficients on nozzle sidewall

	.926	-0.067	180	0.001	0.153	0.148	0.153	0.152	0.139	-0.083	-0.038	-0.013	-0.025	800	0.000	0.01	0.070	0.018	0.018	7200	0.156	0.122	0.027	0.002	0.000	2/0.0	180.0	871.0
	.853	780 0-	-0.007	0.123	0110	0.118	0.122	0.121	0.112	-0.119	6900	-0.038	-0.056	-0.035	0100	0.00	0.006	8000	0.000	0.00	0.136	0 108	0000	0.093	0.00	760.0-	01.0	50.0
0.75	977.	921.05	0 133	0 008	060 0	0.093	0.098	0.100	0.095	-0.160	-0.101	-0.070	-0.092	10.064	-0.038	8100	-0.013	-0.037	0000	0.030	0.109	0.078	-0.124	0.121	0.133	-0.133	-0.139	10.140
Static pressure coefficients on nozzle sidewall at $z/Z = 0.75$.705	-0.205	-0.212	0.072	0.064	0.072	0.080	0.087	0.089	-0.192	-0.138	-0.102	-0.126	860.0-	9200-	-0.053	-0.028	-0.069	-0.039	0.015	0.081	0.053	-0.229	0 182	100	0.199	0.171	0.143
efficients on nozzle side	.558	-0.319	-0.355	-0.010	-0.024	-0.011	0.002	0.014	0.023	-0.238	-0.214	-0.188	-0.212	-0.184	-0.188	-0.197	-0.149	-0.154	-0.126	-0.053	-0.002	-0.016	-0.347	7970	0.241	0.352	-0.333	-0.389
coefficients o	.411	-0.375	-0.416	-0.175	-0.191	-0.175	-0.156	-0.137	-0.122	-0.443	-0.395	-0.350	-0.356	-0.350	-0.369	-0.444	-0.552	-0.321	-0.292	-0.214	-0.175	-0.168	-0.384	-0401	-0 404	0.401	-0.473	-0.455
tic pressure c	.337	-0.488	-0.536	-0.416	-0.437	-0.421	-0.399	-0.385	-0.371	-0.877	-0.902	-0.815	-0.851	-0.796	-0.770	-0.893	-0.984	-0.644	-0.585	-0.543	-0.436	-0.379	-0.510	-0.522	-0.520	-0.542	-0.549	-0.576
Sta	300	-0.370	-0.411	-0.772	-0.794	-0.775	-0.739	-0.745	-0.740	-0.756	-0.803	-0.855	-0.861	-0.856	-0.860	-0.873	-0.871	-0.912	-0.965	-1.078	-0.926	-0.661	-0.425	-0.402	-0.410	-0.416	-0.418	-0.456
	.226	-0.012	-0.029	-0.350	-0.374	-0.352	-0.350	-0.354	-0.356	-0.154	-0.180	-0.209	-0.224	-0.209	-0.226	-0.233	-0.236	-0.234	-0.255	-0.303	-0.362	-0.323	-0.035	-0.017	-0.036	-0.045	-0.057	-0.038
	.153	-0.012	-0.027	-0.232	-0.253	-0.235	-0.238	-0.244	-0.251	-0.101	-0.121	-0.141	-0.154	-0.141	-0.153	-0.166	-0.174	-0.157	-0.173	-0.203	-0.237	-0.222	-0.029	-0.012	-0.026	-0.039		-0.028
	α, deg	-0.007	0.017	-0.026	-3.007	0.030	2.997	5.992	9.003	0.036	-0.011	-0.012	-3.024	0.002	3.002	9.000	9.018	0.025	0.021	-0.018	0.002	-0.012	-3.030	0.004	2.942	6.007	9.002	0.020
	M _∞	1.249	1.201	0.598	0.599	0.600	0.601	0.601	0.601	0.948	0.925	0.901	0.900	0.898	0.898	0.897	0.899	0.875	0.850	0.798	0.700	0.401	1.201	1.202	1.199	1.200	1.198	1.153

Table 6. Continued

(b) Continued

-0.142 -0.0860.004 0.134 0.154 0.155 0.160 -0.064 -0.024 0.019 0.030 0.023 0.082 0.157 -0.080-0.073990.0 -0.0790.159 0.157 0.141 -0.065 0.001 0.031 926 0.00 0.025 990.0 0.136 -0.109-0.086 -0.032-0.024 -0.0050.134 -0.094-0.101 -0.1530.120 -0.0280.008 -0.092 -0.089 960.0-0.132 0.135 -0.053-0.001 0.11 -0.081 0.131 0.131 .853 *6LL*: ı ı ı ŧ Static pressure coefficients on nozzle sidewall at z/Z = 0.50-0.1760.016 -0.214-0.185-0.092 -0.065 0.046 -0.068 -0.0420.058 -0.181-0.143-0.095 -0.082-0.195-0.1990.070 0.067 0.069 0.075 0.079 0.075 -0.1580.081 -0.201 9.11 6.103 with values of x/l of-.558 ł -0.386 -0.350-0.514-0.508 -0.510 -0.526-0.444-0.468-0.184-0.158-0.388 -0.318-0.249-0.182-0.570-0.470-0.182-0.174-0.593-0.465-0.5660.180 -0.520-0.165-0.526-0.19614. -0.549 -0.619 -0.565<u>-0.403</u> -0.565 -0.535-0.566 -0.819 -0.972-1.092-0.503 0.444 -0.478-0.446 -0.438 -0.443 -0.795 -0.872 -0.457-0.598-0.943-0.774-0.571-0.439-0.980 -0.547.337 -1.078 -0.989 -0.409-0.406 -0.424-0.418 -0.765 -0.816 -0.875 -0.875 -0.926 -0.694-0.420 -0.813 -0.913-0.812-0.874-0.873-0.899 -0.973-0.461-0.374-0.831-0.877-0.421-0.801 300 -0.048 -0.045 -0.219-0.206-0.221 -0.229 -0.229-0.224 -0.244 -0.269 -0.321 -0.392 -0.349-0.023-0.040 -0.390-0.164 4 -0.192-0.014-0.018 -0.035-0.383-0.385-0.384-0.390-0.381 .226 -0.040 -0.176-0.236-0.010 -0.026-0.032-0.029 -0.266 -0.270-0.102 -0.144-0.144 -0.144 -0.159 -0.209-0.255-0.151-0.166-0.009 -0.123-0.161-0.247-0.257-0.261 -0.011 .153 3.002 -0.018 -0.012 2.942 9.002 0.020 a, deg 0.036 -3.0249.018 0.025 0.002 -3.0300.004 6.007 -0.0260.0300.002 5.992 9.003 0.017 -3.0072.997 -0.0120.021 -0.007-0.0110.948 0.901 0.898 0.898 0.899 0.875 0.798 0.700 1.202 1.200 1.198 0.598 0.600 249 0.401 1.201 M 0.601 0.601

Table 6. Continued

(b) Continued

| Ţ | Τ | Τ | Τ | Т | Т | Т | Т | Т

 | Т

 | T | Т | Т | Т | Т | Т | 7 | Т

 | Т | Т | Т
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| .926 | 0.067 | 90.00 | 0.148 | 0 150 | 0 141 | 0.143 | 0.135 | 0.115

 | -0.042

 | 6100 | 0007 | 0000 | 100 | 0.00 | 0.017 | 0.006 | 0.021

 | 0.046 | 0.080 | 0.154
 | 0.133 | 5/00 | 200 | 0200
 | 1200 | 0.158 | 9200 |
| .853 | -0.003 | 901 | 0.131 | 0.138 | 0.134 | 0.137 | 0.132 | 0.105

 | -0.064

 | -0.042 | -0.029 | -0.015 | -0.025 | 1100 | -0.006 | -0.021 | -0.002

 | 0.024 | 0.066 | 0.136
 | 0.100 | -0.105 | 0.081 | -0.004
 | -0.113 | 06100 | -0.085 |
| <i>911</i> : | -0 142 | -0.139 | 0.101 | 0.106 | 0.101 | 0.102 | 0.098 | 0.065

 | -0.091

 | -0.070 | -0.063 | -0.052 | -0.061 | -0.047 | -0.040 | -0.055 | -0.037

 | -0.008 | 0.041 | 0.109
 | 0.083 | 0.14 | 0 118 | 041
 | -0.158 | -0.211 | 6.10 |
| .705 | -0.196 | -0.203 | 0.071 | 0.072 | 0.066 | 990.0 | 0.061 | 0.028

 | -0.122

 | -0.103 | -0.102 | -0.102 | -0.099 | -0.092 | -0.081 | -0.086 | -0.079

 | -0.047 | 0.013 | 0.080
 | 0.057 | -0.200 | -0.180 | -0.199
 | -0.203 | -0.243 | -0.148 |
| .632 | -0.256 | -0.276 | 0.036 | 0.040 | 0.036 | 0.037 | 0.035 | 0.008

 | -0.165

 | -0.150 | -0.152 | -0.168 | -0.151 | -0.155 | -0.149 | -0.128 | -0.127

 | -0.097 | -0.025 | 0.045
 | 0.022 | -0.264 | -0.259 | -0.270
 | -0.280 | -0.307 | -0.235 |
| .558 | -0.350 | -0.375 | -0.013 | -0.013 | -0.019 | -0.021 | -0.025 | -0.047

 | -0.231

 | -0.217 | -0.220 | -0.254 | -0.221 | -0.244 | -0.264 | -0.229 | -0.192

 | -0.159 | -0.077 | -0.003
 | -0.021 | -0.378 | -0.364 | -0.386
 | -0.425 | -0.448 | -0.392 |
| .484 | -0.436 | -0.484 | 6/0'0- | 6/0.0- | -0.081 | -0.083 | -0.087 | -0.106

 | -0.348

 | -0.315 | -0.307 | -0.347 | -0.304 | -0.343 | -0.404 | -0.393 | -0.268

 | -0.240 | -0.154 | -0.071
 | -0.087 | -0.511 | -0.477 | -0.518
 | -0.557 | -0.590 | -0.540 |
| .411 | -0.485 | -0.544 | -0.190 | -0.193 | -0.192 | -0.196 | -0.204 | -0.221

 | -0.814

 | -0.484 | -0.403 | -0.440 | -0.395 | -0.436 | -0.519 | -0.671 | -0.359

 | -0.336 | -0.281 | -0.187
 | -0.189 | -0.505 | -0.525 | -0.528
 | -0.532 | -0.546 | -0.591 |
| .337 | -0.499 | -0.548 | -0.449 | -0.464 | -0.451 | -0.468 | -0.490 | -0.520

 | -0.946

 | -0.969 | -0.659 | -0.722 | -0.641 | -0.693 | -0.885 | -1.096 | -0.544

 | -0.505 | -0.533 | -0.462
 | -0.416 | -0.534 | -0.537 | -0.550
 | -0.560 | -0.558 | -0.598 |
| .300 | -0.387 | -0.428 | -0.857 | -0.911 | -0.862 | -0.918 | -1.011 | -1.086

 | -0.782

 | -0.834 | -0.887 | -0.880 | -0.886 | -0.884 | -0.885 | -0.880 | -0.914

 | -0.927 | -1.036 | -1.061
 | -0.726 | -0.405 | -0.417 | -0.423
 | -0.417 | -0.418 | -0.474 |
| .226 | -0.020 | -0.042 | -0.393 | -0.398 | -0.394 | -0.400 | -0.403 | -0.386

 | -0.170

 | -0.198 | -0.227 | -0.217 | -0.226 | -0.218 | -0.209 | -0.201 | -0.249

 | -0.276 | -0.329 | -0.409
 | -0.371 | -0.018 | -0.027 | -0.034
 | -0.043 | -0.048 | -0.054 |
| .153 | -0.008 | -0.027 | -0.260 | -0.263 | -0.263 | -0.267 | -0.270 | -0.261

 | -0.106

 | -0.128 | -0.150 | -0.148 | -0.150 | -0.149 | -0.154 | -0.156 | -0.166

 | -0.184 | -0.218 | -0.261
 | -0.249 | -0.008 | -0.011 | -0.026
 | -0.043 | -0.052 | -0.033 |
| α, deg | -0.007 | 0.017 | -0.026 | -3.007 | 0.030 | 2.997 | 5.992 | 9.003

 | 0.036

 | -0.011 | -0.012 | -3.024 | 0.002 | 3.002 | 9.000 | 9.018 | 0.025

 | 0.021 | -0.018 | 0.002
 | -0.012 | -3.030 | 0.004 | 2.942
 | 6.007 | 9.002 | 0.020 |
| M∞ | 1.249 | 1.201 | 0.598 | 0.599 | 0.600 | 0.601 | 0.601 | 0.601

 | 0.948

 | 0.925 | 0.901 | 0.900 | 0.898 | 0.898 | 0.897 | 0.830 | 0.875

 | 0.850 | 0.798 | 0.700
 | 0.401 | 1.201 | 1.202 | 1.199
 | 1.200 | 1.198 | 1.153 |
| | α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 | a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.007 -0.008 -0.037 -0.485 -0.485 -0.436 -0.356 -0.196 -0.142 -0.003 | α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.007 -0.008 -0.020 -0.387 -0.485 -0.436 -0.350 -0.256 -0.196 -0.142 -0.093 0.017 -0.027 -0.0428 -0.544 -0.484 -0.375 -0.203 -0.139 -0.100 | α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.007 -0.008 -0.020 -0.387 -0.485 -0.436 -0.356 -0.196 -0.142 -0.093 - 0.017 -0.020 -0.328 -0.548 -0.484 -0.375 -0.203 -0.139 -0.100 - -0.026 -0.260 -0.393 -0.857 -0.449 -0.190 -0.019 -0.013 0.036 0.071 0.101 0.131 | α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.007 -0.008 -0.020 -0.387 -0.485 -0.436 -0.350 -0.256 -0.196 -0.142 -0.093 0.017 -0.026 -0.042 -0.548 -0.544 -0.375 -0.276 -0.203 -0.139 -0.100 -0.026 -0.260 -0.393 -0.857 -0.449 -0.190 -0.079 -0.013 0.036 0.071 0.101 0.131 -3.007 -0.263 -0.398 -0.911 -0.464 -0.193 -0.013 0.040 0.072 0.106 0.138 | α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.007 -0.008 -0.020 -0.387 -0.485 -0.436 -0.350 -0.256 -0.196 -0.142 -0.093 -0.017 -0.027 -0.042 -0.428 -0.548 -0.484 -0.375 -0.276 -0.196 -0.199 -0.100 -0.026 -0.360 -0.393 -0.857 -0.484 -0.079 -0.013 0.036 0.071 0.101 0.131 -3.007 -0.263 -0.398 -0.911 -0.464 -0.193 -0.013 0.040 0.072 0.106 0.134 0.030 -0.263 -0.394 -0.851 -0.192 -0.019 0.036 0.040 0.072 0.106 0.134 | α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.007 -0.008 -0.020 -0.387 -0.485 -0.436 -0.350 -0.256 -0.196 -0.142 -0.093 -0.017 -0.027 -0.042 -0.428 -0.544 -0.484 -0.375 -0.276 -0.196 -0.199 -0.109 -0.026 -0.260 -0.393 -0.857 -0.484 -0.013 0.036 0.071 0.101 0.131 -3.007 -0.263 -0.398 -0.911 -0.464 -0.193 -0.013 0.040 0.072 0.106 0.134 0.030 -0.263 -0.394 -0.451 -0.193 -0.019 0.036 0.036 0.106 0.104 2.997 -0.267 -0.400 -0.918 -0.196 -0.081 -0.027 0.066 0.102 0.137 | α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.007 -0.008 -0.020 -0.387 -0.485 -0.436 -0.350 -0.256 -0.196 -0.142 -0.093 -0.017 -0.027 -0.042 -0.428 -0.544 -0.484 -0.375 -0.276 -0.203 -0.139 -0.100 -0.026 -0.260 -0.393 -0.857 -0.449 -0.190 -0.013 0.036 0.071 0.101 0.131 -3.007 -0.263 -0.398 -0.911 -0.464 -0.193 -0.013 0.040 0.072 0.106 0.131 0.030 -0.263 -0.263 -0.451 -0.193 -0.019 0.040 0.072 0.106 0.134 2.997 -0.270 -0.400 -0.196 -0.196 -0.091 -0.091 0.037 0.066 0.101 0.134 5.992 -0.270 -0.403 -1.011 <td>α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.007 -0.008 -0.020 -0.387 -0.485 -0.436 -0.350 -0.256 -0.196 -0.142 -0.093 0.017 -0.027 -0.042 -0.428 -0.544 -0.484 -0.375 -0.276 -0.196 -0.139 -0.190 -0.026 -0.260 -0.393 -0.857 -0.449 -0.190 -0.013 0.036 0.071 0.101 0.131 -3.007 -0.263 -0.263 -0.911 -0.464 -0.193 -0.013 0.040 0.072 0.106 0.138 0.030 -0.263 -0.394 -0.862 -0.451 -0.192 -0.013 0.036 0.066 0.106 0.134 2.997 -0.270 -0.409 -0.204 -0.196 -0.083 -0.025 0.005 0.106 0.137 5.992 -0.270 -0.403 -1.011<td>α, deg.153.226.300.337.411.484.558.632.705.779.853-0.007-0.008-0.020-0.387-0.485-0.436-0.350-0.256-0.196-0.142-0.093-0.007-0.008-0.042-0.428-0.544-0.484-0.375-0.276-0.203-0.139-0.100-0.026-0.260-0.393-0.857-0.449-0.190-0.079-0.0130.0360.0710.1010.131-3.007-0.263-0.394-0.862-0.454-0.193-0.0130.0400.0720.1060.1342.997-0.267-0.400-0.918-0.468-0.196-0.0210.0360.1010.1342.997-0.270-0.403-1.011-0.490-0.204-0.0250.0350.0660.1020.1375.992-0.261-0.386-1.081-0.204-0.206-0.0250.0350.0610.0980.1050.036-0.106-0.106-0.106-0.106-0.210-0.0250.0050.0050.105</td><td>α, deg.153.226.300.337.411.484.558.632.705.779.853-0.007-0.008-0.020-0.387-0.485-0.436-0.350-0.256-0.196-0.142-0.0930.017-0.027-0.022-0.428-0.544-0.484-0.375-0.276-0.203-0.139-0.100-0.026-0.260-0.393-0.857-0.449-0.190-0.079-0.0130.0360.0710.1010.131-0.026-0.263-0.394-0.867-0.494-0.193-0.0130.0400.0720.1060.1342.997-0.267-0.400-0.918-0.451-0.195-0.0130.0360.0660.1010.1342.997-0.261-0.403-1.011-0.496-0.204-0.087-0.0250.0350.0610.0980.1329.003-0.261-0.136-0.136-0.210-0.0250.0350.0610.0980.1050.036-0.106-0.110-0.128-0.186-0.184-0.184-0.136-0.1650.0050.0050.036-0.106-0.110-0.186-0.814-0.315-0.165-0.105-0.091-0.042</td><td>α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.007 -0.008 -0.020 -0.387 -0.485 -0.436 -0.350 -0.256 -0.196 -0.142 -0.093 0.017 -0.027 -0.042 -0.428 -0.544 -0.436 -0.276 -0.276 -0.196 -0.197 -0.276 -0.203 -0.139 -0.190 -0.190 -0.019</td><td>a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.007 -0.008 -0.020 -0.387 -0.485 -0.436 -0.350 -0.196 -0.196 -0.102 -0.093 0.017 -0.027 -0.042 -0.489 -0.484 -0.350 -0.256 -0.196 -0.195 -0.195 -0.196 -0.196 -0.196 -0.196 -0.196 -0.196 -0.196 -0.196 -0.196 -0.196 -0.196 -0.197 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019
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-0.0077 -0.008 -0.032 -0.489 -0.485 -0.486 -0.356 -0.196 |

Table 6. Continued

(b) Concluded

e sidewall at $z/Z = -0.75$ I of—	.411 .558 .705 .926	0.322 -0.250 -0.071	0.361 -0.255 -0.082	0.013 0.071 0.146	- 0.003 0.082 0.151	0.013 0.072 0.140	0.028 0.062 0.139	0.046 0.042 0.132	0.061 0.039 0.134	0.226 -0.123 -0.041	0.212 -0.108 -0.029		0.231 -0.093 0.006	- -0.206 -0.097 -0.006	0.221 -0.104 -0.003	0.245 -0.131 -0.007	- -0.270 -0.142 -0.015	0.184 -0.075 0.019	0.154 -0.044 0.044	0.080 0.012 0.081	0.079	0.027 0.053 0.129	0.340 -0.234 -0.076	0.349 -0.233 -0.067	0.373 -0.290 -0.089	0.380 -0.353 -0.104	- -0.398 -0.391 -0.123	
Static pressure coefficients on nozzle sidewall at $z/Z = -0.75$ with values of x/l of—	. 300 .337	0.498	0.548	0.408	0.385	0.415	0.445	0.458	0.489	- -0.934	996:0- -	- -0.754	- -0.780	- -0.731	0.790	0.943	1.036	0.590	- [-0.547	0.556	- -0.425	0.367	- -0.532	0.535	0.545	- -0.554	, – –0.573	
	.153 .226	7 -0.010 -0.018	7 -0.023 -0.035	-0.225	7 -0.227 -0.345) -0.224 -0.352	7 -0.251 -0.383	2 -0.290 -0.427		5 -0.102 -0.157	1 -0.123 -0.181	2 -0.142 -0.209	-0.151	2 -0.140 -0.210	2 -0.160 -0.228	0 -0.198 -0.268	\vdash	-0.157	1 -0.173 -0.256	-0.206	2 -0.235 -0.359		0 -0.007 -0.019	4 -0.013 -0.020	2 -0.052 -0.057	7 -0.094 -0.103	2 -0.148 -0.157	
	M _∞ α, deg	1.249 -0.007	1.201 0.017	-	0.599 -3.007	-	0.601 2.997	0.601 5.992		0.948 0.036	<u>'</u>	0.901 -0.012		0.898 0.002	0.898 3.002	0.897 6.000	0.899 9.018	\vdash	0.850 0.021	0.798 -0.018	0.700 0.002	0.401 -0.012	1.201 –3.030	1.202 0.004	1.199 2.942	1.200 6.007	1.198 9.002	

Table 6. Continued

(c) Static pressure coefficients on nozzle bottom flap

	.926	-0.069	-0.088	0.152	0.162	0.151	0.152	0.153	0.150	-0.068	-0.060	-0.033	-0.012	-0.028	-0.035	-0.033	-0.019	0.002	0.036	0.089	0.157	0.133	-0.069	-0.075	-0.101	-0.109	-0.102	-0.088
	.853	-0.095	-0.110	0.125	0.134	0.123	0.118	0.115	0.107	-0.094	-0.094	-0.066	-0.045	-0.062	-0.075	-0.076	-0.065	-0.030	0.005	0.068	0.131	0.106	-0.106	-0.098	-0.122	-0.133	-0.183	-0.112
: 0.875	<i>6LL</i> :	-0.167	-0.158	0.098	0.109	0.098	0.000	0.082	0.070	-0.130	-0.132	-0.106	-0.088	-0.100	-0.117	-0.120	-0.113	-0.068	-0.032	0.044	0.105	0.079	-0.187	-0.135	-0.156	-0.191	-0.352	-0.142
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.875$ with values of x/I of—	705	-0.300	-0.278	0.065	0.076	0.064	0.050	0.038	0.019	-0.169	-0.176	-0.143	-0.136	-0.139	-0.158	-0.171	-0.174	-0.109	-0.069	0.014	0.073	0.049	-0.310	-0.236	-0.263	-0.370	-0.401	-0.200
cients on nozzle bottom with values of x/l of—	.558	-0.331	-0.374	-0.025	-0.013	-0.031	-0.052	-0.077	-0.103	-0.261	-0.249	-0.226	-0.243	-0.223	-0.239	-0.270	-0.291	-0.195	-0.163	-0.085	-0.014	-0.032	-0.348	-0.364	-0.386	-0.397	-0.405	-0.397
fficients on n with values	.411	-0.376	-0.420	-0.178	-0.154	-0.179	-0.210	-0.235	-0.254	-0.612	-0.375	-0.332	-0.376	-0.333	-0.347	-0.391	-0.468	-0.320	-0.314	-0.273	-0.180	-0.173	-0.385	-0.404	-0.415	-0.433	-0.461	-0.459
pressure coe	.337	-0.475	-0.524	-0.391	-0.351	-0.392	-0.438	-0.467	-0.489	-0.879	-0.764	-0.585	-0.630	-0.585	-0.614	-0.751	-0.930	-0.549	-0.563	-0.612	-0.420	-0.363	-0.530	-0.508	-0.537	-0.543	-0.541	-0.566
Static	.300	-0.402	-0.447	-0.769	-0.714	-0.777	-0.869	-0.927	-0.970	-0.795	-0.843	-0.885	-0.924	-0.885	-0.891	-0.902	-0.901	-0.922	-0.983	-1.130	-0.927	-0.664	-0.447	-0.433	-0.442	-0.443	-0.438	-0.486
	.226	-0.021	-0.044	-0.369	-0.361	-0.377	-0.395	-0.409	-0.418	-0.167	-0.196	-0.223	-0.243	-0.224	-0.215	-0.214	-0.211	-0.250	-0.273	-0.327	-0.388	-0.339	-0.033	-0.028	-0.034	-0.045	-0.052	-0.050
	.153	-0.006	-0.029	-0.236	-0.241	-0.240	-0.251	-0.264	-0.277	-0.103	-0.125	-0.144	-0.159	-0.143	-0.142	-0.149	-0.157	-0.162	-0.178	-0.211	-0.244	-0.226	-0.014	-0.013	-0.029	-0.041	-0.062	-0.029
	α, deg	-0.007	0.017	-0.026	-3.007	0.030	2.997	5.992	9.003	0.036	-0.011	-0.012	-3.024	0.002	3.002	9.000	9.018	0.025	0.021	-0.018	0.002	-0.012	-3.030	0.004	2.942	6.007	9.002	0.020
	Μ∞	1.249	1.201	0.598	0.599	0.600	0.601	0.601	0.601	0.948	0.925	0.901	0.900	0.898	0.898	0.897	0.899	0.875	0.850	0.798	0.700	0.401	1.201	1.202	1.199	1.200	1.198	1.153

Table 6. Continued

(c) Continued

				Static	pressure coe	Static pressure coefficients on nozzle bottom flap at $v/Y = 0.50$	ozzle botton	flap at y/Y =	- 0.50		
				Otalic	on a messard	with values of x/l of-	—jo //x. jo				
M	α. deg	.153	.226	.300	.337	.411	.558	.705	677.	.853	.926
970	2000	7000	-0.027	-0.412	-0.505	-0.495	-0.464	-0.200	-0.138	-0.107	-0.080
1 201	0.00	0.030	-0.049	-0.462	-0.558	-0.552	-0.500	-0.195	-0.155	-0.128	-0.105
1.201	9000	0.030	-0.464	-0.889	-0.473	-0.217	-0.038	0.064	0.100	0.131	0.151
0.390	3 007	0.20	-0.446	-0.864	-0.453	-0.202	-0.031	0.070	0.106	0.136	0.155
0,500	0.030	0.205	-0.470	-0.897	-0.477	-0.220	-0.045	0.061	0.098	0.129	0.147
0.000	2 997	-0.307	-0.496	-0.994	-0.531	-0.259	-0.076	0.041	0.085	0.122	0.146
0.00	\$ 000	0310	-0.509	-1.080	-0.570	-0.289	-0.103	0.021	0.070	0.112	0.141
1090	9,003	-0.304	-0.512	-1.142	-0.598	-0.311	-0.127	-0.001	0.051	0.097	0.132
0.00	0.036	5116	-0.195	-0.822	-0.887	-0.582	-0.288	-0.192	-0.151	-0.110	-0.072
0.040	0.000	0 138	-0.224	-0.837	-0.568	-0.360	-0.253	-0.178	-0.139	-0.102	-0.060
0.000	0.012	0.1.0	-0.252	-0.802	-0.457	-0.322	-0.229	-0.151	-0.110	-0.071	-0.035
106.0	2007	0.165	7570	-0.858	-0.529	-0.363	-0.259	-0.162	-0.113	-0.069	-0.031
0.300	-5.024	0.161	0.250	-0 794	-0.459	-0.320	-0.228	-0.146	-0.106	-0.069	-0.031
0.090	3,002	0.151	-0.230	928 0-	-0.491	-0.336	-0.239	-0.155	-0.114	-0.074	-0.033
0.090	2:007	0130	-0 224	-0.884	-0.627	-0.387	-0.265	-0.166	-0.119	-0.074	-0.028
0.097	0.000	0.133	0.203	_0 903	-0.875	-0.461	-0.287	-0.170	-0.118	-0.068	-0.021
0.039	9.010	0.122	0.282	_0.703	-0.442	-0.317	-0.213	-0.122	-0.081	-0.042	-0.007
0.8/3	0.023	0.173	0.202	0.844	-0.461	-0.326	-0.191	-0.089	-0.045	-0.008	0.026
0.830	0.021	0.136	-0.375	-1 034	-0.582	-0.343	-0.130	-0.015	0.026	0.056	0.077
07.70	2000	7070	-0.476	-1.165	-0.489	-0.212	-0.024	0.073	0.106	0.135	0.154
200.00	200.0	0.283	-0.426	792 0-	-0.440	-0.217	-0.049	0.046	0.083	0.109	0.130
0.40	2.030	0.012	0.033	-0 445	-0.539	-0.533	-0.520	-0.244	-0.155	-0.119	-0.083
1.201	-5.050	0.012	0.036	-0 440	-0 543	-0.537	-0.477	-0.179	-0.144	-0.121	-0.093
1,00	20.0	0.01	0.030	-0.447	-0.551	-0.533	-0.509	-0.190	-0.159	-0.136	-0.115
1.199	2.942	0.022	0.03	0.441	0 550	-0.523	-0.521	-0.231	-0.171	-0.144	-0.123
1.200	30.00	10.01	0100	-0.430	-0.544	-0.512	-0.520	-0.454	-0.311	-0.157	-0.116
1.170	200.0	0.033	0 041	505 0-	-0.603	-0.599	-0.438	-0.199	-0.168	-0.143	-0.114
1.133	0.020	CC0.0	7.001	3333							

Table 6. Continued

(c) Concluded

M_{∞} α , deg								
0.007	.153	.226	.300	.337	.337 .411	.558	.705	.926
	-0.006	-0.032	-0.406	-0.486	1	-0.462	-0.182	-0.094
0.017	-0.027	-0.054	-0.456	-0.538		-0.478	-0.192	-0.118
-0.026	-0.311	-0.472	-0.920	-0.496	1	-0.051	0.056	0.152
-3.007	-0.299	-0.456	-0.889	-0.473	_	-0.038	0.065	0.153
0.030	-0.313	-0.478	-0.931	-0.501	ı	-0.053	0.057	0.145
2.997	-0.327	-0.504	-0.992	-0.545	1	-0.082	0.035	0.138
5.992	-0.331	-0.518	-1.063	-0.579	1	-0.108	0.015	0.132
9.003	-0.327	-0.521	-1.107	-0.602	-	-0.128	-0.00 4	0.121
0.036	-0.125	-0.209	-0.818	-0.815	ı	-0.287	-0.206	-0.079
-0.0	-0.146	-0.234	-0.830	-0.556	1	-0.242	-0.174	-0.057
-0.012	-0.170	-0.261	-0.822	-0.478	1	-0.220	-0.141	-0.032
-3.024	-0.174	-0.266	-0.865	-0.540	ı	-0.246	-0.150	-0.027
0.002	-0.169	-0.261	-0.816	-0.475	1	-0.218	-0.138	-0.030
3.002	-0.161	-0.254	-0.841	-0.507		-0.226	-0.148	-0.034
9.000	-0.150	-0.243	-0.881	-0.598	-	-0.256	-0.172	-0.035
9.018	-0.132	-0.226	-0.905	-0.771	1	-0.290	-0.190	-0.032
0.025	-0.189	-0.290	-0.840	-0.476	1	-0.199	-0.110	-0.003
0.021	-0.206	-0.319	-0.889	-0.496		-0.176	-0.082	0.028
-0.018	-0.257	-0.387	-1.083	-0.611	***	-0.124	-0.016	0.082
0.002	-0.313	-0.487	-1.165	-0.519		-0.039	0.066	0.159
-0.012	-0.297	-0.429	-0.792	-0.450	_	-0.065	0.033	0.137
-3.030	-0.013	-0.044	-0.447	-0.530	1	-0.498	-0.220	-0.102
0.0 20	-0.017	-0.045	-0.447	-0.530	1	-0.452	-0.182	-0.107
2.942	-0.021	-0.046	-0.449	-0.536	-	-0.460	-0.192	-0.125
6.007	-0.016	-0.040	-0.443	-0.530	-	-0.510	-0.211	-0.133
9.002	-0.004	-0.025	-0.435	-0.525	1	-0.504	-0.461	-0.129
0.020	-0.034	-0.068	-0.500	-0.588	1	-0.442	-0.203	-0.118

Table 6. Concluded

(d) Force data

c_D	0.2724	0.2926	9/90.0	0.0672	0.0651	0.0675	0.0777	0.0937	0.2803	0.2444	0.2144	0.2353	0.2137	0.2203	0.2446	0.2724	0.1939	0.1744	0.1349	0.0805	0.0651	0.3048	0.2859	0.3004	0.3154	0.3395	0.3058
α, deg	-0.007	0.017	-0.026	-3.007	0.030	2.998	5.992	9.003	0.036	-0.011	-0.012	-3.024	0.002	3.002	9.000	810.6	0.025	0.021	-0.018	0.002	-0.012	-3.029	0.004	2.942	6.007	9.002	0.020
M∞	1.249	1.201	0.598	0.599	0.600	0.601	0.601	0.601	0.948	0.925	0.901	0.900	0.898	868.0	0.897	0.899	0.875	0.850	0.798	0.700	0.401	1.201	1.202	1.199	1.200	1.198	1.153

Table 7. Pressure and Force Data for Nozzle 5 With $\beta_{l,top/bot} = 17.9^{\circ}/\beta_{l,side} = 0^{\circ}$, Plume On, and $\alpha = 0^{\circ}$

(a) Static pressure coefficients on nozzle top flap

	_	_	_				_	_		_	_		_	_	
	.926	0.171	0.018	-0.105	-0.118	-0.135	-0.150	-0.121	-0.092	-0.068	0.044	0.014	0.159	0.191	0.178
	.853	0.152	-0.012	-0.120	-0.135	-0.152	-0.173	-0.146	-0.121	-0.100	-0.075	-0.017	0.139	0.167	0.147
	<i>6LL</i> :	0.130	-0.041	-0.139	-0.148	-0.167	-0.191	-0.167	-0.143	-0.124	-0.102	-0.043	0.118	0.139	0.123
line	.705	960'0	-0.067	-0.147	-0.162	-0.181	-0.205	-0.184	-0.162	-0.141	-0.125	690:0-	680'0	0.104	060'0
Static pressure coefficients on nozzle top flap at centerline with values of x/l of—	.632	0.055	-0.097	-0.158	-0.171	-0.193	-0.219	-0.199	-0.183	-0.165	-0.150	-0.098	0.047	0.051	0.033
efficients on nozzle top with values of x/l of—	.558	-0.003	-0.132	-0.176	-0.191	-0.211	-0.235	-0.215	-0.201	-0.190	-0.179	-0.133	-0.012	-0.014	-0.032
coefficients o	.484	-0.087	-0.175	-0.431	-0.411	-0.326	-0.258	-0.236	-0.226	-0.218	-0.209	-0.177	-0.097	-0.103	-0.124
atic pressure	.411	-0.224	-0.233	-0.491	-0.541	-0.608	-0.304	-0.271	-0.256	-0.251	-0.248	-0.237	-0.237	-0.238	-0.250
Str	.337	-0.578	-0.351	-0.523	-0.574	-0.637	-0.412	-0.359	-0.326	-0.314	-0.323	-0.352	-0.589	-0.533	-0.498
	.300	-1.303	-0.758	-0.427	-0.473	-0.530	699.0-	-0.615	-0.596	-0.596	-0.629	-0.739	-1.243	-1.193	-0.975
	.226	-0.462	-0.342	-0.025	-0.031	-0.055	-0.170	-0.206	-0.236	-0.264	-0.288	-0.341	-0.459	-0.490	-0.460
	.153	-0.302	-0.230	-0.021	-0.018	-0.036	-0.105	-0.135	-0.156	-0.176	-0.195	-0.229	-0.300	-0.322	-0.311
	M∞	969.0	0.799	1.252	1.199	1.150	0.954	0.926	0.900	0.876	0.851	0.801	0.702	0.602	0.400

	,	_		,							_				
	.926	0.178	0.025	-0.099	-0.112	-0.128	-0.154	-0.124	-0.090	-0.0 6 4	-0.039	0.022	0.169	0.192	0.183
	.853	0.153	-0.007	-0.115	-0.128	-0.147	-0.180	-0.148	-0.119	-0.093	-0.071	-0.011	0.145	0.166	0.157
0.50	622:	0.124	-0.035	-0.126	-0.142	-0.160	-0.199	-0.172	-0.146	-0.121	-0.098	-0.039	0.113	0.127	0.108
flap at $y/Y =$.705	0.086	-0.061	-0.139	-0.154	-0.175	-0.216	-0.191	-0.168	-0.144	-0.124	-0.065	0.077	0.082	0.064
efficients on nozzle top with values of x/l of—	.558	-0.018	-0.127	-0.223	-0.221	-0.222	-0.247	-0.222	-0.206	-0.190	-0.175	-0.126	-0.023	-0.026	-0.035
oefficients o	.411	-0.215	-0.248	-0.479	-0.525	-0.590	-0.325	-0.289	-0.275	-0.270	-0.263	-0.252	-0.227	-0.221	-0.223
Static pressure coefficients on nozzle top flap at $y/Y = 0.50$ with values of x/l of—	.337	-0.547	-0.409	-0.526	-0.575	-0.643	-0.441	-0.386	-0.366	-0.362	-0.363	-0.413	-0.571	-0.502	-0.479
Sta	300	=	-	1	1	_	_		_	ı	_	_	_	_	-
	.226	-0.444	-0.339	-0.022	-0.030	-0.058	-0.168	-0.205	-0.236	-0.264	-0.286	-0.337	-0.442	-0.466	-0.439
	.153	-0.272	-0.213	-0.010	-0.011	-0.033	-0.095	-0.125	-0.146	-0.165	-0.182	-0.212	-0.272	-0.287	-0.280
	М	969.0	0.799	1.252	1.199	1.150	0.954	0.926	0.900	0.876	0.851	0.801	0.702	0.602	0.400

Table 7. Continued
(a) Concluded

			Staf	o presente c	Static pressure coefficients on nozzle top flap at $y/Y = 0.75$	nozzle top f	$ ap \ at \ v/Y = ($	1.75		
			Stat	o picesano si	with values of x/l of—	—Jo <i>I/x</i> Jo				
	.5.	300	300	337	411	.558	705	622	.853	.926
M	cc1.	077.	ooc:	757.0	7000	0.066	0.034	0.078	0.123	0.170
9690	-0.248	-0.378	-1.098	-0.430	-0.220	0,000	1000	2000	000	0.061
0 700	-0.207	-0.309	-0.911	-0.445	-0.224	-0.109	-0.051	-0.023	0.003	0.00
0.727	0.10	2100	0.418	-0.517	-0.338	-0.309	-0.215	-0.182	-0.161	-0.0%
707.1		70.01	27.0	0.550	992.0	0 334	-0.219	-0.190	-0.166	-0.101
1.199	810.0	-0.025	-0.407	40.23	000.0-	1000	2000	0010	0.178	9010
1.50	CA10.0_	-0.053	-0.523	-0.620	-0.421	-0.360	-0.222	10.1%	0,170	
1.130	/ I '	251.0	172.0	-0.467	-0 328	-0.236	-0.204	-0.187	-0.160	-0.125
0.954	-0.100	-0.13/	7.7	101-0	2000	2100	0 101	0 1 50	0510	-0.097
9200	-0.130	-0.196	-0.678	-0.412	1-0.291	-0.217	101.0	61.0		6000
077.0	. 1	7000	0.676	708	-0.278	-0.197	-0.155	-0.128	-0.102	-0.003
0.900		-0.220	2000	2000	0 271	9210	-0 131	-0.104	-0.075	-0.033
0.876	-0.168	-0.253	-0.695	-0.397	-0.271	21.0	201.0	0.002	0.050	2000
0.851	-0.183	-0.270	-0.738	-0.404	-0.260	-0.134	201.02	C00:0-	0000	0900
		0.212	0880	-0.453	-0.230	90.109	-0.054	-0.027	0.008	0.038
0.801		717	0,0,0		0.033	1,200	0.005	0.072	0.116	0.162
0.705	-0.251	-0.386	-1.112	70.400	-0.233	1,0.0	2000	0.020	001.0	0 160
0,603	0.056	180	-0.930	0.440	-0.228	-0.073	0.020	0.07	0.120	61.5
0.007	0.530	7220	0.786	-0411	_0.223	-0.075	-0.006	0.053	960.0	0.147
0.400	-0.248	1/5.0	70.700							

						_	_	_	_	_	_	_	_	_	ı	T	_	_	_		Г	٦
	.926		-0.002	-0.030	-0.316		-0.28/	-0.288	1010	171.0	- - - - - - - - - - - - - - - - - - -	0300	-0.009	-0.052	660	-0.0 1	-0.028	500	10.00	600.0 00.00	000	070.0
	.853	2000	-0.080	9.100	0.434	1	-0.415	-0.423		-0.139	0.129		-0.10/	900	200	-0.095	960.0	5600	//0:0-	-0.082	180	-0.0%
C/8	770		-0.110	-0.133	1770	1/+/1	-0.475	0.503	COCIO	-0.191	7510		-0.136	0/10	0.127	-0.128	-0.128		901.0	A) 104		-0.10 4
$ap \ at \ y/Y = 0.$	705	50/:	-0.120	-0.145	0 440	-0.44o	-0.467	0070	-0.407	-0.219	0.170	21.5	5.16 24	7510	-0.133	-0.149	-0 144	11.0	-0.119	0 118		-0.123
Static pressure coefficients on nozzle top flap at $y/Y = 0.873$ with values of x/I of—	055	900.	-0.166	-0.167	100	-0.398	-0.428	0.450	-0.409	-0.246	0.010	7.77	-0.196	2010	-0.18/	-0.176	0.168	901.0	-0.170	7610	27.7	-0.186
efficients on nozzle top with values of v/l of—	111	.411	-0.341	7800	0.204	-0.338	-0.371		-0.470	-0.321	0.00	20.270	-0.252		-0.249	-0.255	7000	-0.204	-0.342	0.221	1000	0300
c pressure co	200	.33/	-0.476	0110	-0.419	-0.314	0 342	2.0.0	-0.393	-0.450		-U.384	79.4	200	-0.357	-0.370		-0.418	-0.480		-0.442	765 0
Static		300	0.706	27.0	-0./42	-0.326	0.357	4.0.0	-0.406	0.638	200.0	99.0	0.687	700.0	-0.697	517	200	-0.736	0.717		-0.633	295 0
		.226	0.325	0.323	-0.288	40.014	2000	-0.020	-0.055	0 156	20.1.20	-0.192	600	70.220	-0.242	0.057	157.0	-0.287	0 220	-0.327	0.321	0 306
		.153	7100	-0.21¢	-0.188	-0.005		-0.011	-0.035	100	1,0,71	-0.120	9,10	-0.140	-0.154	0.167	70.10	-0.186	2100	70.210	-0.215	0000
		M	8 3	0.090	0.799	1 252	7.77	1.199	1 150	7 30 0	0.934	9200		0.900	0.876	0.051	0.831	0.801		0.707	0.602	007

Table 7. Continued

(b) Static pressure coefficients on nozzle sidewall

		Т	T		Г	т	7		Т	т	_	Т	-		т	_	_	_	_	_	_	_
		900	027:	0.087	0.016	25.0	-0.270	-0.258	0770	0.617	-0.115	7000	4.0.7	690.0	970	25.5	-0.029	0.013	200	0.081	0.076	
		853	Con:	-0.034	-0.093	0.417	11.0	-0.415	0.420	27.0	-0.141	-0 133	60.0	6119	5113		-0.10/	-0.096	0000	-0.040	-0.055	700.0
nd sidewall		622	31, 3	-0.148	-0.172	0 512	0.5.0	-0.528	285 OT	0010	-0.109	50 164		-0.103	-0.165	0 167	7.10	-0.172	141	17:7	-0.169	2000
zle top flap a		.705	3.00	-0.219	-0.216	20,576	2,5,5	-0.017	-0.647	201.0	77.17	-0.175	105	-0.183	0.190	001.0	0.177	-0.211	21.0	0.210	-0.229	CVCO
Static pressure coefficients on corner between nozzle top flap and sidewall	with values of .v/l of	.558	0 213	20.51.5	-0.281	-0.433	077.0	-0.408	-0.509	1000	0.471	-0.211	0.22	7777	-0.242	7355	0.433	-0.275	-0.310	21.00	-0.311	<u></u> የሀኔ ሀገ
ents on come	with value	1 1	0.366	0000	-0.329	-0.274	0 202	505.0	-0.352	705 0	7/25	0.334	787	0.70	-0.284	-0.299		-0.325	-0.365	276.0	0.240	70322
sure coefficie		.337	5413	Citio	-0.395	-0.214	7260	0.4.37	-0.283	-0.435		-0.424	-0411		-0.389	-0.375	7000	±0.394	-0.418	0 207	70.70	-0.362
Static pres		 995:	-0.405		-0.314	-0.220	-0.240	25.5	-0.286	-0.465	000	-0.508	-0.538		-U.344	-0.533	0.514	+10.0	-0.501	2 455		-0.417
	755	077:	-0.287	1700	1/7.0	-0.017	-0.028	0.00	-0.039	-0.153	0 100	-0.109	-0.215	222	0.433	-0.251	0.70	0.710	-0.289	776		-0.262
	153	.133	-0.194	9710	0.170	-0.004	-0.012	0.030	0.030	0.000	0110	7.17	-0.138	0.151		-0.164	721 0		-0.196	161.0-	0 105	-0.185
	7	8	969.0	0 700		1.222	1.199	150	2	0.954	9200	0.720	0.800	9280	2,070	0.851	0.801	200	0.702	0.602	5	0.400

Table 7. Continued

(b) Concluded

				Sta	tic pressure o	coefficients o	Static pressure coefficients on nozzle sidewall at centerline	wall at center	line			
						WILL VALUE	with values of .v.r of—					1
M	.153	.226	300	.337	.411	.484	.558	.632	.705	.779	.853	.926
969 0		-0.162	-0.175	-0.176	-0.165	-0.146	-0.121	-0.094	-0.061	-0.021	0.029	0.092
0 790		-0.177	-0.200	-0.203	-0.190	-0.169	-0.144	-0.121	-0.091	-0.056	-0.012	0.047
1 252		-0001	-0.016	-0.030	-0.069	-0.114	-0.165	-0.208	-0.246	-0.288	-0.326	-0.342
1 100		-0.017	-0.032	-0.051	-0.095	-0.140	-0.192	-0.238	-0.286	-0.322	-0.368	-0.352
1.150	1	-0.047	90.02	-0.088	-0.135	-0.181	-0.214	-0.250	-0.297	-0.342	-0.388	-0.333
0.054		-0 120	9.180	-0.219	-0.290	-0.337	-0.330	-0.258	-0.184	-0.138	-0.101	-0.065
0.006		-0.153	-0.215	-0.256	-0.314	-0.303	-0.211	-0.144	-0.125	-0.109	-0.089	-0.053
0.000		174	-0 234	-0.268	-0.267	-0.198	-0.162	-0.143	-0.123	-0.097	-0.071	-0.028
0.500		-0.183	ACC 0-	-0.244	-0.220	-0.190	-0.162	-0.138	-0.115	-0.085	-0.055	-0.006
0.851		-0.185	-0.218	-0.224	-0.206	-0.181	-0.160	-0.135	-0.107	-0.079	-0.041	0.011
0.801	1	-0 181	-0.200	-0.204	-0.192	-0.170	-0.148	-0.120	-0.091	-0.057	-0.014	0.048
0.707		-0.167		-0.180	-0.170	-0.152	-0.127	960'0-	-0.062	-0.023	0.025	0.092
0,602		-0.152	-0.155	-0.160	-0.152	-0.140	-0.120	-0.091	-0.063	-0.025	0.019	0.086
0.400	,	-0.140	-0.135	-0.147	-0.141	-0.138	-0.116	-0.089	-0.069	-0.034	0.000	0.069
2												

															_
	.926	0.000	0.043	-0.341	-0.325	-0.311	-0.075	-0.066	-0.043	-0.024	0.002	0.039	0.081	0.070	0.033
0.50	.705	-0.081	-0.109	-0.282	-0.321	-0.336	-0.182	-0.135	-0.134	-0.127	-0.121	-0.109	-0.081	-0.083	-0.085
/all at z/Z = -	.558	-0.149	-0.171	-0.201	-0.230	-0.254	-0.333	-0.216	-0.178	-0.179	-0.178	-0.171	-0.151	-0.143	-0.139
nozzle sidew of x/l of—	.411	-0.197	-0.221	-0.108	-0.134	-0.179	-0.333	-0.345	-0.293	-0.246	-0.234	-0.225	-0.204	-0.185	-0.169
efficients on nozzle side with values of x/l of—	.337	-0.214	-0.245	-0.062	880.0-	-0.125	-0.263	-0.300	-0.316	-0.294	-0.267	-0.247	-0.222	-0.199	-0.184
Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$ with values of x/l of—	300	-0.221	-0.252	-0.045	-0.067	-0.102	-0.220	-0.258	-0.280	-0.280	-0.271	-0.251	-0.225	-0.199	-0.178
Stati	.226		-	1	1	1	1	i	1	1	ł		-	-	
	.153	-0.161	-0.161	0.001	-0.010	-0.038	-0.083	-0.112	-0.129	-0.139	-0.151	-0.157	-0.159	-0.147	-0.133
	M	0.696	0.799	1.252	1.199	1.150	0.954	0.926	0.900	0.876	0.851	0.801	0.702	0.602	0.400

Table 7. Continued

(c) Static pressure coefficients on nozzle bottom flap

		.853 .926	- 0.031	0000		0.245	0.249) (13.	- 0.077	0.053	2000	0000	0.007	1000	470.0	10.00
= 0.875		.779	-0.077	-0.106	-0.427	-0.433	-0.461	-0.173	J 134	1 4 5	18	2 5	9 2	200	200	0.072
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.875$	ļ	.705	-0.091	-0.121	-0.422	-0.436	-0.447	-0.200	-0.157	-0 140	131	-0.128	-0.124	-0.095	-0.095	-0.094
nozzle bottor	with values of X/I of—	.558	-0.150	-0.160	-0.365	-0.408	-0.444	-0.249	-0.207	-0 187	-0.177	-0.169	161	-0.152	-0.155	-0.155
efficients on	with value	.411	-0.327	-0.304	-0.343	-0.383	-0.436	-0.360	-0.293	-0.271	-0.267	-0.272	-0.307	-0.330	-0.318	-0.303
pressure cox	233	.33/	-0.467	-0.446	-0.335	-0.372	-0.422	-0.521	-0.434	-0.408	-0.402	-0.406	-0.449	-0.472	-0.434	-0.396
Static	2000	.300	1	-	-	-	1	1	,	I	ı	ı	1		ı	ı
	375	077:	-0.327	-0.293	-0.014	-0.033	-0.062	-0.157	-0.193	-0.220	-0.241	-0.260	-0.292	-0.329	-0.318	-0.303
	153	CCT	-0.209	-0.187	0.002	-0.014	-0.037	-0.091	-0.122	-0.141	-0.155	-0.169	-0.188	-0.215	-0.212	-0.208
	7	W _∞	0.696	0.799	1.252	1.199	1.150	0.954	0.926	0.900	0.876	0.851	0.801	0.702	0.602	0.400

	_	_	_	_	_	_	_	_	_	_	_	_	_	_	_	_
	.926	0.107	0.077	0.078	960 0	801.9	9117	0.00	0.003	-0.034	0.030	0.004	0.075	0 181	0.107	0.177
	.853	0.168	0.100	101 0	50 118	-0.133	-0.147	8110	0.000	0.000	0000	-0.029	0.046	0.160	0.170	0.159
= 0.50	<i>611</i> :	0 138	0017	-0.122	-0.140	-0.154	-0.174	-0.147	0.116	0000	0.030	-0.001	0.016	0 129	0 133	0.116
n flap at y/Y	.705	0.096	-0.018	-0.145	-0.163	-0.181	-0.202	-0 175	-0.148	0.133	0.122	-0.092	-0.020	0.088	0.085	0.066
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.50$ with values of x/I of—	.558	-0.018	-0.112	-0.352	-0.270	-0.254	-0.263	-0.235	2160	0.217	0.176	2/17	-0.117	-0.029	-0.039	-0.062
efficients on with values	.411	-0.212	-0.286	-0.486	-0.533	-0.596	-0.353	-0.310	-0.202	786	0 280	0.507	-0.285	-0.217	-0.211	-0.211
pressure cox	.337	-0.501	-0.467	-0.528	-0.581	-0.645	-0.480	-0.412	-0.384	-0 380	0 305	2,7,0	-0.40 5	-0.514	-0.464	-0.434
Static	.300	-1.244	-0.838	-0.464	-0.515	-0.575	-0.714	-0.646	-0.623	-0.631	7) 666	000	-0.820	-1.204	-1.030	-0.872
	.226	-0.442	-0.341	-0.012	-0.030	-0.061	-0.172	-0.209	-0.238	-0.264	-0.288	0.341	-0.341	-0.441	-0.451	-0.425
	.153	-0.278	-0.222	0.001	-0.017	-0.041	-0.103	-0.134	-0.154	-0.172	-0.190	0.22	-0.222	-0.279	-0.286	-0.275
	M∞	969.0	0.799	1.252	1.199	1.150	0.954	0.926	0.900	0.876	0.851	0.801	0.001	0.702	0.602	0.400

Table 7. Concluded

(c) Concluded

		Static	pressure coe	Static pressure coefficients on nozzle bottom flap at centerline	ozzle bottom	flap at cente	rline	
				Willi values	10 1/4 10	033	305	300
M∞	.153	.226	.300	.337	.411	866.	cu/.	.920
9690	-0.299	-0.462	**	+	-0.233	-0.016	0.100	0.213
0.799	-0.234	-0.354	-	1	-0.276	-0.115	-0.018	0.080
1.252	0.004	-0.020	1	ļ	-0.486	-0.222	-0.176	-0.097
1 199	-0.020	-0.044	1	I	-0.536	-0.236	-0.183	-0.105
1.150	-0.043	-0.069	+		-0.595	-0.255	-0.204	-0.113
0.954	-0.110	-0.188	1		-0.349	-0.263	-0.207	-0.114
9260	-0.138	-0.219	1		-0.304	-0.231	-0.176	-0.088
0060	-0.158	-0.246		1	-0.289	-0.212	-0.147	-0.058
0.876	-0.175	-0.271	1		-0.284	-0.194	-0.120	-0.033
0.851	-0.197	-0.296	1	ļ	-0.284	-0.174	-0.093	0.008
0.801	-0.231	-0.352		I	-0.276	-0.119	-0.021	0.076
0.702	-0.296	-0.460	1	1	-0.239	-0.022	0.095	0.198
0.602	-0.307	-0.473	1	1	-0.236	-0.031	0.093	0.210
0.400	-0.294	-0.442	1	l	-0.239	-0.051	0.078	0.179

(d) Force data

													_
0.0131	0.0128	0.0119	0.0120	0.0122	0.0126	0.0127	0.0127	0.0128	0.0128	0.0130	0.0133	0.0136	0.0145
0.0660	0.1250	0.2306	0.2439	0.2589	0.2171	0.1913	0.1740	0.1614	0.1511	0.1260	0.0722	0090∵	J.0624
0.090.0	0.1116	0.2367	0.2535	0.2656	0.2119	0.1814	0.1644	0.1501	0.1373	0.1103	0.0579	0.0445	0.0360
969.0	0.799	1.252	1.199	1.150	0.954	0.926	006:0	0.876	0.851	0.801	0.702	0.602	0.400
	0990.0 0090.0	0.0600 0.0660 0.1116 0.1250	0.0600 0.0660 0.1116 0.1250 0.2367 0.2306	0.0600 0.0660 0.1116 0.1250 0.2367 0.2306 0.2535 0.2439	0.0600 0.0660 0.1116 0.1250 0.2367 0.2306 0.2535 0.2439 0.2656 0.2589	0.0600 0.0660 0.1116 0.1250 0.2367 0.2306 0.2535 0.2439 0.2656 0.2589 0.2119 0.2171	0.0600 0.0660 0.1116 0.1250 0.2367 0.2306 0.2535 0.2439 0.2656 0.2589 0.2119 0.2171 0.1814 0.1913	0.0600 0.0660 0.1116 0.1250 0.2367 0.2306 0.2535 0.2439 0.2656 0.2589 0.2119 0.2171 0.1814 0.1913	0.0600 0.0660 0.1116 0.1250 0.2367 0.2306 0.2535 0.2439 0.2656 0.2589 0.2119 0.2171 0.1814 0.1913 0.1644 0.1740	0.0600 0.0660 0.1116 0.1250 0.2367 0.2306 0.2535 0.2439 0.2656 0.2589 0.2119 0.2171 0.1814 0.1913 0.1644 0.1740 0.1501 0.1614	0.0600 0.0660 0.1116 0.1250 0.2367 0.2306 0.2535 0.2439 0.2656 0.2589 0.2119 0.2171 0.1814 0.1913 0.1501 0.1614 0.1373 0.1511 0.1103 0.1260	0.0600 0.0660 0.1116 0.1250 0.2367 0.2306 0.2535 0.2439 0.2656 0.2589 0.2119 0.2171 0.1814 0.1913 0.1644 0.1740 0.1501 0.1614 0.1373 0.1511 0.1103 0.1260 0.0579 0.0722	0.0600 0.0660 0.1116 0.1250 0.2367 0.2306 0.2535 0.2439 0.2656 0.2589 0.2119 0.2171 0.1814 0.1913 0.1644 0.1740 0.1501 0.1501 0.1501 0.1501 0.1501 0.1501 0.1501 0.0579 0.0722 0.0445 0.00600

Table 8. Pressure and Force Data for Nozzle 5 With $\beta_{l,top/bot} = 17.9^{\circ}/\beta_{l,side} = 0^{\circ}$ and Plume Off

(a) Static pressure coefficients on nozzle top flap

					St	itic pressure	coefficients o	Static pressure coefficients on nozzle top flap at centerline	flap at center	line			
							with value	with values of x/l of-					
M	α, deg	.153	.226	300	.337	114.	.484	.558	.632	.705	622.	.853	.926
1.252	-0.005	-0.011	-0.017	-0.425	-0.522	-0.488	-0.382	-0.169	-0.152	-0.141	-0.129	-0.121	-0.107
1.199	-0.009	-0.012	-0.026	-0.471	-0.577	-0.531	-0.363	-0.185	-0.164	-0.153	-0.143	-0.134	-0.120
1.200	-2.999	-0.016	-0.024	-0.466	-0.577	-0.522	-0.445	-0.201	-0.178	-0.166	-0.158	-0.151	-0.138
1.201	0.012	-0.012	-0.025	-0.467	-0.573	-0.531	-0.374	-0.184	-0.164	-0.151	-0.142	-0.135	-0.120
1.199	2.950	-0.007	-0.028	-0.468	-0.572	-0.544	-0.484	-0.276	-0.197	-0.175	-0.165	-0.154	-0.132
1.199	5.971	-0.010	-0.032	-0.466	-0.571	-0.548	-0.507	-0.383	-0.218	-0.188	-0.177	-0.166	-0.143
1.152	0.004	-0.032	-0.050	-0.524	-0.627	-0.592	-0.314	-0.203	-0.184	-0.172	-0.162	-0.152	-0.141
0.925	-0.239	-0.132	-0.200	-0.571	-0.297	-0.223	-0.195	-0.181	-0.169	-0.156	-0.144	-0.131	-0.117
0.901	0.162	-0.153	-0.229	-0.549	-0.279	-0.216	-0.194	-0.176	-0.161	-0.149	-0.132	-0.116	-0.095
0.877	900'0	-0.170	-0.253	-0.560	-0.282	-0.221	-0.187	-0.164	-0.146	-0.128	-0.110	-0.090	-0.064
0.849	-0.036	-0.190	-0.280	-0.574	-0.278	-0.216	-0.181	-0.155	-0.132	-0.110	-0.085	-0.063	-0.038
0.802	0.014	-0.219	-0.328	-0.663	-0.288	-0.195	-0.145	-0.113	-0.083	-0.059	-0.037	-0.015	0.013
0.702	0.000	-0.298	-0.454	-1.271	-0.604	-0.247	-0.103	-0.018	0.042	0.085	0.118	0.143	0.162
0.603	0.001	-0.325	-0.499	_1.244	-0.556	-0.254	-0.121	-0.038	0.026	0.075	0.119	0.156	0.188
0.600	-3.002	-0.336	-0.521	-1.373	809.0-	-0.291	-0.154	-0.066	0.003	0.058	0.109	0.154	0.194
0.602	0.001	-0.327	-0.501	_1.247	-0.559	-0.257	-0.125	-0.041	0.024	0.074	0.117	0.154	0.185
0.602	2.996	-0.316	-0.483	-1.172	-0.531	-0.242	-0.115	-0.034	0.028	0.077	0.121	0.160	0.194
0.602	800.9	-0.309	-0.477	-1.177	-0.538	-0.252	-0.128	-0.050	0.009	0.056	0.101	0.143	0.188
0.602	8.986	-0.311	-0.485	-1.293	-0.584	-0.286	-0.160	-0.084	-0.026	0.019	0.064	0.112	0.167
0.401	0.001	-0.309	-0.458	-1.011	-0.512	-0.252	-0.131	-0.050	0.011	0.059	0.103	0.142	0.177

Table 8. Continued

(a) Continued

				Stat	Static pressure coefficients on nozzle top flap at $v/Y = 0.50$	pefficients or	nozzle top	lan at $v/Y = 0$	0.50		
						with values of x/l of-	—Jo //x Jo				
W	α, deg	.153	.226	300	.337	114.	.558	.705	6 <i>LL</i>	.853	.926
1 252	5005	-0.005	-0.018	1	-0.522	-0.477	-0.200	-0.134	-0.119	-0.109	-0.103
1 199	6000	9000	-0.028	1	-0.574	-0.520	-0.198	-0.145	-0.132	-0.122	-0.116
1 200	-2.999	0.011	-0.028	1	-0.573	-0.515	-0.228	-0.161	-0.149	-0.138	-0.129
1 201	0.012	-0.006	-0.027		-0.573	-0.520	-0.204	-0.146	-0.134	-0.123	-0.116
1 199	2 950	-0.005	-0.030	ŀ	-0.574	-0.528	-0.305	-0.183	-0.162	-0.144	-0.127
1.100	5 971	-0013	-0.039	1	-0.580	-0.544	-0.346	-0.198	-0.175	-0.156	-0.140
1150	0.004	-0.030	-0.056	,	-0.635	-0.577	-0.210	-0.169	-0.154	-0.143	-0.134
0.005	-0.230	-0.120	-0.200	-	-0.330	-0.240	-0.188	-0.161	-0.148	-0.134	-0.116
000	0 162	-0 142	-0.231	!	-0.324	-0.246	-0.185	-0.154	-0.135	-0.117	-0.095
0.877	9000	-0.159	-0.252	1	-0.313	-0.233	-0.172	-0.130	-0.112	-0.091	-0.067
0.840	-0.036	-0.176	-0.280		-0.325	-0.233	-0.153	-0.104	-0.085	-0.061	-0.038
0.802	0.014	-0.203	-0.323	1	-0.352	-0.214	-0.108	-0.050	-0.029	-0.008	0.013
0 707	0000	-0.269	-0.437		-0.585	-0.232	-0.030	0.073	0.111	0.140	0.159
0.603	0.001	-0.288	-0.469	1	-0.513	-0.236	-0.051	0.053	0.100	0.141	0.175
0090	-3.002	-0.297	-0.490		-0.562	-0.268	-0.072	0.038	0.087	0.136	0.178
0.602	0.001	-0.290	-0.471	1	-0.515	-0.238	-0.053	0.052	0.097	0.140	0.175
0.602	2.996	-0.280	-0.452	1	-0.499	-0.230	-0.052	0.047	0.091	0.134	0.173
0.602	800.9	-0.276	-0.443	1	-0.515	-0.244	-0.071	0.021	0.062	0.107	0.152
0.602	8.986	-0.291	-0.463	ı	-0.554	_0.272	-0.100	-0.018	0.020	0.065	0.117
0.401	0.001	-0.275	-0.432	ı	-0.474	-0.231	-0.059	0.039	0.083	0.126	0.164

Table 8. Continued

(a) Continued

										_												
		.926	-0.147	-0.152	-0.154	-0.155	-0.181	-0.254	-0.168	-0.112	-0.084	-0.058	-0.030	0.014	0.125	0.123	0.120	0.122	0.085	0.022	0.002	0.105
		.853	-0.153	-0.157	-0.161	-0.160	-0.235	-0.295	-0.171	-0.127	-0.105	-0.079	-0.052	-0.005	0.099	0.087	0.082	0.086	0.058	-0.003	-0.049	0.071
0.75		.779	-0.170	-0.174	-0.180	-0.177	-0.261	-0.310	-0.186	-0.144	-0.126	-0.100	-0.073	-0.025	090'0	0.041	0.034	0.039	0.022	-0.027	-0.073	0.025
Static pressure coefficients on nozzle top flap at $y/Y = 0.75$.705	-0.199	-0.196	-0.202	-0.202	-0.289	-0.325	-0.203	-0.154	-0.139	-0.115	-0.090	-0.041	0.021	0.001	-0.005	-0.002	-0.012	-0.046	-0.081	-0.012
n nozzle top	of x// of—	.558	-0.302	-0.323	-0.325	-0.327	-0.348	-0.347	-0.334	-0.183	-0.176	-0.155	-0.136	-0.089	-0.076	-0.090	-0.093	-0.092	-0.096	-0.111	-0.126	-0.088
oefficients or	with values of x/l of-	.411	-0.338	-0.366	-0.390	-0.364	-0.360	-0.375	-0.412	-0.246	-0.251	-0.236	-0.228	-0.194	-0.235	-0.236	-0.246	-0.238	-0.233	-0.235	-0.234	-0.222
tic pressure c		.337	-0.510	-0.554	-0.563	-0.554	-0.560	-0.568	-0.614	-0.354	-0.355	-0.349	-0.369	-0.393	-0.470	-0.444	-0.479	-0.446	-0.415	-0.404	-0.405	-0.405
Sta		.300	-0.416	-0.460	-0.449	-0.458	-0.476	-0.483	-0.516	-0.629	-0.635	-0.647	-0.703	-0.852	-1.134	-0.953	-1.109	-0.951	-0.841	-0.865	-0.898	-0.796
		.226	0.013	-0.020	-0.021	-0.022	-0.035	-0.053	-0.049	-0.187	-0.216	-0.239	-0.261	-0.300	-0.378	_0.382	-0.396	-0.385	-0.370	-0.376	-0.394	-0.355
		.153	-0.012	-0.014	-0.020	-0.013	-0.023	-0.040	-0.035	-0.124	-0.146	-0.160	-0.175	-0.200	-0.245	-0.255	-0.260	-0.257	-0.256	-0.266	-0.281	-0.243
		α, deg	-0.005	-0.009	-2.999	0.012	2.950	5.971	0.004	-0.239	0.162	9000	-0.036	0.014	0.000	0.001	-3.002	0.001	2.996	800.9	8.986	0.001
		M_{∞}	1.252	1.199	1.200	1.201	1.199	1.199	1.152	0.925	0.901	0.877	0.849	0.802	0.702	0.603	0.600	0.602	0.602	0.602	0.602	0.401

Table 8. Continued
(a) Concluded

				Stati	Static pressure coefficients on nozzle top flap at $y/Y = 0.875$	efficients on	nozzle top f	lap at $y/Y = 0$.875		
						with values of x/l of-	—Jo //x Jo :				
M	a, deg	.153	.226	300	.337	.411	.558	.705	.779	.853	.926
1 252	-0.005	10.004	-0.014	-0.324	-0.316	-0.336	-0.395	-0.433	-0.453	-0.411	-0.357
1 199	600.0	-0.007	-0.021	-0.355	-0.342	-0.370	-0.427	-0.449	-0.451	-0.381	-0.337
1 200	-2.999		-0.020	-0.386	-0.383	-0.333	-0.383	-0.348	-0.317	-0.276	-0.236
1 201	0.012		-0.021	-0.352	-0.339	-0.368	-0.428	-0.452	-0.456	-0.391	-0.344
1 199	2.950	-0.013	-0.040	-0.337	-0.324	-0.357	-0.453	-0.594	-0.667	-0.632	-0.476
1 199	5 971	-0.026	-0.054	-0.341	-0.324	-0.348	-0.460	-0.660	-0.739	-0.689	-0.464
1.152	0.004	-0.032	-0.049	-0.403	-0.386	-0.417	-0.457	-0.466	-0.472	-0.396	-0.355
0.925	-0.239	-0.117	-0.180	-0.654	-0.327	-0.226	-0.177	-0.152	-0.140	-0.125	-0.109
1060	0.162	-	-0.210	-0.654	-0.330	-0.229	-0.172	-0.144	-0.128	-0.111	-0.089
0.877	0.00		-0.229	-0.665	-0.320	-0.218	-0.156	-0.128	-0.114	-0.095	-0.073
0.840	9600-	-0.162	-0.249	-0.690	-0.337	-0.225	-0.145	-0.119	-0.104	-0.082	-0.057
0.80	0.014		-0.277	-0.701	-0.380	-0.242	-0.129	-0.107	-0.093	-0.074	-0.043
0.707	0000	-0.214	-0.326	-0.725	-0.485	-0.351	-0.177	-0.135	-0.130	-0.115	-0.062
0,603	000		-0.320	-0.643	-0.453	-0.347	-0.192	-0.147	-0.146	-0.137	-0.088
0090	-3.002		-0.323	-0.699	-0.446	-0.323	-0.176	-0.082	-0.048	-0.016	0.030
090	1000	-0.217	-0.322	-0.644	-0.456	-0.350	-0.195	-0.149	-0.151	-0.142	-0.093
0,607	2 996	-0.227	-0.329	-0.603	-0.444	-0.349	-0.225	-0.211	-0.209	-0.183	-0.090
0,000	8009	-0.235	-0.335	-0.569	-0.421	-0.327	-0.279	-0.260	-0.221	-0.135	900.0
0,602	8 986	-0.246	-0.340	-0.565	-0.409	-0.321	-0.344	-0.307	-0.242	-0.135	0.023
0.007	1000	-0.203	-0.296	-0.566	-0.410	-0.320	-0.190	-0.144	-0.144	-0.140	-0.106
1		2020	2 2210								

Table 8. Continued

(b) Static pressure coefficients on nozzle sidewall

				Static pres	sure coeffici	Static pressure coefficients on corner between nozzle top flap and sidewall with values of x/l of—	is on comer between not with values of x/l of—	zle top flap a	ind sidewall		
M _∞	α, deg	.153	.226	.300	.337	.411	.558	705	977.	.853	.926
1.252	-0.005	-0.005	-0.017	-0.215	-0.212	-0.273	-0.426	-0.567	-0.493	-0.401	7330
1.199	-0.009	-0.005	-0.025	-0.236	-0.239	-0.303	-0.463	-0.596	-0.494	-0 391	-0.375
1.200	-2.999	-0.018	-0.025	-0.255	-0.236	-0.259	-0.371	-0.508	-0.530	-0.428	-0 350
1.201	0.012	-0.004	-0.023	-0.235	-0.239	-0.301	-0.464	-0.598	-0.503	-0.399	-0.331
1.199	2.950	-0.015	-0.041	-0.248	-0.266	-0.350	-0.561	-0.635	-0.576	-0.485	-0.332
1.199	5.971	-0.029	-0.057	-0.249	-0.280	-0.389	-0.649	-0.628	-0.578	-0.502	-0.350
1.152	0.004	-0.033	-0.054	-0.279	-0.277	-0.344	-0.497	-0.613	-0.500	-0.401	-0.336
0.925	-0.239	-0.116	-0.185	-0.501	-0.375	-0.269	-0.174	-0.139	-0.135	-0.120	-0.103
0.901	0.162	-0.135	-0.212	-0.524	-0.377	-0.261	-0.183	-0.147	-0.131	-0.109	-0.081
0.877	0.006	-0.148	-0.229	-0.524	-0.354	-0.254	-0.193	-0.138	-0.119	-0.088	-0.059
0.849	-0.036	-0.160	-0.247	-0.514	-0.349	-0.267	-0.202	-0.137	-0.111	-0.075	-0.038
0.802	0.014	-0.173	-0.263	-0.491	-0.364	-0.290	-0.218	-0.135	-0.097	-0.051	-0.005
0.702	0.000	-0.195	-0.289	-0.504	-0.418	-0.370	-0.318	-0.232	-0.171	-0.077	0.029
0.603	0.001	-0.191	-0.278	-0.458	-0.388	-0.357	-0.332	-0.272	-0.227	-0.134	0.001
0.600	-3.002	-0.195	-0.281	-0.451	-0.350	-0.296	-0.248	-0.192	-0.158	-0.096	0.007
0.602	0.001	-0.193	-0.280	-0.461	-0.392	-0.362	-0.336	-0.278	-0.233	-0.139	-0.003
0.602	2.996	-0.213	-0.302	-0.490	-0.439	-0.433	-0.427	-0.339	-0.258	-0.119	0.022
0.602	6.008	-0.239	-0.332	-0.521	-0.481	-0.491	-0.481	-0.322	-0.210	-0.073	0.045
0.602	8.986	-0.247	-0.342	-0.503	-0.471	-0.486	-0.454	-0.269	-0.174	-0.058	0.060
0.401	0.001	-0.178	-0.259	-0.408	-0.352	-0.331	-0.317	-D 283	0 240	9910	0000

Table 8. Continued (b) Continued

				Sta	Static pressure coefficients on nozzle sidewall at $z/Z = 0.50$	pefficients or	nozzle side	wall at $z/Z = 0$	0.50		
					•	with value	with values of x/l of-				
M	α, deg	.153	.226	300	.337	.411	.558	.705	622.	.853	.926
1.252	-0.005	1		-0.044	-0.068	-0.106	-0.196	-0.280	-0.319	1	-0.332
1 199	-0.009	ı	1	-0.064	-0.093	-0.132	-0.231	-0.320	-0.359	ı	-0.346
1.200	-2.999		1	-0.062	-0.086	-0.118	-0.204	-0.289	-0.327	1	-0.350
1.201	0.012	-	1	-0.062	-0.090	-0.131	-0.230	-0.320	-0.358	1	-0.352
1 100	2.950	-	1	-0.070	-0.103	-0.152	-0.253	-0.343	-0.376	ı	-0.388
1.199	5.971	1	ı	-0.084	-0.119	-0.175	-0.271	-0.357	-0.388	l	-0.413
1.152	0.004	1	ı	-0.097	-0.128	-0.170	-0.251	-0.331	-0.375	,	-0.356
0.925	-0.239	-		-0.260	-0.294	-0.299	-0.212	-0.129	-0.117	ı	-0.083
0.901	0.162	1		-0.282	-0.310	-0.277	-0.175	-0.135	-0.115	I	-0.066
0.877	0.006	1	1	-0.283	-0.283	-0.235	-0.172	-0.128	-0.104	ı	-0.0 4
0.849	-0.036	ı	1	-0.270	-0.263	-0.222	-0.170	-0.119	-0.091	1	-0.022
0.802	0.014	ı		-0.253	-0.245	-0.217	-0.164	-0.108	-0.077		0.004
0.702	0000	ı	-	-0.237	-0.234	-0.213	-0.170	-0.108	-0.069	Į.	0.044
0.603	0.001	1	1	-0.213	-0.209	-0.196	-0.164	-0.113	-0.080	1	0.036
0.600	-3.002			-0.206	-0.196	-0.176	-0.137	-0.087	-0.054	ı	0.050
0.602	0.001	ı	-	-0.217	-0.213	-0.199	-0.167	-0.118	_0.083	1	0.033
0.602	2.996	ı	1	-0.239	-0.240	-0.232	-0.205	-0.154	-0.112	1	0.031
0.602	8009	1	1	-0.270	-0.276	-0.273	-0.251	-0.193	-0.140	ı	0.031
0.602	8.986	1	ı	-0.303	-0.311	-0.315	-0.296	-0.231	-0.169	l .	0.031
0.401	0.001	1	-	-0.188	-0.189	-0.179	-0.153	-0.114	-0.087	I	0.022
	2220										

Table 8. Continued

(b) Continued

	\neg	Т	_	_	_	_	_	_		_		_	- -	_	_	_	_	_		_			
	926	0 2 3 3 0	-0.339	-0.555	0.338	-0.338	-0.384	-0.385	-0.364	-0.081	-0.063	50045	3000	0.023	100.0	0.050	0.049	0.055	0.047	0.050	20.0		6.65
	.853	0.331	0.367	0.366	0.350	-0.301	-0.300	-0.333	-0.378	-0.108	-0.097	-0.082	0.067	1900	0000	-0.008	-0.012	-0.010	D 014	5004	0.010	000	670.0
	971.	1 36 0	0.201	0.323	0.314	0.320	0.510	-0.311	-0.336	-0.124	-0.121	0.110	000	1000	-0.00	-0.050	-0.052	-0.052	-0.054	-0.057	-0.065	0800	0.056
ine	.705	CPC 0	0.281	0.220	0.270	0 277	0.270	0.270	-0.289	-0.137	-0.140	-0.132	-0123	1110	1100		-0.082	-0.083	-0.084	-0.087	660 0	2117	080
Static pressure coefficients on nozzle sidewall at centerline with values of x/l of—	.632	-0 202	-0.337	0.230	0.230	0.230	10.00	777.0	-0.244	-0.172	-0.159	-0.152	-0.145	5136	251.0	-0.11.5	-0.108	-0.110	 - - - -	-0.114	-0.127	-0.145	50103
nozzle sidev	.558	-0.157	-0 195	819	-0.194	1961	0.102	0.130	-0.209	-0.247	-0.183	-0.175	-0.169	51.6	01.0	2.1.0	-0.129	-0.131	-0.131	-0.135	-0.148	-0.167	8119
pefficients on nozzle sid with values of x/l of—	.484	-0.115	-0.142	-0.136	-0.141	144	8710	01.10	8/1.7	-0.306	-0.235	-0.200	-0.192	-0.183	0 150	00.10	-0.145	-0.147	-0.147	-0.151	-0.162	-0.181	-0.128
ic pressure co	.411	-0.068	-0.093	-0.086	0.09	-0.093	20102	0.131	10.131	-0.305	-0.289	-0.240	-0.218	-0.203	0 178		٦ ا	-0.159	-0.159	-0.162	-0.174	-0.192	-0.137
Stat	.337	-0.027	-0.049	-0.043	-0.047	-0.051	70.067	0000	70.007	-0.253	-0.268	-0.253	-0.232	-0.214	184		\$ 1.0	-0.167	-0.166	-0.169	-0.180	-0.198	-0.140
	.300	-0.010	-0.030	-0.024	-0.027	-0.032	-0.050	1900	3.5	-0.215	-0.235	-0.235	-0.224	-0.207	281 0	1710	-0.101		-0.163	-0.167	-0.178	-0.196	-0.141
	.226	0.004	-0.012	-0.008	-0.011	-0.020	-0.040	129	150	1	1	-0.182	-0.186	-0.184	-0.168	0310	0.1.0	-0.155	-0.152	-0.156	-0.168	-0.188	-0.131
	.153	1	-	-	l		,			<u> </u>	-	1	1	1	1			1	1	1	ı	1	1
	α, deg	-0.005	-0.009	-2.999	0.012	2.950	5.971	0.004	0 230	-0.239	0.162	0.006	-0.036	0.014	0.000	1000	180	-3.002	0.001	2.996	800.9	986.8	0.001
	M _∞	1.252	1.199	1.200	1.201	1.199	1.199	1.152	2000	0.72	105.0	0.877	0.849	0.802	0.702	0,603	200	0.000	0.602	0.602	0.602	0.602	0.401

Table 8. Continued

(b) Concluded

+	1	-0.343	-0.358	-0.356	-0.406	-0.395	-0.374	12	4	9	Q	6	္ဌ	္ဓါ	<u>∞</u>	اي	اي	∞	22	∞
50/		Ī	- 1			۲	Ġ	-0.112	-0.094	-0.076	-0.060	-0.039	0.030	0.030	0.028	0.026	0.036	0.038	0.032	0.018
- 1	-0.277	-0.319	-0.334	-0.316	-0.289	-0.262	-0.329	-0.180	-0.181	-0.177	-0.171	-0.162	-0.119	-0.110	-0.144	-0.112	-0.089	-0.079	-0.085	9.11
866.	-0.196	-0.232	-0.249	-0.229	-0.209	-0.188	-0.254	-0.298	-0.219	-0.216	-0.215	-0.209	-0.174	-0.158	-0.196	-0.161	-0.138	-0.128	-0.133	-0.149
.411	401.04	-0.134	-0.145	-0.131	-0.126	-0.134	-0.173	-0.366	-0.353	-0.293	-0.265	-0.255	-0.216	-0.190	-0.223	-0.192	-0.174	-0.167	-0.173	-0.168
.337	-0.061	-0.083	-0.086	-0.082	-0.086	-0.107	-0.120	-0.302	-0.323	-0.315	-0.294	-0.273	-0.228	-0.200	-0.226	-0.202	-0.190	-0.188	-0.198	-0.170
.300	-0.042	-0.066	-0.064	-0.063	-0.069	-0.094	-0.097	-0.261	-0.283	-0.290	-0.288	-0.273	-0.232	-0.205	-0.227	-0.207	661.0-	-0.202	-0.216	-0.177
.226	_	_	_	1		1	1	1	-		-			1	1	1	-	1	-	
.153	0.010	-0.009	-0.007	9000-	-0.021	-0.055	-0.036	-0.114	-0.130	-0.139	-0.153	-0.162	-0.163	-0.151	-0.162	-0.154	-0.161	-0.187	-0.228	-0130
α, deg	-0.005	-0.009	-2.999	0.012	2.950	5.971	9000	-0.239	0.162	9000	-0.036	0.014	000.0	0.001	-3.002	0.001	2.996	900.9	8.986	0.00
M∞	1.252	1.199	1.200	1.201	1 199	661	1.152	0.925	1060	0.877	0.849	0.802	0.702	0.603	009.0	0.602	0.602	0.602	0.602	0.401
	α, deg .153 .226 .300 .357 .411 .350	a, deg .153 .226 .300 .337 .411 .330 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196	a, deg .153 .226 .300 .337 .411 .330 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196 -0.009 - -0.066 -0.083 -0.134 -0.232	a, deg .153 .220 .300 .337 .411 .330 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196 -0.009 - -0.066 -0.083 -0.134 -0.232 -2.999 -0.007 - -0.064 -0.086 -0.145 -0.249	a, deg .153 .220 .300 .337 .411	a, deg .153 .220 .300 .337 .411 .330 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196 -0.009 - 0.066 -0.083 -0.134 -0.232 -2.999 -0.007 - -0.064 -0.086 -0.145 -0.249 0.012 -0.006 - -0.063 -0.031 -0.229 -0.229 2.950 -0.021 - -0.069 -0.086 -0.126 -0.209	a, deg .153 .220 .300 .337 .411 .330 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196 -0.009 - -0.066 -0.083 -0.134 -0.232 -2.999 -0.007 - -0.064 -0.086 -0.145 -0.249 0.012 -0.006 - -0.063 -0.082 -0.131 -0.229 2.950 -0.021 - -0.069 -0.086 -0.126 -0.209 5.971 -0.055 - -0.094 -0.107 -0.134 -0.188	a, deg .153 .226 .300 .337 .411 .339 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196 -0.009 - -0.066 -0.083 -0.134 -0.232 -2.999 -0.007 - -0.064 -0.086 -0.145 -0.249 0.012 -0.006 - -0.063 -0.082 -0.131 -0.229 2.950 -0.021 - -0.069 -0.086 -0.131 -0.209 5.971 -0.055 - -0.094 -0.107 -0.134 -0.188 0.004 -0.036 - -0.094 -0.107 -0.134 -0.188	a, deg .153 .226 .300 .337 .411 .330 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196 -0.009 -0.009 - -0.066 -0.083 -0.134 -0.232 -2.999 -0.007 - -0.064 -0.086 -0.145 -0.249 0.012 -0.006 - -0.063 -0.082 -0.131 -0.229 2.950 -0.021 - -0.069 -0.086 -0.126 -0.209 5.971 -0.055 - -0.094 -0.107 -0.134 -0.188 0.004 -0.036 - -0.097 -0.120 -0.18 -0.239 -0.114 - -0.261 -0.302 -0.296	a, deg .153 .22b .300 .337 .411 .330 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196 -0.009 -0.009 - -0.066 -0.083 -0.134 -0.232 -2.999 -0.007 - -0.064 -0.086 -0.145 -0.249 0.012 -0.006 - -0.063 -0.082 -0.131 -0.229 2.950 -0.021 - -0.069 -0.086 -0.126 -0.209 5.971 -0.055 - -0.094 -0.107 -0.134 -0.188 5.971 -0.035 - -0.097 -0.120 -0.18 -0.18 0.004 -0.036 - -0.097 -0.130 -0.254 -0.239 -0.114 - -0.261 -0.302 -0.366 -0.298 -0.162 -0.233 -0.353 -0.219	a, deg .153 .226 .300 .337 .411 .330 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196 -0.009 - -0.066 -0.083 -0.134 -0.232 -2.999 -0.007 - -0.064 -0.086 -0.145 -0.249 0.012 -0.006 - -0.063 -0.082 -0.131 -0.229 2.950 -0.021 - -0.069 -0.086 -0.136 -0.209 2.950 -0.021 - -0.094 -0.107 -0.134 -0.188 5.971 -0.055 - -0.094 -0.107 -0.134 -0.188 0.004 -0.036 - -0.097 -0.120 -0.134 -0.254 -0.239 -0.130 - -0.261 -0.302 -0.366 -0.298 0.006 -0.033 - -0.283 -0.333 -0.219 0.007 -0.130 - -0.293	a, deg .153 .226 .300 .337 .411 .330 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196 -0.009 - -0.066 -0.083 -0.134 -0.232 -2.999 -0.007 - -0.064 -0.086 -0.145 -0.249 0.012 -0.006 - -0.063 -0.085 -0.131 -0.229 2.950 -0.021 - -0.069 -0.086 -0.136 -0.209 5.971 -0.055 - -0.094 -0.107 -0.134 -0.188 0.004 -0.036 - -0.097 -0.120 -0.188 0.029 -0.130 - -0.097 -0.130 -0.254 0.026 -0.130 - -0.261 -0.302 -0.296 0.006 -0.130 - -0.281 -0.293 -0.216 0.036 -0.139 - -0.290 -0.293 -0.216 <td< td=""><td>a, deg .153 .226 .300 .337 .411 .330 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196 -0.009 - -0.066 -0.083 -0.134 -0.232 -2.999 -0.007 - -0.064 -0.086 -0.145 -0.249 0.012 -0.006 - -0.063 -0.085 -0.131 -0.229 2.950 -0.021 - -0.069 -0.086 -0.136 -0.209 2.950 -0.021 - -0.094 -0.107 -0.134 -0.188 5.971 -0.055 - -0.094 -0.107 -0.134 -0.188 0.004 -0.036 - -0.097 -0.120 -0.134 -0.254 0.162 -0.130 - -0.261 -0.302 -0.296 -0.298 0.006 -0.130 - -0.283 -0.353 -0.219 0.006 -0.136 - -0.294</td><td>a, deg .153 .226 .300 .337 .411 .330 -0.005 0.010 - -0.042 -0.061 -0.104 -0.196 -0.009 -0.009 - -0.066 -0.083 -0.134 -0.232 -2.999 -0.007 - -0.064 -0.086 -0.145 -0.249 0.012 -0.006 - -0.063 -0.082 -0.131 -0.229 2.950 -0.021 - -0.069 -0.086 -0.136 -0.209 2.950 -0.031 - -0.094 -0.107 -0.134 -0.188 2.971 -0.055 - -0.094 -0.107 -0.134 -0.188 0.004 -0.036 - -0.094 -0.107 -0.134 -0.254 0.162 -0.130 - -0.261 -0.209 -0.266 -0.298 0.162 -0.130 - -0.291 -0.353 -0.216 -0.036 -0.153 -</td><td>a, deg .153 .226 .300 .337 .411 .330 -0.005 0.010 - 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Table 8. Continued

(c) Static pressure coefficients on nozzle bottom flap

Г	T	П				Т	Т	Т	Т	Т	Т		Т	Т	Т	T	П	Т	Т	Т	T	т
	Š	97.6	-0.362	-0.331	-0.400	-0.341	-0.258	-0.264	-0.369	-0.160	-0.148	-0.162	-0.179	-0.210	-0.088	-0.074	-0.093	-0.078	0.031	0.068	0.071	100
	Cito	.833	-	1	-				-	-	1	1	1	'	ı			1	ı	1		
0.875	000	6//:	-0.467	-0.511	-0.683	-0.509	-0.390	-0.367	-0.543	-0.218	-0.203	-0.210	-0.220	-0.235	-0.154	-0.133	-0.212	-0.136	-0.048	-0.018	-0.014	
flap at y/Y =	302	co/.	-0.424	-0.471	-0.565	-0.469	-0.395	-0.360	-0.499	-0.239	-0.217	-0.218	-0.219	-0.220	-0.153	-0.135	-0.209	-0.138	-0.080	-0.059	-0.054	
ozzle bottom	Jo /// Jo	8.C.	-0.361	-0.405	-0.425	-0.402	-0.373	-0.338	-0.440	-0.288	-0.253	-0.248	-0.248	-0.256	-0.200	-0.185	-0.218	-0.188	-0.172	-0.154	-0.141	11.0
ficients on n	with values of x/l of-	2000	-0.339	-0.380	-0.352	-0.379	-0.352	-0.331	-0.429	-0.421	-0.366	-0.351	-0.358	-0.404	-0.369	-0.339	-0.336	-0.341	-0.320	-0.288	-0.266	0000
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.875$ with values of x/l of—	337	755.0	-0.32/	-0.367	-0.332	-0.366	-0.408	-0.449	-0.414	-0.557	-0.526	-0.515	-0.522	-0.549	-0.505	-0.450	-0.433	-0.452	-0.444	-0.425	-0.417	0.403
	300	ooc.	-		-	-	I	ļ	1	-		_		_		1	-	_		-	1	
	326	2000	70.0-	-0.030	-0.046	-0.029	-0.031	-0.059	-0.058	-0.200	-0.220	-0.244	-0.266	-0.300	-0.337	-0.323	-0.328	-0.324	-0.328	-0.342	-0.367	20%
	153	0000	0.009	-0.009	-0.011	-0.008	-0.024	-0.052	-0.033	-0.123	-0.142	-0.154	-0.172	-0.192	-0.216	-0.211	-0.223	-0.213	-0.215	-0.232	-0.262	199
	α dea	0.005	500.0	-0.009	-2.999	0.012	2.950	5.971	0.004	-0.239	0.162	9000	-0.036	0.014	0.000	0.001	-3.002	0.001	2.996	900.9	8.986	1000
	M	CSC 1	2071	1.199	1.200	1.201	1.199	1.199	1.152	0.925	0.901	0.877	0.849	0.802	0.702	0.603	0.600	0.602	0.602	0.602	0.602	0.401

Table 8. Continued

(c) Continued

					Static pressu	re on nozzle bottom fla	Static pressure on nozzle bottom flap at $y/Y = 0.50$	at $y/Y = 0.50$			
M	α, deg	.153	.226	.300	.337	.411	.558	.705	<i>6LL</i> :	.853	.926
1.252	-0.005	900.0	-0.006	-0.460	-0.526	-0.485	-0.396	-0.338	-0.326	-0.301	-0.174
1.199	-0.009	-0.012	-0.027	-0.513	-0.579	-0.528	-0.431	-0.368	-0.349	-0.283	-0.148
1.200	-2.999	-0.007	-0.025	-0.512	-0.580	-0.537	-0.420	-0.372	-0.361	-0.351	-0.251
1.201	0.012	-0.010	-0.027	-0.511	-0.577	-0.527	-0.432	-0.370	-0.353	-0.288	-0.149
1.199	2.950	-0.015	-0.027	-0.505	-0.573	-0.525	-0.420	-0.198	-0.164	-0.144	-0.125
1.199	5.971	-0.015	-0.023	-0.500	-0.572	-0.524	-0.488	-0.234	-0.184	-0.159	-0.137
1.152	0.004	-0.037	-0.056	-0.575	-0.642	-0.588	-0.467	-0.353	-0.298	-0.208	-0.141
0.925	-0.239	-0.134	-0.208	-0.774	-0.541	-0.403	-0.295	-0.226	-0.190	-0.152	-0.115
0.901	0.162	-0.155	-0.235	-0.745	-0.496	-0.378	-0.281	-0.201	-0.166	-0.128	-0.091
0.877	9000	-0.171	-0.259	-0.754	-0.491	-0.375	-0.258	-0.170	-0.130	-0.091	-0.056
0.849	-0.036	-0.190	-0.290	-0.794	-0.511	-0.381	-0.238	-0.135	-0.091	-0.052	-0.017
0.802	0.014	-0.225	-0.342	-0.939	-0.607	-0.406	-0.196	-0.072	-0.027	0.012	0.043
0.702	0.000	-0.281	-0.443	-1.240	-0.594	-0.260	-0.069	0.033	0.077	0.115	0.149
0.603	0.001	-0.291	-0.459	-1.073	-0.488	-0.231	-0.059	0.046	0.092	0.136	0.173
0.600	-3.002	-0.281	-0.440	-1.028	-0.470	-0.223	-0.061	0.037	0.079	0.122	0.165
0.602	0.001	-0.293	-0.460	-1.074	-0.489	-0.232	190.0-	0.045	0.091	0.135	0.172
0.602	2.996	-0.299	-0.478	-1.195	-0.534	-0.261	-0.083	0.026	0.075	0.123	0.168
0.602	900.9	-0.299	-0.485	-1.309	-0.567	-0.285	-0.104	9000	0.055	0.104	0.154
0.602	8.986	-0.291	-0.483	-1.397	-0.592	-0.304	-0.123	-0.015	0.033	0.083	0.134
0.401	0.001	-0.278	-0.423	-0.898	-0.450	-0.225	-0.063	0.036	0.081	0.122	0.161

Table 8. Continued

(c) Concluded

with values of x/l of—	.411 .558 .705 .926	-0.481 -0.474 -0.460 -0.097	-0.527 -0.517 -0.471 -0.105	-0.528	-0.527 -0.516 -0.474 -0.108	-0.528 -0.374 -0.199 -0.140	-0.526 -0.494 -0.214 -0.152	-0.588 -0.545 -0.334 -0.133	-0.393 -0.296 -0.232 -0.121	-0.369 -0.284 -0.207 -0.099	-0.363 -0.258 -0.176 -0.059	-0.371 -0.237 -0.140 -0.021	-0.399 -0.198 -0.080 0.035	-0.284 -0.065 0.042 0.155	-0.258	-0.244 -0.051 0.055 0.181	-0.260	-0.290	-0.315 -0.107 0.014 0.175	-0.332 -0.126 -0.005 0.166	
10	.153 .226	0.006 -0.016	-0.017 -0.039	-0.010 -0.035	-0.016 -0.039	-0.021 -0.042	-0.018 -0.038	-0.038 -0.066	-0.138 -0.218	-0.159 -0.242	-0.176 -0.267	-0.197 -0.298	-0.234 -0.357	-0.301 -0.467	-0.316 -0.481	-0.306 -0.466	-0.318 -0.483	-0.327 -0.503	-0.330 -0.513	-0.324 -0.515	
	M_{∞} α , deg	1.252 -0.005	1.199 -0.009	1.200 –2.999	1.201 0.012	1.199 2.950	1.199 5.971	1.152 0.004	0.925 -0.239	0.901 0.162	0.877 0.006	0.849 -0.036	0.802 0.014	0.702 0.000	0.603 0.001	0.600 -3.002	0.602 0.001	0.602 2.996	0.602 6.008	0.602 8.986	

Table 8. Concluded

(d) Force data

c_D	0.2862	0.3066	0.3252	0.3065	0.2955	0.3155	0.3186	0.2122	0.1949	0.1835	0.1704	0.1473	0.0970	0.0853	0.0935	0.0861	0.0927	0.1095	0.1335	0.0824
α, deg	-0.005	-0.009	-2.999	0.012	2.950	5.971	0.004	-0.239	0.162	900.0	-0.036	0.014	0.000	0.001	-3.002	0.001	2.996	800.9	8.986	0.001
M	1.252	1.199	1.200	1.201	1.199	1.199	1.152	0.925	0.901	0.877	0.849	0.802	0.702	0.603	0.600	0.602	0.602	0.602	0.602	0.401

Table 9. Pressure and Force Data for Nozzle 6 With $\beta_{t,top/bot} = 17.3^{\circ}/\beta_{t,side} = 9.7^{\circ}$ and Plume Off

(a) Static pressure coefficients on nozzle top flap

		700	076.	-0.097	0113	-6.113	000 0	0.020	-0.068 -	0 00	CC0.0-	-0.038	000	20.0	6210	0.1/5	0.170	27.0
		053	cco.	— ————————————————————————————————————	0010	071.0	<u>د</u> ا	0.110	7667	7000	-0.000	080	0000	750.04	0710	0.147	0 146	0.131
		770	211.	-0.123	0140	7.140	0.140		= = = = =	V110	-V.114	-0.121	0.063	0.00	2010	0.143	0110	0110
	ine	705	20,1		154	÷.1.5	0.154	1010	-0.12/	0.141		-0.161	0 00	70.00	2000	2000	0.087	0.087
	lap at centerl	632	2500	7.138	1710	1 / 1:5	-0.167	277	-0.142	J 160	2:10	-0.201	2010	, 2,	0.046	2	0.033	0.030
	nozzle top f	558	3000	-0.793	-0.259	1	181.0	T	7.1.7	5		-0.236	5 120	1	-00		-0.028	2009
	Static pressure coefficients on nozzle top flap at centerline with values of y/l of—	484	0770	0.440	-0.476		661.7	174	1.7	-0.211		-0.268	0910		0.103	3	7.13	-0.122
	ic pressure co	411	0.470	0/+/0	-0.532	300	-0.228	901	,,,,	-0.235	200	-0.303	-0.199		-0.248	2500	CC7.0	-0.248
0	Stat	.337	805 0	2000	-0.560	000	-0.308	0920-		-0.599	2000	_0.393	-0.263		-0.633	0.577	7/2	-0.512
	ĺ	.300	70.357		-0.395	7070	-0.000	-0.623		7.656	0.750	20.70	-0.657		-1.392	4111	/11.1-	-0.885
		.226	4100		-0.022	000	W.200	-0.216	300	-0.229	0 224	4.6.7	-0.269	2000	-0.430	7 455	1	-0.412
		.153	9000	0000	-0.008	0.10	0.127	-0.141	151	101.0	0 158	0.1.70	-0.178	0000	7.703	796		-0.268
		α, deg	-0.028	0100	-0.0/0	7 00 7	2:027	-0.029	3.010	3.010	6.012	1000	-0.063	0.00	700.0	250		-0.006
		M_{∞}	1.252	, 200	1.202	000		0.901	0000	0.500	0000	2000	0.830	0.707	70.10	09.0		0.399

		-	926	2000	SS-0-	-0.111		080.0	0.067	25.5	01/0	2.5	0.030	0000	33.9	2710	0.173	9210	0/1:0	97.0
			853	2110	7117	8610	25.0	-0.118	0000	2.02	C80 0	7000	1,00	2000	0.030	0.157	0.134	0 140		
	0.50		677.	1010	-0.121	0 140		-0.139	7115	0.113	7110	0.1.0	2 2 7	0.00	0.00	0 118	0.110	0.107	2000	2
	Static pressure coefficients on nozzle top flap at $y/Y = 0.50$.705	0.139	0.1.0	-0.155	23.0	10.137	CEI 0-	701.0	-0 144		-0.159	7000	10.00	5800	2000	0.073	0.00	-
	n nozzle top	with values of x/l of—	.558	0 332	2.0.0	-0.323	701.0	5.174	-0.167		0010		-0.241	0.132	701.0	0100		-0.020	0.010	
	oefficients o	with value	.411	-0.460) Aria	-0.520	0360	0.2.0	-0.226		-0.271		-0.34	8160	2:510	-0.225		-0.226	0.00	27.7
	ne pressure o		.337	508		-0.560	998 0	200.0	0.309		-0.371		-0.481	-0.314		-0,605		165.0	504	֭֭֭֭֓֞֝֝֝֜֜֝֜֜֜֝֓֓֓֜֜֜֜֜֜֜֓֓֓֓֓֜֜֜֜֜֓֓֓֡֡֜֜֜֡֡֡֡֓֜֜֡֡֡֡֓֡֡֡֡
·	Sta		300	-0.340		0.384	744		989.0	9.50	-0.742	010	-0.819	-0.730		-1.372	500	-1.083	5980-	3
			.226	-0.008		-0.018	J 189		-0.206	0.00	-0.219	0.021	167.0-	-0.259		-0.411	0070	-0.422	-0.384	
			.153	0.001	900	-0.008	-0.124		-0.134	2710	-0.14/	0.161	101.0	-0.171		-0.703	0300	-0.209	-0.244	
		•	α, deg	-0.028	0.070	77.070	-3.024	000	-0.029	2.010	3.018	6.012	710.0	-0.063	0,000	-0.002	7000	30.0	9000	
		-	M∞	1.252	1 200	1.202	0.905	200	0.501	200	0.700	0 800	6.0.0	0.850	202	0.702	1090	20.0	0.399	

Table 9. Continued

(a) Concluded

				ŀ				- A/ ** B	0.75		
·				Sta	Static pressure coefficients on nozzie top trap at $y(t) = 0.7.7$ with values of x/l of—	oerricients of with values	with values of x/l of—	iiap ai <i>yi I</i> =	0.70		
2	n dea	153	.226	300	.337	.411	.558	705	6LL:	.853	.926
1 252	0.008	000	2000	-0.340	-0.512	-0.402	-0.316	-0.165	-0.122	-0.108	-0.091
2021	0.020	8000	-0015	-0.387	-0.567	-0.438	-0.342	-0.170	-0.139	-0.121	-0.104
2027	3.007	0.120	71.0	-0.783	-0.417	-0.279	-0.201	-0.160	-0.142	-0.117	-0.088
0.907	-3.024	0.120	0 100	962.0	-0.344	-0.239	-0.173	-0.133	-0.114	-0.091	-0.065
0.90	2010	0.150	0.22	27.5	-0 392	-0.285	-0.198	-0.131	-0.097	-0.063	-0.031
0.900	5.010	0.130	0.247	513	-0.455	-0.352	-0.235	-0.125	-0.075	-0.035	-0.004
0.699	0.012	0 164	0.254	-0.784	-0.350	-0.228	-0.131	-0.082	-0.055	-0.033	-0.005
0.830	-0.003	0 237	-0.378	-1 189	-0.500	-0.203	-0.021	0.063	0.106	0.135	0.162
0.702	0.007	0.236	-0.372	-0.910	-0.471	-0.201	-0.029	0.048	0.094	0.123	0.156
0.001	900	-0.213	-0.347	-0.739	-0.421	-0.181	-0.018	0.033	0.088	0.110	0.141
0.777	20.0										

								41.	450		
				Stati	ic pressure co	Static pressure coefficients on nozzle top thap at $y/Y = 0.8/3$ with values of x/I of—	nozzle top t	$ap \ at \ y/Y = 0$	C/8.		
	•		,,,,,	300	727	117	855	705	6/1	.853	.926
W _∞	a, deg	.133	077	wc.	,cc.		9000	55.5			
252	-0.028	0.003	-0.005	-0.419	-0.410	-0.321	-0.304	-0.222	-0.173	-0.141	-0.114
202	0700	6000	9100	-0.463	-0.456	-0.355	-0.343	-0.223	-0.175	-0.140	-0.117
707.	2,072	0.131	0 186	-0.867	-0.447	-0.300	-0.215	-0.160	-0.138	-0.115	-0.084
200.0	13.02-	0.131	202.0	797.0-	-0.378	-0.254	-0.179	-0.128	-0.107	-0.084	-0.059
105.	20.023	200	2027	0.00	7070	0.282	_0 102	-0.115	-0.084	-0.057	-0.033
0.900	3.018	-0.149	-0.230	0.010	5	207.0	7/1:0		1200	0700	0.030
0 899	6.012	-0.166	-0.250	-0.862	-0.463	-0.342	-0.215	-0.102	-0.0/1	10.0 4 8	050.0
0.850	-0.063	-0 164	-0.252	-0.825	-0.394	-0.234	-0.123	-0.066	-0.043	-0.021	0.005
2020	290.0	0.223	-0 347	-1 010	-0.433	-0.215	-0.045	0.047	0.082	0.111	0.139
207.0	7007	0.216	0 320	-0.863	-0.398	-0.208	-0.051	0.036	0.072	0.102	0.133
1000	300	0.210	2000	707.0	-0 346	188	-0.042	0.035	0.074	0.097	0.120
2	5	ì	7,47	7	2	,					

Table 9. Continued

(b) Static pressure coefficients on nozzle sidewall

		7	Т	_	_	┰	_		3	$\overline{}$	т	_	_	ъ	_	т	7	_
		926	077	-0.141	0219	0000	7.039	890 0	0000	P\$0 0	970	5.54	900	20.00	0.132	201.0	0.120	0 117
		853	2010	70.107	174	0 1 20	0.120	70 086	0000	2002	7200	₩.O.4	9000	0.000	0.063	0.070	0.075	0.062
nd sidewall		779	0.73.1	-0.431	0219	0.141	7.141	9010	20110	960.0	7000	0.030	-0.045		0.023	0.035	660.0	0.018
zle top flap ar		705	9260	0/7:0	-0.284	5 163	0.105	-0.122		01.0	0 115	7.11.7	-0.056		0.022	800	2000	0.00
Static pressure coefficients on comer between nozzle top flap and sidewall	—Jo //x Jo	.558	080	0.50	-0.325	517	,	0.170		-0.163	0 176	0/1.0	101.0	1,00	29.7	-0.073	2/2/3	-0.063
its on comer	with values of x/l of-	.411	2000	,,,,,,	-0.334	-0 289	,	-0.251		-0.282	-0 333	66.0	-0.213	000	70.70	-0.198		99.7
ure coefficier		.337	175 0-		0.408	-0.494		-0.420	30,	-0.499	795 O	200	-0.426	0170	0.410	-0.377	2000	0.335
Static press		300	-0.372		-0.417	-0.849		-0.826	ì	-0.876	106.0		-0.910	0000	7007	-0.746	,,,,	-0.034
		.226	,		ı	ı		ı		!	ı		1		'	ı		'
		.153	0.004	2000	-0.005	-0.132	3	-0.128	2710	-C-14/	-0.167		-0.161	217	21.7:	-0.206	100	701.0
		α, deg	-0.028	0000	-0.070	-3.024	000	-0.029	2.010	3.010	6.012	6,000	-0.003	2900		-0.004	900 0	30.5
		M	1.252	1 202	1.202	0.902	1000	0.501	0000	30.5	0.899	0.000	0.650	0.702		0.601	00 U	//5.0

	Ţ		12	;] ₂	t	2	5	2],	_	4	١	5 5
	926	0.152	0.132	0.084	30.0	3	-0.025	9000		0.013	0.134	0 130	0.130
	853	700	107	000	0.000	-V:0.3	-0.050	9500	2000	30.0	0.093	0.085	080
0.50	977.	-0.243	-0 247	0110	0.077	//??	-0.069	-0.082	2000	270.0	0.057	0.048	0 040
wall at $z/Z =$.705	-0.252	-0.276	-0 133	9000	0.020	060.0	921.07	0.044	1	0.015	0.007	0 007
efficients on nozzle side with values of x/l of—	.558		1				ı	-			1		
Static pressure coefficients on nozzle sidewall at $z/Z = 0.50$ with values of x/l of—	.411	-0.322	-0.354	-0.305	-0.273	2,12,0	-0.315	-0.374	101 0		-0.206	-0.194	-0.170
tic pressure c	.337	-0.333	-0.374	-0.685	-0.717		-0.786	-0.823	-0.655		-0.367	-0.331	-0.288
Sta	300	-0.319	-0.355	-0.761	-0.770	200	-0.//3	-0.792	-0.879		_0.599	-0.513	-0.428
	.226	-0.001	-0.018	-0.207	-0.207	1100	-0.217	-0.235	-0.257	0220	0.530	-0.303	-0.264
	.153	0.007	-0.003	-0.131	-0.129	0.141	-0.141	-0.164	-0.165	0.217	-0.417	-0.208	-0.194
	α, deg	-0.028	-0.070	-3.024	-0.029	2010	010.0	6.012	-0.063	0.062	70.00	-0.004	-0.006
	M	1.252	1.202	0.902	0.901	0000	0.200	0.899	0.850	0.707	30.5	0.601	0.399

Table 9. Continued

(b) Concluded

									otage at Hair	انته			
					Š	tic pressure	Static pressure coefficients on nozzle sidewall at celletille with values of vI of—	efficients on nozzle side	wan at cente	2			
							Willi varue	10.00	33,	202	022	053	920
•	, do	153	226	300	.337	114:	.484	.558	.632	co/·	6//:	CCO.	. 720
M∞	a, acg	CC1:	227		2000	3000	707.0	7900	-0 243	-0.241	-0.247	-0.223	ı
1 252	-0.028	0.012	9000	-0.321	-0.333	-0.320	WC.U	0.70	25.0		0.06.0	0100	
		600	0.005	0 364	774	-0.368	0.344	-0.306	-0.274	-0.700	-0.203	7.717	
1.202	0.070	-0.002	-0.023	55.77			6	0110	101	0 111	200	20078	ı
0000	3 004	-0134	-0.220	-0.782	-0.792	-0.470	-0.1%	Q-140	17.17	-		200	
0.502	-2.027		200	707	0.783	75.0	951 0-	-0.112	960.0	-0.089	-0.075	-0.05	
06.0	-0.059	51.0	777.0	-0.702	Co/.0	2000			300	3000	0.064	0 041	ı
	0,0	2010	0100	785	207.02	7388	99.0	4.1.4	4.0.7	-0.000	10.00	5.5	
0.60	5.018	-0.133	20.210				20.00	0 146	0.121	0 106	070	-0.050	ì
000	6.012	0.150	231	-0.792	008.0	1.451	-0.1% -	-0.143	171.7	3	, , ,		
0.039	210.0	20.13		1000	0.017	0.00	0,10	000	900	-0.052	-0.026	-0.002	1
0.850	0.063	-0.170	-0.7/4	-0.890	7.01	20.5.0	2			1000	0.000	0000	1
	0,00	0000	0.242	0.587	-0.359	-0.203	-0.125	-0.073	-0.021	0.004	0.032	0.027	
0.705	790.0	0.770	7.545	790.0			3	3500	7000	7000	0.046	0.093	1
1070	200	8000	1	-0.505	-0.324	<u>36</u>	O.1.0	-0.0/3	-0.02#	5	2000	2000	
0.001	10.00	202			550	01.70	0 100	0.077	0.016	0100	0.043	260.0	-
0 300	900	1.07	-0.268	-0.433	6/7:0-	-0.1 <i>/</i> 0	7.100	7,0.0	010.0				
10:0	2000												

			Stati	ic pressure co	Static pressure coefficients on nozzle sidewall at $z/z = -0.30$ with values of x/l of—	nozzie sidew of x// of—	all at 2/2 = -	00.0	
		9	,35	55,	227	411	558	705	926
Mes	α, deg	.153	977	300	755.	.411	occ.	2011	
1 252	8000	0000	-0.006	-0.315	-0.328	_	-0.276	-0.255	-0.161
2001	0.070	\$000	9200-	-0.358	-0.370	1	-0.317	-0.285	-0.158
707.1	2,00,0	0.146	0.223	-0.773	_0.793	1	-0.149	-0.130	-0.063
0.907	-5.024	0.140	0.217	122.0	0 760	,	-0.125	-0.097	-0.052
0.901	1-0.029	-0.133	717.0		201.0		1410	0000	0.034
0060	3.018	-0.134	-0.213	-0.766	-0.748	ŀ	141	-0.007	10.00
0000	6013	0.160	_0 233	-0.784	-0.735	ı	-0.190	-0.125	-0.047
0.0%	0.012	0.100	0 271	-0.883	-0.838	 	-0.102	-0.057	-0.007
0.850	-0.003	20.100	7:7.	200.0			27.7	0.015	0.112
0.702	-0.062	-0.211	-0.340	-0.607	-0.369	1	7/0.0	0.015	2.1.5
0.601	0.004	-0 197	-0.313	-0.520	-0.332	1	-0.070	0.012	0.100
100.0	700.0	0 168	0.787	-0.437	-0.288	1	-0.059	0.018	0.078
	5	2	107.0						

Table 9. Continued

(c) Static pressure coefficients on nozzle bottom flap

		.926	-0.122	-0.133	-0.079	-0.044	-0.052	0.054	0.00	0.137	0 130	0.134
		.853	-0.163	-0.176	0.086	070	9800	-0.105	8000	0 102	0 102	960'0
2000	= 0.8/3	<i>ett</i> .	-0.219	-0.229	-0.095	-0.098	-0.118	-0.137	-0.032	0.076	0.076	0.078
flor of V	i iiap at <i>yi I</i> =	705	-0.282	-0.293	-0.117	-0.133	-0.153	-0.176	-0.068	0.038	0.037	0.036
mottod election	Seattle pressure coefficients on 1022/16 bottom 114p at $y/I = 0.8/3$ with values of x/I of—	.558	-0.311	-0.350	-0.212	-0.218	-0.229	-0.262	-0.160	-0.056	-0.057	-0.059
fficients on n	with values	.411	-0.347	-0.391	-0.379	-0.351	-0.330	-0.371	-0.301	-0.209	-0.195	-0.167
acciling Coa	ana a meeard	.337	-0.429	-0.473	-0.801	-0.760	-0.677	-0.744	-0.679	-0.456	-0.415	-0.360
Static	Otalic	.300	-0.354	-0.402	-0.849	-0.840	-0.829	-0.829	-0.961	-0.969	-0.805	-0.690
		.226	-0.011	-0.034	-0.241	-0.214	-0.202	-0.222	-0.266	-0.352	-0.327	-0.293
		.153	0.004	-0.016	-0.157	-0.139	-0.139	-0.169	-0.175	-0.228	-0.215	-0.190
		α, deg	-0.028	-0.070	-3.024	-0.029	3.018	6.012	-0.063	-0.062	-0.004	-0.006
		M_{∞}	1.252	1.202	0.902	0.901	0.900	0.899	0.850	0.702	0.601	0.399

vith values of x/l of— with values of x/l of— .153 .226 .300 .337 .411 .558 .705 .779 .853 0.002 -0.017 -0.366 -0.525 -0.490 -0.408 -0.169 -0.138 -0.113 -0.016 -0.045 -0.415 -0.578 -0.542 -0.420 -0.169 -0.139 -0.113 -0.159 -0.256 -0.853 -0.588 -0.398 -0.287 -0.184 -0.130 -0.130 -0.150 -0.256 -0.853 -0.341 -0.257 -0.175 -0.130 -0.096 -0.138 -0.231 -0.819 -0.442 -0.310 -0.155 -0.129 -0.109 -0.129 -0.220 -0.819 -0.536 -0.252 -0.165 -0.103 -0.103 -0.189 -0.310 -0.878 -0.352 -0.262 -0.180 -0.103 -0.277 -0.462 -1.193 -0.548 -0.215 -0.034 0.074 0.105 <		.926	0.095	0.109	-0.038	0.055	0000	8900	010	0.010	0.177	0.157
α, deg .153 .226 .300 .337 .411 .558 .705 .779 -0.028 0.002 -0.017 -0.366 -0.525 -0.490 -0.408 -0.169 -0.138 -0.024 -0.016 -0.045 -0.415 -0.578 -0.542 -0.169 -0.159 -3.024 -0.159 -0.256 -0.853 -0.588 -0.398 -0.287 -0.184 -0.159 -0.029 -0.150 -0.250 -0.824 -0.388 -0.398 -0.287 -0.184 -0.130 -0.029 -0.138 -0.233 -0.824 -0.341 -0.257 -0.184 -0.130 -0.029 -0.138 -0.231 -0.341 -0.257 -0.165 -0.129 -0.029 -0.129 -0.231 -0.442 -0.310 -0.257 -0.165 -0.142 -0.063 -0.189 -0.219 -0.262 -0.189 -0.142 -0.162 -0.142 -0.063 -0.189 -0.218			Ť	Ť	H	H	Ť	H	\dagger	+	+	╁
α, deg .153 .226 .300 .337 .411 .558 .705 -0.028 0.002 -0.017 -0.366 -0.525 -0.490 -0.408 -0.169 -0.070 -0.016 -0.045 -0.415 -0.578 -0.542 -0.169 -3.024 -0.159 -0.256 -0.853 -0.588 -0.387 -0.184 -0.029 -0.150 -0.250 -0.824 -0.389 -0.387 -0.184 -0.029 -0.138 -0.233 -0.801 -0.449 -0.310 -0.257 -0.165 -0.053 -0.139 -0.237 -0.819 -0.342 -0.310 -0.155 -0.063 -0.189 -0.231 -0.889 -0.352 -0.257 -0.165 -0.063 -0.189 -0.310 -0.878 -0.356 -0.319 -0.108 -0.064 -0.277 -0.462 -1.193 -0.548 -0.215 -0.039 -0.074 -0.004 -0.275 -0.446 <td< td=""><td></td><td>.853</td><td>9</td><td>-0.13</td><td>000</td><td>000</td><td>9</td><td>9</td><td>3 9</td><td>0.14</td><td>0 14</td><td>0 142</td></td<>		.853	9	-0.13	000	000	9	9	3 9	0.14	0 14	0 142
α, deg .153 .226 .30 -0.028 0.002 -0.017 -0.3 -0.070 -0.016 -0.045 -0.4 -3.024 -0.159 -0.256 -0.8 -0.029 -0.150 -0.250 -0.8 3.018 -0.138 -0.233 -0.8 6.012 -0.129 -0.233 -0.8 -0.063 -0.129 -0.210 -0.8 -0.063 -0.179 -0.465 -1.19 -0.004 -0.277 -0.446 -0.89 -0.006 -0.272 -0.446 -0.89 -0.006 -0.245 -0.404 -0.74	0.30	<i>ett</i> :	-0.138	-0.159	-0.130	-0.132	-0.129	-0.142	1900	0 113	0 115	0 138
α, deg .153 .226 .30 -0.028 0.002 -0.017 -0.3 -0.070 -0.016 -0.045 -0.4 -3.024 -0.159 -0.256 -0.8 -0.029 -0.150 -0.250 -0.8 3.018 -0.138 -0.233 -0.8 6.012 -0.129 -0.23 -0.8 -0.063 -0.129 -0.21 -0.8 -0.063 -0.277 -0.462 -1.19 -0.004 -0.272 -0.446 -0.89 -0.006 -0.245 -0.404 -0.74	n napan <i>yn</i>	705	-0.169	-0.192	-0.184	-0.175	-0.165	-0.180	-0.108	0.074	0.073	0.067
α, deg .153 .226 .30 -0.028 0.002 -0.017 -0.3 -0.070 -0.016 -0.045 -0.4 -3.024 -0.159 -0.256 -0.8 -0.029 -0.150 -0.250 -0.8 3.018 -0.138 -0.233 -0.8 6.012 -0.129 -0.233 -0.8 -0.063 -0.189 -0.310 -0.8 -0.063 -0.277 -0.462 -1.19 -0.004 -0.272 -0.446 -0.89 -0.006 -0.245 -0.404 -0.74	nozzie bottor s of x/l of—	.558	-0.408	-0.420	-0.287	-0.257	-0.237	-0.262	-0.219	-0.034	-0.039	-0.056
α, deg .153 .226 .30 -0.028 0.002 -0.017 -0.3 -0.070 -0.016 -0.045 -0.4 -3.024 -0.159 -0.256 -0.8 -0.029 -0.150 -0.250 -0.8 3.018 -0.138 -0.233 -0.8 6.012 -0.129 -0.233 -0.8 -0.063 -0.189 -0.310 -0.8 -0.063 -0.277 -0.462 -1.19 -0.004 -0.272 -0.446 -0.89 -0.006 -0.245 -0.404 -0.74	with values	.411	-0.490	-0.542	-0.398	-0.341	-0.310	-0.352	-0.331	-0.215	-0.215	-0.203
α, deg .153 .226 .30 -0.028 0.002 -0.017 -0.3 -0.070 -0.016 -0.045 -0.4 -3.024 -0.159 -0.256 -0.8 -0.029 -0.150 -0.250 -0.8 3.018 -0.138 -0.233 -0.8 6.012 -0.129 -0.233 -0.8 -0.063 -0.189 -0.310 -0.8 -0.063 -0.277 -0.462 -1.19 -0.004 -0.272 -0.446 -0.89 -0.006 -0.245 -0.404 -0.74	pressure co	.337	-0.525	-0.578	-0.588	-0.489	-0.442	-0.536	-0.438	-0.548	-0.527	-0.473
α, deg .153 -0.028 0.002 -0.070 -0.016 -3.024 -0.159 -0.029 -0.150 3.018 -0.138 6.012 -0.139 -0.063 -0.189 -0.064 -0.272 -0.004 -0.272	Static	300	-0.366	-0.415	-0.853	-0.824	-0.801	-0.819	-0.878	-1.193	-0.892	-0.749
α, deg -0.028 -0.070 -3.024 -0.029 3.018 6.012 -0.063 -0.064 -0.004		.226	-0.017	-0.045	-0.256	-0.250	-0.233	-0.220	-0.310	-0.462	-0.446	-0.404
		.153	0.002	-0.016	-0.159	-0.150	-0.138	-0.129	-0.189	-0.277	-0.272	-0.245
M _∞ 1.252 1.202 0.902 0.900 0.899 0.850 0.702 0.601		α, deg	-0.028	-0.070	-3.024	-0.029	3.018	6.012	-0.063	-0.062	-0.004	-0.006
		M_{∞}	1.252	1.202	0.902	0.901	0.000	0.899	0.850	0.702	0.601	0.399

Table 9. Continued

(c) Concluded

_			_	_	_	_	_	_	_	_	_	Т	Ŧ	7	ĺ
		926	-0.106	-0.123	-0.047	-0.057	7700	-0.004	-0.076	9000	0.161	1010	0.104	0.139	
dine		.705	-0.172	-0.198	-0.184	-0.172		-0.16/	-0.184	-0.100	0.081	o to	0.079	0.077	
State of gont	nap ar cente	.558	-0.375	-0.372	-0.278	0.250	0.530	-0.231	-0.253	-0.200	_0.032	2000	-0.039	-0.049	
	Static pressure coefficients on nozzle bottom flap at centerine with values of x/l of—	.411	-0.488	-0.543	-0.378	0.221	0.00	-0.299	-0.332	-0.319	0.244	7.7	-0.246	-0.234	
	tricients on nozzle borto with values of x/l of—	.337	-0.502	-0.558	-0.545	0.046	-0.400	-0.417	-0.499	-0.466	V05 0	17:7	-0.561	-0.499	
	pressure coe	300	-0 370	-0417	0.842	0.012	-0.013	-0.782	-0.821	-0.912	1.071	-1.271	-0.937	-0.793	
	Static	.226	0000	0.055	570.0	-0.203	-0.200	-0.253	-0 244	0.321	1.22.1	-0.483	-0.467	-0.471	1
		153	0000	0.00	0.150	-0.109	-0.162	-0.154	-0.144	0.00	0.202	-0.303	-0.298	0.270	21.7
		o dea	90000	0.020	2,0070	-3.024	-0.029	3.018	6.012	0.012	-0.003	-0.062	7000	9000	3
		7	ω ₁₁ ,	1.252	1.202	0.907	0.301	0.000	0.300	0.079	0.830	0.702	0.601	0000	1,333

(d) Force data

c_D	0.2524	0.2710	0.2242	0.1985	0.1978	0.2233	0.1603	0.0749	0.0691	0.0630
α, deg	-0.028	-0.070	-3.024	-0.029	3.018	6.012	-0.063	-0.062	-0.004	-0.006
M	1.252	1.202	0.902	0.901	0.900	0.899	0.850	0.702	0.601	0.399
-										

Table 10. Pressure and Force Data for Nozzle 7 With $\beta_{t,top/bot} = \beta_{t,sidc} = 16.4^{\circ}$, Plume On, and $\alpha = 0^{\circ}$

(a) Static pressure coefficients on nozzle top flap

	.926	0.224	0.204	0.082	-0.076	-0.088	-0.089	-0.061	-0.033	-0.003	0.026	0.081	0.199	0.222	0.217
	.853	0.198	0.185	0.048	-0.096	-0.111	-0.122	-0.092	-0.065	-0.036	-0.009	0.048	0.180	0.195	0.187
	622	0.166	0.161	0.020	-0.113	-0.128	-0.149	-0.121	-0.094	-0.064	-0.042	0.017	0.156	0.164	0.156
erline	307.	0.124	0.125	-0.012	-0.127	-0.146	-0.168	-0.146	-0.121	-0.097	-0.072	-0.013	0.124	0.124	0.113
Static pressure coefficients on nozzle top flap at centerline with values of x/l of	.632	0.076	0.083	-0.044	-0.142	-0.158	-0.185	-0.164	-0.145	-0.126	-0.10 4	-0.046	0.082	0.077	0.066
fficients on nozzle top with values of x/l of—	.558	0.013	0.025	-0.082	-0.232	-0.204	-0.200	-0.183	-0.169	-0.156	-0.136	-0.084	0.022	0.013	0.004
oefficients o	.484	-0.071	-0.057	-0.129	-0.432	-0.471	-0.225	-0.204	-0.192	-0.185	-0.171	-0.132	-0.058	-0.070	-0.076
c pressure c	.411	-0.203	-0.189	-0.200	-0.471	-0.512	-0.275	-0.241	-0.224	-0.221	-0.218	-0.200	-0.193	-0.201	-0.196
Stati	.337	-0.493	-0.514	-0.347	-0.494	-0.544	-0.420	-0.349	-0.306	-0.296	-0.308	-0.346	615:0-	-0.488	-0.443
	300	-1.014	-1.303	-0.827	-0.383	-0.422	-0.712	699.0-	-0.644	-0.643	-0.681	-0.807	-1.277	-1.014	-0.834
	.226	-0.436	-0.439	-0.331	-0.010	-0.017	-0.159	-0.190	-0.221	-0.247	-0.275	-0.330	-0.438	-0.440	-0.393
	.153	-0.289	-0.286	-0.222	-0.004	-0.002	-0.096	-0.121	-0.146	-0.165	-0.183	-0.218	-0.285	-0.288	-0.263
	M	0.598	0.699	0.798	1.250	1.200	0.950	0.926	0.000	0.874	0.851	0.800	0.703	0.603	0.402

			Stati	Static pressure coefficients on nozzle top flap at $y/Y = 0.50$	oefficients or	fficients on nozzle top	flap at y/Y:	= 0.50		
;					with value	—IO /// IO s				
M	.153	.226	.300	.337	.411	.558	.705	622.	.853	.926
0.598	-0.262	-0.409	-1.008	-0.461	-0.181	0.017	0.123	0.164	0.195	0.224
0.699	-0.265	-0.414	-1.285	-0.491	-0.180	0.025	0.125	0.160	0.186	0.206
0.798	-0.210	-0.318	-0.876	-0.413	-0.226	-0.083	-0.011	0.021	0.051	0.084
1.250	-0.001	-0.007	-0.370	-0.500	-0.455	-0.267	-0.124	-0.107	-0.091	-0.073
1.200	0.002	-0.010	-0.411	-0.546	-0.494	-0.241	-0.134	-0.117	-0.103	-0.082
0.950	-0.092	-0.150	-0.743	-0.498	-0.313	-0.222	-0.184	-0.160	-0.129	-0.093
0.926	-0.115	-0.180	-0.749	-0.434	-0.292	-0.205	-0.157	-0.127	-0.097	-0.061
0.900	-0.137	-0.209	-0.717	-0.386	-0.267	-0.182	-0.124	-0.097	-0.064	-0.035
0.874	-0.157	-0.238	-0.721	-0.366	-0.254	-0.165	-0.101	-0.068	-0.036	0.001
0.851	-0.173	-0.263	-0.738	-0.367	-0.247	-0.145	-0.077	-0.042	-0.008	0.028
0.800	-0.208	-0.316	-0.856	-0.405	-0.227	-0.082	-0.011	0.021	0.050	0.083
0.703	-0.263	-0.412	-1.261	-0.503	-0.180	0.025	0.124	0.158	0.183	0.202
0.603	-0.263	-0.411	-1.009	-0.461	-0.181	0.018	0.122	0.162	0.194	0.220
0.402	-0.240	-0.367	-0.823	-0.417	-0.174	0.010	0.113	0.155	0.189	0.217

Table 10. Continued

(a) Concluded

Mo	.153	.226	.300	Static pressure coefficients on nozzle top flap at $y/Y = 0.75$ with values of x/l of— 337 337 337 337 3409 3409 3409	with values	with values of x/l of—	Tap at v/Y =	0.75 - 779 - 0.155	.853	.926
	-0.243	-0.302	-0.663	-0.436	-0.160	0.027	0.123	0.155	0.185	0.207
	-0.204	-0.308	-0.964	-0.470	-0.228	-0.070	0.001	0.031	0.066	0.101
*	-0.006	0.010	-0.378	-0.500	-0.421	-0.319	-0.113	-0.100	-0.082	-0.061
_	-0.004	-0.013	-0.416	-0.544	-0.453	-0.294	-0.125	-0.110	-0.094	-0.073
•	-0.093	-0.149	-0.764	-0.565	-0.338	-0.231	-0.188	-0.161	-0.126	-0.088
+	-0.117	-0.177	-0.794	-0.479	-0.314	-0.214	-0.156	-0.123	-0.089	-0.053
+	-0.138	-0.207	-0.777	-0.431	-0.286	-0.188	-0.122	-0.093	-0.057	-0.025
-	-0.156	-0.234	-0.778	-0.411	-0.273	-0.163	-0.095	-0.060	-0.022	0.011
+-	-0.173	-0.257	-0.802	-0.415	-0.265	-0.142	-0.069	-0.034	0.003	0.038
1	-0.202	-0.307	-0.935	-0.464	-0.228	-0.073	-0.001	0.031	0.063	0.099
1-	-0.245	-0.379	-1.119	-0.439	-0.161	0.026	0.120	0.153	0.182	0.204
1	-0.235	-0.362	-0.884	-0.407	-0.160	0.021	0.116	0.154	0.187	0.217
T	-0.211	-0.322	-0.732	-0.363	-0.147	0.022	0.108	0.143	0.180	0.211

		Stati	c pressure cc	Static pressure coefficients on nozzle top flap at $y/Y = 0.875$	nozzle top f	$\int \int dx dx dx = 0$	3.875		
				with values of XI of—	-10 IX 10				
.226	_	.300	.337	.411	.558	.705	622.	.853	.926
-0.329	_	-0.818	-0.379	-0.149	1	0.113	0.151	0.185	0.213
-0.349		-0.994	-0.411	-0.154		0.119	0.153	0.183	0.208
-0.297	_	-1.052	-0.477	-0.205	ı	810'0	0.045	0.077	0.107
9000	T -	-0.362	-0.454	-0.348	1	-0.117	680.0-	-0.071	-0.049
0.010		-0.401	-0.489	-0.382	1	-0.126	-0.102	-0.083	-0.061
-0.145		-0.741	-0.660	-0.338	ı	-0.188	-0.157	-0.120	-0.088
0.174		-0.794	-0.550	-0.324	-	-0.151	-0.119	-0.085	-0.052
-0.202		-0.837	-0.466	-0.299	ı	-0.118	-0.085	-0.053	-0.023
-0.227		-0.864	-0.442	-0.282	1	-0.086	-0.053	-0.018	0.014
-0.250		-0.899	-0.443	-0.269	1	-0.060	-0.024	0.010	0.043
-0.293		-1.024	-0.472	-0.208	1	0.015	0.045	0.076	0.104
0.350		-1.005	-0.412	-0.155	1	0.117	0.152	0.180	0.204
0.328		-0.818	-0.380	-0.151	1	0.113	0.150	0.183	0.209
-0.294	1	-0.684	-0.335	-0.136	ı	0.104	0.142	0.175	0.202

Table 10. Continued

(b) Static pressure coefficients on nozzle sidewall

		926	0.203	0000	101.0	-0.028	-0.048	-0.117	0.074	0.07	200.0	0.000	0.034	0.077	0.197	0.200
		.853	0.176	0.180	0.083	-0.058	-0.072	5135	36	2000	0.00	0.01	0.00	0.177	0.176	0.165
	and sidewall	977.	0.146	0.152	0.065	-0.088	-0.093	-0.159	5116	0800	0.000	0100	0.000	0 148	0.147	0.136
	zzle top flap	705	0.11	0.118	0.040	-0.145	-0.140	-0.187	-0.147	20107	0.071	-0.038	0.037	9110	0.110	0.101
	s on comer between no with values of x/l of—	.558	0.023	0.029	-0.029	-0.292	-0.324	-0.244	-0.225	-0 183	-0 145	5119	-0.032	0.027	0.005	0.026
	ents on come with value	.411	-0.137	-0.141	-0.189	-0.325	-0.357	-0.341	-0.326	-0.303	-0.284	-0.265	161.0	-0.142	-0.135	-0.118
. 200	Static pressure coefficients on corner between nozzle top flap and sidewall with values of x/l of—	.337	-0.355	-0.382	-0.536	-0.440	-0.481	-0.739	-0.651	-0.527	-0.498	-0.503	-0.531	-0.384	-0.358	-0.314
	Static pres	300	-0.858	-1.023	-1.001	-0.401	-0.447	-0.809	-0.857	-0.874	-0.855	698.0-	-0.965	-1.029	-0.861	-0.722
		.226	-0.326	-0.346	-0.296	-0.005	-0.009	-0.145	_0.172	-0.202	-0.227	-0.249	-0.293	-0.347	-0.325	-0.288
		.153	1	ı	1	-	1	ı	1	1	ı	ı	I	1	!	1
		M∞	0.598	0.699	0.798	1.250	1.200	0.950	0.926	0.900	0.874	0.851	0.800	0.703	0.603	0.402

	779 853 926	0710	0.181	0.112	-0 036	-0.046	2000	3000	700.0-	50 -0.017 0.018	0.010	0.040	0110	0.170	0.170	0.1/2
Static pressure coefficients on nozzle sidewall at $z/Z = 0.50$ with values of x/l of	7. 705	+	╁	t	╀	\dagger	t	\dagger	1	-0.086 -0.050	-0.051 -0.014		+	ł	+	+
fficients on nozzle sidew:	.558		1		ı		1			1	ı	1				
coefficients or with values	.411	-0.151	-0.152	-0.203	-0.422	-0.454	-0.441	-0 345		-0.301	-0.281	-0.266	-0.208	-0.151	-0.151	-0 140
atic pressure	.337	-0.397	-0.419	-0.526	-0.474	-0.519	-0.877	-0.853		-0.577	-0.502	-0.492	-0.520	-0.420	-0.398	-0.355
Sta	300	-0.529	-0.660	-0.759	-0.196	-0.227	-0.483	-0.524		-0.568	-0.606	-0.645	-0.742	-0.662	-0.523	-0.408
	.226	-0.357	-0.376	-0.317	-0.007	-0.018	-0.158	-0.186	7100	-0.216	-0.241	-0.266	-0.315	-0.378	-0.353	-0.315
	.153	-0.223	-0.230	-0.201	0.000	-0.004	-0.094	-0.116		-0.138	-0.156	-0.171	-0.200	-0.232	-0.224	-0.202
	M	0.598	0.699	0.798	1.250	1.200	0.950	0.926	800	0.900	0.874	0.851	0.800	0.703	0.603	0.402

Table 10. Continued

(b) Concluded

				Sta	tic pressure c	coefficients or with values	efficients on nozzle sider with values of .x/l of—	Static pressure coefficients on nozzle sidewall at centerline with values of x/l of—	line			
M	.153	.226	300	.337	.411	.484	.558	.632	.705	<i>6LL</i> :	.853	.926
0.598	-0.236	-0.383	-0.770	-0.414	-0.160	-0.047	0.023	0.073	0.115	0.147	0.178	0.204
0.699	-0.244	-0.405	-0.925	-0.431	-0.154	-0.041	0.031	0.079	0.122	0.154	0.181	0.204
0.798	-0.208	-0.335	-1.104	-0.526	-0.222	-0.095	-0.022	0.025	0.062	0.090	0.116	0.143
1 250	0.007	-0.011		-0.479	-0.471	-0.396	-0.297	-0.220	-0.155	-0.086	-0.031	0.018
1 200	-0.003	-0.028	-0.430	-0.527	-0.511	-0.423	-0.318	-0.223	-0.138	-0.077	-0.041	-0.001
0.950	-0.094	-0.167	-0.781	40.67	-0.536	-0.249	-0.169	-0.136	-0.112	-0.087	-0.057	-0.014
9260	-0.120	-0.197	-0.835	-0.845	-0.376	-0.239	-0.175	-0.133	860.0-	-0.069	-0.033	0.003
0060	-0 140	-0.227	-0.882	-0.538	-0.314	-0.228	-0.170	-0.126	-0.087	-0.049	-0.015	0.021
0.874	-0.159	-0.254	-0.901	-0.472	-0.293	-0.205	-0.140	-0.092	-0.050	-0.016	0.021	0.053
0.851	-0.175	-0.280	-0.923	-0.463	-0.280	-0.180	-0.111	-0.059	-0.018	0.018	0.051	0.084
0 800	-0.207	-0.332	-1.072	-0.519	-0.226	-0.099	-0.028	0.021	0.055	0.086	0.112	0.138
0.703	-0.246	-0.404	-0.932	-0.429	-0.155	-0.042	0.028	0.079	0.119	0.151	0.178	0.200
0.603	-0.238	-0,380	-0.768	-0.412	-0.156	-0.045	0.023	0.073	0.114	0.147	0.177	0.201
0.402	-0.218	-0.343	-0.648	-0.370	-0.149	-0.045	0.021	0.068	0.108	0.138	0.168	0.194

		Static	Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$	efficients on	nozzle sidew	"all at $z/Z = -$	0.50	
			•	with values	with values of x/l of-			
M	.153	.226	300	.337	.411	.558	.705	.926
0.598	-0.221	-0.356	-0.758	-0.392	-0.151	810.0	0.110	0.205
0.699	-0.228	-0.374	-0.920	-0.414	-0.152	0.027	0.116	0.207
0.798	-0.198	-0.318	-1.126	-0.536	-0.215	-0.021	0.063	0.145
1.250	0.012	-0.001	-0.387	-0.467	-0.426	-0.307	-0.186	0.013
1.200	-0.002	-0.020	-0.432	-0.516	-0.458	-0.336	-0.156	-0.008
0.950	-0.090	-0.155	-0.782	-0.877	-0.537	-0.174	-0.114	-0.020
0.926	9.111	-0.185	-0.834	-0.854	-0.366	-0.178	-0.099	0.005
0.900	-0.135	-0.215	-0.890	-0.575	-0.309	-0.171	-0.084	0.020
0.874	-0.152	-0.241	-0.925	-0.498	-0.287	-0.140	-0.051	0.054
0.851	-0.169	-0.265	-0.963	-0.491	-0.273	-0.109	-0.015	0.083
0.800	-0.196	-0.313	-1.100	-0.533	-0.220	-0.025	0.059	0.140
0.703	-0.228	-0.375	-0.927	-0.412	-0.151	0.026	0.118	0.201
0.603	-0.219	-0.354	-0.757	-0.391	-0.149	0.021	0.111	0.202
0.402	-0.197	-0.316	-0.639	-0.344	-0.136	0.018	0.104	0.193

Table 10. Continued

(c) Static pressure coefficients on nozzle bottom flap

	.926	0.217	0.217	0.147	-0.012	-0.038	-0.050	-0.024	-0.001	0.036	0.070	0.143	0.214	0.213	0.205
	.853	0.185	0.189	0.121	-0.050	-0.070	-0.087	-0.060	-0.034	0.003	0.040	0.117	0.187	0.184	0.175
= 0.875	<i>6LL</i> :	0.149	0.157	0.093	-0.093	-0.102	-0.121	-0.095	-0.066	-0.031	0.008	0.091	0.156	0.150	0.141
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.875$ with values of x/I of—	.705	0.113	0.119	190'0	-0.220	-0.157	-0.150	-0.130	-0.102	-0.063	-0.028	0.057	0.117	0.111	0.102
cients on nozzle bottom	.558	0.015	0.022	-0.028	-0.315	-0.342	-0.212	-0.208	-0.180	-0.148	-0.113	-0.033	0.020	0.016	0.014
fficients on n	.411	_	-	_	_	_	-		444		1		_		ļ
pressure coe	.337	-0.377	-0.403	-0.566	-0.446	-0.490	-0.781	-0.736	-0.550	-0.508	-0.518	-0.567	-0.400	-0.375	-0.330
Static	.300	-0.862	-1.025	-1.035	-0.412	-0.454	-0.816	-0.867	-0.893	-0.877	-0.893	-1.005	-1.027	-0.857	-0.723
	.226	-0.328	-0.351	-0.303	-0.001	-0.020	-0.148	-0.178	-0.205	-0.232	-0.254	-0.299	-0.352	-0.329	-0.291
	.153	-0.216	-0.227	-0.199	0.008	-0.007	-0.090	-0.114	-0.135	-0.152	-0.168	-0.197	-0.227	-0.214	-0.191
	M∞	0.598	0.699	0.798	1.250	1.200	0.950	0.926	0.900	0.874	0.851	0.800	0.703	0.603	0.402

	T	Τ_	Τ	Т	Т	Г	Т	Γ	_	Т	Г	Т	Г	Т	Т
	.926	0.223	0.223	0.137	-0.046	-0.064	0.049	-0.028	-0.002	0.031	0.061	0.135	0.217	0.219	0.214
	.853	0.195	0.196	0.113	-0.076	-0.090	-0.085	-0.061	-0.037	-0.001	0.033	0.109	0.193	0.192	0.185
= 0.50	977.	0.159	0.165	0.085	-0.102	-0.115	-0.118	-0.096	-0.070	-0.038	-0.002	0.078	0.162	0.159	0.150
ı flap at y/Y :	705	0.119	0.126	0.051	-0.133	-0.142	-0.152	-0.131	-0.105	-0.073	-0.041	0.045	0.124	0.118	0.110
ozzle botton of x/l of—	.558	0.010	0.020	-0.053	-0.432	-0.394	-0.215	-0.202	-0.185	-0.162	-0.137	-0.059	0.019	0.007	0.002
fficients on nozzle botto with values of x/l of—	.411	-0.186	-0.179	-0.255	-0.478	-0.512	-0.349	-0.313	-0.280	-0.271	-0.278	-0.258	-0.179	-0.184	-0.175
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.50$ with values of x/l of—	.337	-0.463	-0.482	-0.513	-0.498	-0.550	699.0-	-0.521	-0.418	-0.397	-0.410	-0.508	-0.480	-0.464	-0.415
Static	.300	-0.852	-1.067	-1.062	-0.362	-0.410	-0.746	-0.787	-0.794	-0.811	-0.848	-1.037	-1.077	-0.851	-0.715
	.226	-0.411	-0.433	-0.345	-0.004	-0.021	-0.170	-0.198	-0.229	-0.257	-0.284	-0.341	-0.432	-0.412	-0.368
	.153	-0.260	-0.266	-0.220	0.012	-0.004	-0.096	-0.119	-0.141	-0.162	-0.180	-0.218	-0.266	-0.259	-0.237
	M_{∞}	0.598	0.699	0.798	1.250	1.200	0.950	0.926	0.900	0.874	0.851	0.800	0.703	0.603	0.402

Table 10. Concluded

(c) Concluded

		Static	pressure coe	Static pressure coefficients on nozzle bottom flap at centerline	ozzle botton	flap at cente	rline	
			,	with values of x/l of—	—jo <i>1/x</i> jo			
Mes	.153	.226	.300	.337	.411	.558	.705	.926
0.598	-0.278	-0.422	-0.867	-0.484	-0.213	-0.005	0.111	0.236
0.699	-0.284	-0.444	-1.099	-0.510	-0.206	800.0	0.120	0.238
0.798	-0.230	-0.354	-1.065	-0.508	-0.250	-0.057	0.044	0.139
1 250	0.008	-0.014	-0.363	-0.480	-0.463	-0.386	-0.151	-0.066
1.200	-0.009	-0.033	-0.408	-0.529	-0.509	-0.280	-0.164	-0.076
0.950	-0.105	-0.187	-0.745	-0.584	-0.326	-0.228	-0.170	-0.061
0.926	-0.128	-0.208	-0.769	-0.447	-0.286	-0.200	-0.136	-0.036
0060	-0.151	-0.237	-0.788	-0.417	-0.278	-0.181	-0.106	-0.004
0.874	-0.168	-0.265	-0.818	-0.406	-0.269	-0.157	-0.073	0.029
0.851	-0.187	-0.289	-0.859	-0.419	-0.265	-0.134	-0.043	0.063
0.800	-0.229	-0.350	-1.043	-0.504	-0.254	-0.063	0.041	0.136
0.703	-0.284	-0.444	-1.116	-0.510	-0.207	0.008	0.121	0.232
0.603	-0.277	-0.420	-0.866	-0.483	-0.211	-0.005	0.112	0.234
0.402	-0.250	-0.371	-0.723	-0.425	-0.199	-0.012	0.101	0.225

(d) Force data

$\begin{array}{c} CDf \\ 0.0119 \\ 0.0117 \\ 0.0117 \\ 0.0106 \\ 0.0112 \\ 0.0113 \\ 0.0113 \\ 0.0114 \\ 0.0115 \\ 0.0117 \\ 0.0120 \\ \end{array}$
$\begin{array}{c} CD_{,p} \\ 0.0381 \\ 0.0494 \\ 0.0494 \\ 0.1075 \\ 0.2237 \\ 0.2278 \\ 0.2278 \\ 0.2278 \\ 0.2278 \\ 0.2278 \\ 0.2278 \\ 0.2278 \\ 0.2278 \\ 0.2278 \\ 0.2278 \\ 0.2278 \\ 0.2278 \\ 0.2278 \\ 0.0208 \\ 0.0508 \\ 0.0306 \\ 0.0306 \\ \end{array}$
$\begin{array}{c} C_D \\ 0.0352 \\ 0.0408 \\ 0.1016 \\ 0.2365 \\ 0.2527 \\ 0.2394 \\ 0.2013 \\ 0.1766 \\ 0.1766 \\ 0.1766 \\ 0.1766 \\ 0.1766 \\ 0.0406 \\ 0.0406 \\ 0.0357 \\$
0.598 0.598 0.798 1.250 1.200 0.950 0.950 0.900 0.851 0.800 0.703

Table 11. Pressure and Force Data for Nozzle 7 With $\beta_{f,top/bot} = \beta_{f,side} = 16.4^\circ$ and Plume Off

(a) Static pressure coefficients on nozzle top flap

	Π	Ι.	Ι.						Γ.	Γ	Γ	Γ		Γ				Π	Γ	Γ		Γ	T
	926	0.104	-0.124	-0.112	-0.099	-0.082	-0.048	-0.067	-0.054	-0.039	-0.025	-0.00	-0.020	0.013	090.0	0.180	0.178	0.169	0.177	0.180	0.170	0.154	
	.853	-0.123	-0.138	-0.128	-0.122	-0.107	-0.082	-0.104	-0.086	-0.074	-0.062	-0.053	-0.051	-0.022	0.031	0.155	0.151	0.133	0.151	0.155	0.145	0.126	21 2
	622	-0.139	-0.147	-0.141	-0.138	-0.127	-0.108	-0.128	-0.111	-0.104	-0.101	-0.099	-0.081	-0.054	0.002	0.127	0.119	0.092	0.118	0.126	0.117	960.0	
line	.705	-0.157	-0.159	-0.153	-0.149	-0.145	-0.130	-0.148	-0.130	-0.131	-0.142	-0.147	-0.109	-0.082	-0.027	0.092	0.081	0.048	0.080	0.093	0.084	0.065	
flap at center	.632	-0.200	-0.182	-0.169	-0.158	-0.157	-0.152	-0.168	-0.153	191.0-	9/1.0-	-0.190	-0.135	-0.110	-0.055	0.050	0.038	0.000	0.037	0.054	0.048	0.029	
n nozzle top s of x/l of—	.558	-0.436	-0.333	-0.202	-0.171	-0.169	-0.168	-0.185	-0.171	-0.184	-0.210	-0.232	-0.161	-0.136	-0.089	-0.011	-0.021	-0.065	-0.023	-0.002	-0.005	-0.023	
coefficients on nozzle to with values of x/l of-	.484	-0.468	-0.482	-0.463	-0.190	-0.182	-0.189	-0.205	-0.191	-0.207	-0.239	-0.270	-0.187	-0.169	-0.134	-0.091	-0.102	-0.149	-0.104	-0.077	-0.077	-0.095	
Static pressure coefficients on nozzle top flap at centerline with values of x/l of—	.411	-0.530	-0.521	-0.575	-0.235	-0.217	-0.214	-0.237	-0.219	-0.238	-0.280	-0.318	-0.222	-0.213	-0.201	-0.225	-0.233	-0.286	-0.235	-0.202	-0.198	-0.217	
Sta	.337	-0.540	-0.545	-0.603	-0.351	-0.305	-0.294	-0.332	-0.305	-0.322	-0.381	-0.436	-0.298	-0.293	-0.335	-0.576	-0.518	-0.588	-0.521	-0.472	-0.463	-0.491	
	300	-0.421	-0.419	-0.476	-0.646	-0.616	-0.616	-0.660	-0.623	-0.638	-0.710	-0.768	-0.635	-0.654	-0.790	-1.317	-1.056	-1.202	-1.065	-0.966	-0.944	-1.011	
	.226	-0.025	-0.030	-0.043	-0.161	-0.191	-0.221	-0.205	-0.217	-0.230	-0.232	-0.229	-0.246	-0.276	-0.327	-0.448	-0.455	-0.490	-0.458	-0.427	-0.410	-0.409	
	.153	-0.007	-0.021	-0.026	-0.097	-0.123	-0.147	-0.134	-0.144	-0.154	-0.158	-0.162	-0.165	-0.188	-0.219	-0.292	-0.300	-0.320	-0.302	-0.282	-0.269	-0.263	
	α, deg	6.017	600.6	-0.020	0.078	0.020	-0.011	-2.988	-0.009	3.016	5.998	9.035	0.022	0.003	0.000	-0.001	-0.012	-2.981	0.000	3.014	5.989	9.000	
	M_{∞}	1.199	1.200	1.151	0.950	0.926	0.899	0.900	0.903	0.902	0.901	0.600	0.877	0.848	0.802	0.701	0.600	0.601	0.602	0.602	0.602	0.601	

Table 11. Continued

	.926	-0.100	-0.121	-0.112	-0.103	0800-	-0.047	890:0-	-0.053	-0.035	-0.019	-0.008	-0.018	0.014	0.059	0.177	0.175	0.167	0.174	0.177	0.168	0.157	0.166
	.853	-0.121	-0.135	-0.128	-0.131	-0.113	-0.084	-0.109	060:0-	-0.074	-0.057	-0.051	-0.054	-0.024	0.032	0.154	0.149	0.132	0.148	0.153	0.142	0.130	0.141
= 0.50	622:	-0.142	-0.148	-0.141	-0.149	-0.138	-0.113	-0.137	-0.119	-0.109	-0.099	-0.100	-0.086	-0.051	0.005	0.127	0.120	0.095	0.118	0.126	0.116	0.104	0.113
flap at y/Y =	.705	-0.160	-0.159	-0.156	-0.163	-0.157	-0.140	-0.163	-0.145	-0.141	-0.138	-0.146	-0.115	-0.083	-0.021	0.092	0.082	0.050	0.081	0.092	0.084	0.072	0.075
efficients on nozzle top with values of x/l of—	.558	-0.404	-0.391	-0.226	-0.191	-0.191	-0.188	-0.206	-0.192	-0.201	-0.217	-0.239	0.174	-0.146	-0.089	-0.005	-0.014	-0.057	-0.016	0.004	0.000	-0.012	9100
Static pressure coefficients on nozzle top flap at $y/Y = 0.50$ with values of x/l of—	.411	-0.524	-0.559	-0.562	-0.268	-0.262	-0.259	-0.279	-0.262	-0.280	-0.322	-0.354	-0.261	-0.244	-0.227	-0.210	-0.206	-0.259	-0.208	-0.176	-0.176	-0.192	701 0
tic pressure	.337	-0.548	-0.564	-0.610	-0.408	-0.383	-0.372	-0.407	-0.374	-0.395	-0.461	-0.477	-0.369	-0.363	-0.401	-0.549	-0.489	-0.560	-0.493	-0.448	-0.446	-0.470	OPP 0
Sta	.300	-0.411	-0.416	-0.466	969.0-	-0.701	-0.705	-0.748	-0.706	-0.722	-0.801	-0.809	-0.718	-0.736	-0.845	-1.293	-1.045	-1.186	-1.053	086.0-	686-0-	-1.026	D 8.40
	.226	-0.025	-0.050	-0.039	-0.150	-0.182	-0.214	-0.199	-0.211	-0.224	-0.230	-0.247	-0.236	-0.267	-0.314	-0.422	-0.424	-0.456	-0.427	-0.393	-0.371	-0.382	975 0-
	.153	-0.015	-0.048	-0.023	-0.090	-0.116	-0.139	-0.127	-0.136	-0.148	-0.161	-0.185	-0.156	-0.177	-0.206	-0.269	-0.272	0.289	-0.274	_0.254	-0.243	-0.255	-0.248
	α, deg	6.017	600.6	-0.020	0.078	0.020	-0.011	-2.988	-0.009	3.016	5.998	9.035	0.022	0.003	0.000	-0.001	-0.012	-2.981	0.000	3.014	5.989	000.6	5000
	M_{∞}	1.199	1.200	1.151	0.950	0.926	0.899	0.900	0.903	0.902	0.901	0.900	0.877	0.848	0.802	0.701	0.600	0.601	0.602	0.602	0.602	0.601	0.401

Table 11. Continued

		SI	Static pressure coefficients on nozzle top flap at $y/Y = 0.75$	coefficients c	on nozzle top	flap at $y/Y =$	0.75		
				with value	with values of x/l of-				
53	.226	.300	.337	.411	.558	.705	611.	.853	.926
.029	-0.045	-0.444	-0.580	-0.500	-0.331	-0.158	-0.128	-0.109	-0.091
.049	-0.067	-0.450	-0.580	-0.501	-0.326	-0.148	-0.132	-0.120	-0.109
.031	-0.041	-0.471	-0.606	-0.513	-0.301	-0.154	-0.140	-0.127	-0.109
.093	-0.147	-0.738	-0.462	-0.298	-0.208	-0.178	-0.161	-0.137	-0.107
119	-0.178	-0.757	-0.433	-0.290	-0.206	-0.165	-0.138	-0.110	-0.075
-0.141	-0.207		-0.420	-0.283	-0.191	-0.136	-0.109	-0.079	-0.0 4 4
.132	-0.187	-0.826	-0.479	-0.314	-0.217	-0.167	-0.140	-0.108	-0.071
-0.138	-0.205	1771	-0.427	-0.287	-0.198	-0.145	-0.116	-0.087	-0.052
156	-0.233	-0.750	-0.432	-0.305	-0.202	-0.133	-0.098	-0.063	-0.028
.169	-0.245	-0.753	-0.445	-0.334	-0.215	-0.123	-0.082	-0.041	-0.005
186	-0.262	-0.767	-0.454	0.347	-0.239	-0.134	-0.082	-0.031	0.012
.155	-0.231	-0.778	-0.418	-0.280	-0.174	_0.111	-0.078	-0.046	-0.012
.176	-0.262	-0.801	-0.417	-0.264	-0.143	-0.077	-0.046	-0.016	0.018
.203	-0.306	-0.920	-0.457	-0.234	-0.081	-0.013	0.012	0.038	0.065
္က	-0.393	-1.167	-0.463	-0.185	0.001	680.0	0.121	0.150	0.174
.246	-0.378	-0.911	-0.431	-0.183	-0.007	0.082	0.113	0.145	0.170
2	-0.403	-1.101	-0.505	-0.232	-0.042	0.056	0.094	0.132	0.164
-0.247	-0.381	-0.920	-0.434	-0.185	-0.008	0.081	0.112	0.144	0.169
္က	-0.351	-0.790	-0.366	-0.145	0.015	0.092	0.121	0.148	0.171
္က	-0.344		-0.336	-0.128	0.017	0.087	0.114	0.141	0.164
243	-0.349	-0.779	-0.324	-0.120	0.017	0.084	0.108	0.134	0.157
.221	-0.332	-0.756	-0.382	-0.164	-0.003	0.075	0.107	0.134	0.163

Table 11. Continued

(a) Concluded

		_	_	_	_	_	_		_	_	_	т-	Т	т	П	_		T	T	Т	Т	\neg			Г	٦.
	.926	-0.080	-0.093	-0.101	-0.109	-0.076	-0.042	-0.070	-0.050	-0.021	0.005	\$000	0.000	-0.010	0.022	0.069	0.171	0.168	0.162	70.1.05	0.168	0.168	0.164	0.153	0.158	
	.853	-0.101	-0.105	-0.117	-0.140	-0.108	-0.071	-0.101	-0.078	-0.049	9000	1100	0.011	-0.040	-0.008	0.046	0.150	0.143	0.131	0.131	0.143	0.147	0.140	0.132	0.135	0.133
875	6LL:	-0.124	-0.115	-0.131	-0.168	-0.140	-0.102	-0.136	-0.110	-0.084	0.065	CO0.0	/20.0	-0.071	-0.038	0.022	0.122	0.114	2000	0.037	0.114	0.121	0.116	0110	001.0	0.107
tp at $y/Y = 0$.	705	-0.168	-0.135	-0.147	881	7910-	-0133	-0.168	-0.142	-0.122	1010	/0.10	1117	-0.104	-0.069	-0.002	0.088	080.0	0000	0.038	0.079	0.091	0.087	0.086	0.075	0.07
nozzle top fla of x// of—	.558											1	1	-	1						1	I				1
Static pressure coefficients on nozzle top flap at $y/Y = 0.875$ with values of x/I of—	.411	75.0-	0.347	0.442	0.307	207	8000	0.270	305	306	200.0	-0.320	-0.343	-0.298	-0.275	20.03	0 176	27.70	-0.1/1	-0.211	-0.173	-0 139	0110	200	-0.100	151.0
pressure coe	.337	174	8870	0.460	5550	-0.532	0.457	0.430	0.766	0.430	10.437	-0.445	-0.460	-0.455	-0.451	0.431	0.40	-0.431	-0.402	-0.469	-0.405	738	7000	0.304	707.0	-0.351
Static	300	0.413	27.0	0.454	-0.434	0.741	-0.780	-0.623	-0.043	0.020	-0.019	-0.802	-0.835	-0.856	0000	1017	-1.01	-1.029	-0.844	-1.021	_0 846	8890	0.000	-0.010	-0.90/	-0.708
	226	2000	100	20.00	25.5	0.143	0.176	40.204	0.187	-0.200	-0.228	-0.244	-0.263	-0.226	0.363	-0.233	-0.290	-0.359	-0.340	-0.359	-0.342	0 333	-0.533	-0.328	-0.322	-0.302
	153		-	1	1	-	-		1	-	ı	1	. 1			1		1	1	1			,	1	1	ı
	 2 2	Cr. urg	6.017	9.009	-0.020	0.078	0.020	-0.011	-2.988	-0.009	3.016	5.998	9.035	0.000	220.0	0.003	0.000	-0.001	-0.012	_2 981	0000	0.00	3.014	5.989	9.000	-0.005
	7	/M,	1.199	1.200	1.151	0.950	0.926	0.899	0.900	0.903	0.902	0.901	0.900	0.877	0.07	0.848	0.802	0.701	0.600	0.601	100.0	0.002	0.602	0.602	0.601	0.401

Table 11. Continued

(b) Static pressure coefficients on nozzle sidewall

		.926	-0.069	-0.092	-0.094	2010	0003	0.051	1000	-0.085	-0.062	-0.020	0.002	0.014	0000	0.020	0.017	0.06/	0.166	0.162	0.154	0.162	731.0	0.10/	0.165	0.161
		.853	860'0-	-0.111	9.110	-0.160	-0.115	20075	6110	20.113	-0.086	-0.046	-0.020	900.0	-0.040		10.00	0.033	0.142	0.137	0.126	0.137	0 143	27.7	0.143	0.143
ind sidewall		.779	-0.136	-0.129	-0.125	-0.186	-0.140	-0.097	0.142	0 100	-0.100	-0.072	-0.050	-0.038	500	9000	0.020	0.030	0.118	0.110	0.096	0.110	0 116		0.110	0.121
Static pressure coefficients on corner between nozzle top flap and sidewall	100	50/	-0.190	-0.158	-0.148	-0.208	-0.169	-0.127	-0.173	0.137	0.157	40.104	0.090	-0.081	-0.095	-0.053	0.00	0.013	0.000	0.080	0.063	0.080	0.087	1000	0000	0.073
r between noz	with values of .v// of—	866.	-0.300	-0.278	-0.364	-0.238	-0.228	-0.197	-0.230	2000	007.0	0.130	-0.190	-0.186	-0.170	-0.125	0.051	2000	50.0	0.00	-0.022	-0.001	0.014	9100	0.000	0.005
ents on come	with value	114.	-0.316	-0.320	-0.416	-0.311	-0.313	-0.304	-0.339	300	0.311	0.333	-0.337	-0.348	-0.305	-0.275	0170	0.162	0.155	6:50	-0.181	-0.156	-0.129	819	-D 098	-0.136
sure coefficie	337	1000	-0.458	-0.455	-0.538	-0.636	-0.579	-0.526	-0.532	-0 540	195 9	303.0	-0.525	-0.524	-0.518	-0.520	-0.542	10404	-0 378	200	-0.424	-0.379	-0.328	-0.283	-0.256	-0.328
Static pres	300	2000	-0.457	-0.453	-0.502	-0.797	-0.840	-0.855	-0.853	-0.863	-0.883	0.022	-0.032	-0.835	-0.875	-0.903	-0.994	-1.057	-0.879	1001	17071-	-0.881	-0.783	-0.700	-0.594	-0.736
	226	0700	10.040	40.00	-0.043	-0.144	-0.176	-0.205	-0.191	-0.201	-0.228	577	1470	-0.203	-0.226	-0.254	-0.294	-0.357	-0.336	0.357	0.237	-0.338	-0.334	-0.337	-0.328	-0.297
	.153		'	-		-	-	1	1	ı	1	<u> </u>		Ţ	1	ı	-	1				-	1	ı	ı	1
	a, deg	6017		2000	0.020	0.0/8	0.020	-0.011	-2.988	-0.009	3.016	5.998	0.035	2.030	0.022	0.003	0.000	-0.001	-0.012	-2 981	000	2.50	3.014	5.989	000.6	-0.005
	W	100	1 200	007:1	1010	0.930	0.926	0.899	0.900	0.903	0.902	0.901	0000	0000	0.8//	0.848	0.802	0.701	0.09	109'0	0,602	200.0	0.002	0.602	0.601	0.401

Table 11. Continued

-0.016 0.164 0.159 0.1690.166 0.165 -0.0020.010 0.092 0.165 0.167 -0.096-0.040-0.0380.014 0.020 -0.072-0.079 90.0 0.051 926 -0.087-0.116 -0.043 -0.030 -0.019 -0.0160.075 0.146 0.142 0.1390.142 0.14 0.137 0.135 -0.036 0.028 -0.099 -0.132-0.074 -0.007 -0.073.853 0.114 0.116 -0.114-0.076 -0.056 -0.0540.055 0.119 0.113 -0.146-0.1140.002 0.107 0.107 -0.1070.115 -0.147 -0.167-0.068-0.037Static pressure coefficients on nozzle sidewall at z/Z = 0.500.074 0.085 0.078 -0.195 -0.178-0.152 -0.192 -0.146-0.155960.0--0.098 -0.0320.030 0.085 -0.112-0.103-0.101 0.081 705 with values of x/l of-.558 1 ī ı ı ì -0.165-0.155-0.370-0.170-0.142-0.318 -0.156-0.488-0.325-0.352-0.233-0.169-0.493-0.525-0.391 -0.351-0.334-0.309-0.287-0.181-0.171.411 -0.546-0.416 -0.429-0.544 -0.558 -0.826 -0.662 -0.598 -0.662 -0.565-0.417-0.413 -0.390-0.794 -0.628-0.588 -0.662 -0.442-0.583-0.531-0.411 -0.371.337 -0.541 -0.525 -0.650 -0.689 -0.537 -0.199 -0.436 -0.540 -0.549-0.564 -0.586 -0.600-0.739 -0.552-0.547-0.534-0.534-0.234300 -0.268 -0.315 -0.368 -0.326 -0.239 -0.389 -0.386-0.366 -0.054 -0.218 -0.215 -0.225-0.239-0.374-0.378-0.157 -0.188-0.053-0.217.226 -0.266-0.210-0.242-0.233-0.248 -0.234-0.146-0.199 -0.154-0.046-0.034 -0.093-0.142-0.141 -0.1520.170 -0.175-0.237-0.251 -0.201 -0.071 -0.118 .153 deg 3.014 000.6 0.000 3.016 0.003 0.020 -2.9885.998 9.035 0.022 -0.005 -0.020 0.078 9.009 -0.009-0.001 -0.012-2.981-0.011 6.017 ಶ 0.900 0.600 0.602 0.602 0.848 0.802 0.903 1.151 0.950 0.926 0.900 0.877 0.601 0.601 0.401 1.200 M 0.901

Table 11. Continued

(b) Continued

	.926	060.0	-0.143	-0.077	-0.078	-0.032	-0.005	-0.021	-0.013	-0.007	-0.00 400.00	0.003	0.020	0.052	0.093	0.169	0.166	0.167	0.166	0.166	0.159	0.133	0 150
	.853	-0.114	-0.164	-0.093	-0.107	-0.059	-0.029	-0.046	-0.034	-0.031	-0.032	-0.033	-0.004	0.031	0.077	0.146	0.140	0.140	0.140	0.138	0.131	0.115	0 133
	977.	-0.170	-0.189	-0.118	-0.137	-0.091	-0.060	-0.078	-0.066	-0.065	-0.067	-0.078	-0.036	0.004	0.055	0.118	0.114	0.114	0.114	0.112	0.105	0.097	0 107
ine	.705	-0.230	-0.228	-0.162	-0.163	-0.119	-0.095	-0.114	-0.102	-0.105	-0.108	-0.128	-0.071	-0.031	0.031	0.089	0.083	0.083	0.084	0.081	0.075	0.069	0.081
Static pressure coefficients on nozzle sidewall at centerline	.632	-0.283	-0.286	-0.231	-0.189	-0.153	-0.134	-0.151	-0.139	-0.146	-0.155	-0.186	-0.113	-0.072	-0.004	0.051	0.046	0.045	0.046	0.044	0.038	0.034	0.046
nozzle sidew	.558	-0.362	-0.368	-0.351	-0.226	-0.193	-0.184	-0.204	-0.190	-0.205	-0.211	-0.244	-0.162	-0.124	-0.052	0.004	0.000	-0.001	-0.001	-0.003	-0.009	-0.012	0.002
efficients on nozzle sic	.484	-0.423	-0.427	-0.480	-0.294	-0.259	-0.245	-0.270	-0.250	-0.272	-0.280	-0.302	-0.232	-0.198	-0.128	-0.065	-0.067	690.0-	-0.068	-0.071	-0.076	-0.078	-0.063
c pressure co	.411	-0.498	-0.480	-0.583	-0.541	-0.396	-0.343	-0.381	-0.353	-0.369	-0.370	-0.391	-0.326	-0.303	-0.260	-0.175	-0.174	-0.177	-0.174	-0.178	-0.183	-0.183	-0.160
Stati	.337	-0.542	-0.554	-0.595	-0.903	868.0-	-0.641	-0.806	-0.685	-0.636	-0.651	-0.774	-0.554	-0.519	-0.555	-0.455	-0.431	-0.441	-0.432	-0.442	-0.447	-0.441	-0.386
	.300	-0.442	-0.457	-0.490	-0.785	-0.839	-0.898	-0.902	-0.893	-0.894	-0.897	-0.919	-0.936	-0.979	-1.098	-0.976	-0.792	-0.823	-0.796	-0.825	-0.827	-0.811	-0.667
	.226	-0.055	-0.081	-0.063	-0.167	-0.199	-0.228	┪	7			-0.258	-0.252	-0.285	-0.333	-0.416	-0.396	-0.402	-0.397	-0.404	-0.414	-0.422	-0.356
	.153	-0.039	-0.067	-0.034	-0.097	-0.121	-0.143	-0. <u>14</u>	-0.141	-0.143	-0.156	-0.180	-0.159	-0.177	-0.210	-0.253	-0.247	-0.251	-0.249	-0.253	-0.265	-0.280	-0.223
	α, deg	6.017	600.6	-0.020	0.078	0.020	-0.011	-2.988	-0.009	3.016	5.998	9.035	0.022	0.003	0.000	-0.001	-0.012	-2.981	0.000	3.014	5.989	000.6	-0.005
	M _∞	1.199	1.200	1.151	0.950	0.926	0.899	0.900	0.903	0.902	0.901	0.900	0.877	0.848	0.802	0.701	0.600	0.601	0.602	0.602	0.602	0.601	0.401

Table 11. Continued

(b) Concluded

			Stati	Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$	efficients on	nozzle sidev	vall at $z/Z = -$	-0.50	
					with values of x/l of-	—Jo /// Jo			
M	α, deg	.153	.226	300	.337	.411	.558	.705	.926
1.199	6.017	-0.055	-0.062	-0.445	-0.527	-0.416	-0.372	-0.313	-0.118
1.200	600.6	-0.107	-0.109	-0.464	-0.533	-0.427	-0.403	-0.374	-0.218
1.151	-0.020	-0.034	-0.052	-0.492	-0.575	-0.530	-0.371	-0.194	-0.080
0.950	0.078	-0.090	-0.158	-0.782	-0.892	-0.646	-0.219	-0.152	-0.065
0.926	0.020	-0.115	-0.187	-0.839	-0.913	-0.409	-0.184	-0.114	-0.031
0.899	-0.011	-0.136	-0.216	968.0-	869:0-	-0.340	-0.181	-0.093	-0.005
0.900	-2.988	-0.145	-0.224	-0.901	-0.787	-0.373	-0.194	-0.089	-0.004
0.903	-0.009	-0.134	-0.215	6880-	-0.748	-0.347	-0.185	-0.098	-0.013
0.905	3.016	-0.137	-0.212	-0.884	-0.756	-0.361	-0.204	-0.107	-0.014
0.901	5.998	-0.165	-0.229	-0.893	-0.726	-0.379	-0.231	-0.132	-0.017
0.900	9.035	-0.210	-0.265	898.0-	-0.575	-0.436	-0.318	-0.160	-0.003
0.877	0.022	-0.152	-0.239	-0.946	-0.588	-0.328	-0.164	-0.070	0.020
0.848	0.003	-0.172	-0.269	-1.000	-0.552	-0.307	-0.126	-0.029	0.052
0.802	0.000	-0.204	-0.316	-1.126	-0.581	-0.260	-0.051	0.032	0.095
0.701	-0.001	-0.241	-0.387	-0.970	-0.438	-0.173	0.000	0.088	0.169
0.600	-0.012	-0.228	-0.365	-0.781	-0.411	-0.169	-0.003	0.082	0.165
0.601	-2.981	-0.230	-0.362	-0.783	-0.408	-0.161	0.005	0.088	0.167
0.602	0.000	-0.229	-0.366	-0.784	-0.412	-0.169	-0.004	0.083	0.164
0.602	3.014	-0.244	-0.386	-0.813	-0.428	-0.180	-0.014	0.074	0.162
0.602	5.989	-0.273	-0.413	-0.835	-0.438	-0.193	-0.028	0.058	0.147
0.601	9.000	-0.312	-0.445	-0.842	-0.446	-0.209	-0.050	0.020	0.119
0.401	-0.005	-0.209	-0.325	099.0-	-0.360	-0.153	-0.001	0.076	0.157

Table 11. Continued

(c) Static pressure coefficients on nozzle bottom flap

Static pressure coefficients on nozzle bottom flap at $y/Y = 0.875$ with values of x/I of—	300 .337 .411 .558 .705 .705 .853 .926	1471 -0.5360.446 -0.415 -0.227 -0.139 -0.111	-0.556	-0.5480.390 -0.258 -0.155 -0.104	-0.8490.244 -0.160 -0.124 -0.092	-0.8530.223 -0.150 -0.111 -0.079	-0.7020.199 -0.117 -0.083 -0.050	-0.699 - -0.201 -0.097 -0.055 -0.021	-0.7340.206 -0.124 -0.090 -0.057	-0.788	-0.84!0.251 -0.157 -0.113 -0.071	-0.735	-0.602	-0.5780.138 -0.043 -0.009 0.023	-0.612 - -0.069 0.021 0.053 0.076	-0.426	-0.3940.008 0.079 0.111 0.141	-0.331 - 0.010 0.090 0.120 0.146	0.3950.010 0.078 0.111 0.140	-0.4600.042 0.054 0.092 0.127	-0.5240.085 0.025	2000 7000 1100 0110	-0.390
ottom flap a		H	Ė						H		_	┢	H	<u> </u>				H	-	-	\vdash	<u> </u>	
n nozzle be ues of x/l o	.558	-0.44	-0.53(-0.390	-0.24	-0.22	-0.19	-0.20	-0.20	-0.23	-0.25	-0.334	-0.171	-0.138	-0.065	-0.00	-0.00	0.010	-0.010	-0.042	-0.085	-0.140	
efficients o	.411	,	ı	1		1	1	1	-	ı	-	-	1	-	1	-	1	-	1	1	-	-	
 pressure co	.337	-0.536	-0.556	-0.548	-0.849	-0.853	-0.702	-0.699	-0.734	-0.788	-0.841	-0.735	-0.602	-0.578	-0.612	-0.426	-0.394	-0.331	-0.395	-0.460	-0.524	-0.590	
Static	.300	-0.471	-0.490	-0.516	-0.818	-0.873	-0.928	-0.928	-0.925	-0.928	-0.934	-0.933	-0.950	-0.975	-1.067	-1.079	-0.885	-0.700	-0.887	-1.062	-1.179	-1.281	
	.226	-0.070	-0.132	-0.050	-0.152	-0.182	-0.208	-0.239	-0.206	-0.194	-0.217	-0.264	-0.230	-0.261	-0.304	-0.365	-0.339	-0.330	-0.341	-0.361	-0.393	-0.436	
	.153	-0.078	-0.155	-0.035	-0.092	-0.116	-0.140	-0.157	-0.137	-0.140	-0.175	-0.241	-0.152	-0.174	-0.201	-0.235	-0.224	-0.229	-0.225	-0.241	-0.279	-0.335	
	α, deg	6.017	600.6	-0.020	0.078	0.020	-0.011	-2.988	-0.009	3.016	5.998	9.035	0.022	0.003	0.000	-0.001	-0.012	-2.981	0.000	3.014	5.989	000.6	
	M _∞	1.199	1.200	1.151	0.950	0.926	0.899	0.900	0.903	0.902	0.901	0.900	0.877	0.848	0.802	0.701	0.600	0.601	0.602	0.602	0.602	0.601	

Table 11. Continued

(c) Continued

				Static	pressure coe	Static pressure coefficients on nozzle bottom flap at $v/Y = 0.50$	nozzle botton	flap at v/Y	= 0.50		
						with values of x/l of-	—Jo <i>I/x</i> : Jo				
M _∞	α, deg	.153	.226	.300	.337	.411	.558	.705	6 <i>LL</i>	.853	.926
1.199	6.017	-0.012	-0.021	-0.398	-0.547	-0.500	-0.503	-0.357	-0.182	-0.144	-0.121
1.200	600.6	-0.009	-0.016	-0.391	-0.542	-0.495	-0.506	-0.455	-0.451	-0.203	-0.126
1.151	-0.020	-0.030	-0.053	-0.464	-0.611	-0.582	-0.506	-0.205	-0.158	-0.129	-0.098
0.950	0.078	-0.096	-0.171	-0.755	-0.924	-0.752	-0.312	-0.195	-0.145	-0.099	-0.063
0.926	0.020	-0.122	-0.203	-0.804	-0.695	-0.385	-0.248	-0.165	-0.127	-0.091	-0.058
0.899	-0.011	-0.148	-0.233	-0.843	-0.528	-0.334	-0.218	-0.132	-0.096	-0.059	-0.030
0.600	-2.988	-0.156	-0.241	-0.869	-0.645	-0.398	-0.257	-0.144	-0.099	-0.055	-0.022
0.903	-0.009	-0.144	-0.230	-0.837	-0.535	-0.337	-0.227	-0.139	-0.101	-0.066	-0.037
0.905	3.016	-0.131	-0.212	-0.834	-0.581	-0.350	-0.233	-0.148	-0.111	-0.073	-0.040
0.901	5.998	-0.118	-0.194	-0.837	-0.762	-0.401	-0.251	-0.158	-0.116	-0.074	-0.032
0.900	9.035	-0.107	-0.180	-0.837	-1.005	-0.575	-0.284	-0.172	-0.117	-0.065	-0.016
0.877	0.022	-0.164	-0.258	-0.867	-0.486	-0.323	-0.198	-0.106	-0.064	-0.030	0.002
0.848	0.003	-0.187	-0.292	-0.931	-0.502	-0.329	-0.172	-0.066	-0.025	0.012	0.038
0.802	0.000	-0.222	-0.348	-1.089	-0.605	-0.325	-0.105	0.005	0.040	0.069	0.090
0.701	-0.001	-0.276	-0.445	-1.166	-0.512	-0.207	-0.014	0.084	0.118	0.147	0.172
0.600	-0.012	-0.272	-0.424	-0.880	-0.487	-0.207	-0.021	0.080	0.115	0.145	0.170
0.601	-2.981	-0.254	-0.394	-0.813	-0.442	-0.175	0.000	0.093	0.125	0.151	0.174
0.602	0.000	-0.273	-0.427	-0.884	-0.488	-0.208	-0.023	0.079	0.115	0.144	0.169
0.602	3.014	-0.287	-0.457	-1.013	-0.563	-0.259	-0.064	0.047	0.089	0.126	0.160
0.602	5.989	-0.293	-0.474	-1.127	-0.619	-0.301	-0.101	0.015	0.060	0.102	0.143
0.601	9.000	-0.289	-0.478	-1.207	-0.661	-0.332	-0.132	-0.014	0.033	0.077	0.124
0.401	-0.005	-0.248	-0.382	-0.736	-0.433	-0.195	-0.022	0.072	0.107	0.135	0.162

Table 11. Continued

(c) Concluded

			Stati	c pressure co	efficients on nozzle bott with values of x/l of—	nozzle botton of x/l of—	Static pressure coefficients on nozzle bottom flap at centerline with values of x/l of—	erline	
W	a, deg	.153	.226	.300	.337	.411	.558	.705	.926
1.199	6.017	-0.011	-0.033	-0.407	-0.534	-0.510	-0.494	-0.293	-0.123
1.200	600.6	-0.001	-0.022	-0.398	-0.526	-0.506	-0.490	-0.451	-0.125
1.151	-0.020	-0.032	-0.061	-0.459	-0.588	-0.570	-0.507	-0.204	-0.110
0.950	0.078	-0.107	-0.188	-0.754	-0.898	-0.759	-0.292	-0.186	-0.068
0.926	0.020	-0.130	-0.213	-0.797	-0.623	-0.364	-0.249	-0.172	-0.061
0.899	-0.011	-0.155	-0.239	-0.827	-0.486	-0.325	-0.218	-0.139	-0.030
0.900	-2.988	-0.161	-0.245	-0.868	-0.611	-0.387	-0.249	-0.148	-0.023
0.903	-0.009	-0.152	-0.236	-0.828	-0.504	-0.329	-0.220	-0.140	-0.037
0.905	3.016	-0.144	-0.229	-0.836	-0.538	-0.338	-0.227	-0.151	-0.041
0.901	5.998	-0.129	-0.218	-0.844	6290-	-0.385	-0.257	-0.170	-0.037
0.900	9.035	-0.116	-0.206	-0.852	-0.897	-0.519	-0.291	-0.185	-0.025
0.877	0.022	-0.169	-0.264	-0.862	-0.479	-0.316	-0.195	-0.107	0.003
0.848	0.003	-0.194	-0.298	-0.934	-0.506	-0.321	-0.170	-0.067	0.041
0.802	0.000	-0.233	-0.357	-1.094	-0.610	-0.324	-0.112	-0.002	0.093
0.701	-0.001	-0.292	-0.460	-1.199	-0.541	-0.236	-0.028	0.079	0.173
0.600	-0.012	-0.288	-0.437	-0.899	-0.507	-0.238	-0.035	0.070	0.172
0.601	2.981	-0.270	-0.409	-0.834	-0.465	-0.206	-0.011	0.084	0.175
0.602	0.000	-0.290	-0.439	-0.904	-0.509	-0.239	-0.036	0.068	0.171
0.602	3.014	-0.308	-0.470	-0.977	-0.566	-0.286	-0.076	0.035	0.159
0.602	5.989	-0.317	-0.490	-1.048	-0.611	-0.323	-0.111	0.004	0.142
0.601	000.6	-0.315	-0.496	-1.091	-0.640	-0.347	-0.136	-0.021	0.127
0.401	-0.005	-0.263	-0.389	-0.747	-0.445	-0.222	-0.039	0.059	0.164

Table 11. Concluded (d) Force data

ļ			
	M_{∞}	α, deg	c_D
Ŀ	661.	6.017	0.3050
	.200	600.6	0.3139
<u> </u>	1.151	-0.020	0.2989
Ö	0.950	0.078	0.2762
0	0.926	0.020	0.2313
0	0.899	-0.011	0.2027
0	0.000	-2.988	0.2276
0	0.903	-0.009	0.2044
0	0.902	3.016	0.2101
0	0.901	5.998	0.2315
0	0.900	9.035	0.2488
0	0.877	0.022	0.1864
0	0.848	0.003	0.1672
0	0.802	0.000	0.1335
0	0.701	-0.001	0.0748
0	0.600	-0.012	0.0709
0	0.601	-2.981	0.0682
0	0.602	0.000	0.0691
0	0.602	3.014	0.0715
0	0.602	5.989	0.0748
0	0.601	000.6	0.0846
0	0.401	-0.005	0.0687

Table 12. Pressure and Force Data for Nozzle 8 With $\beta_{t,lop/bot}$ = 15.0°/ $\beta_{t,side}$ = 22.4°, Plume On, and α = 0°

(a) Static pressure coefficients on nozzle top flap

	~~	_	_	~	_	_	_	_	_	_		_		
	.926	0.223	0.222	0.204	0.107	-0.085	-0.068	-0.034	-0.002	0.029	0.095	0.202	0.220	0.209
	.853	0.189	0.189	0.175	0.082	-0.110	-0.095	-0.063	-0.032	-0.001	0.069	0.171	0.184	0.174
	<i>6LL</i> :	0.148	0.147	0.137	0.051	-0.133	-0.119	-0.088	-0.060	-0.029	0.040	0.137	0.148	0.137
line	.705	0.103	0.102	0.094	0.019	-0.154	-0.140	-0.113	-0.086	-0.060	0.010	960.0	0.106	960.0
Static pressure coefficients on nozzle top flap at centerline with values of v/l of	.632	0.052	0.051	0.045	-0.023	-0.173	-0.163	-0.143	-0.119	-0.093	-0.029	0.047	0.054	0.052
efficients on nozzle top with values of v// of-	.558	-0.010	-0.011	-0.015	-0.076	-0.201	-0.190	-0.172	-0.153	-0.134	-0.081	-0.014	-0.010	-0.009
coefficients o	.484	-0.093	-0.093	-0.094	-0.153	-0.240	-0.223	-0.210	-0.197	-0.184	-0.155	-0.093	-0.091	-0.084
tic pressure	114.	-0.213	-0.214	-0.217	-0.270	-0.317	-0.279	-0.263	-0.252	-0.254	-0.266	-0.218	-0.216	-0.194
Sta	.337	-0.470	-0.469	-0.502	-0.513	-0.618	-0.449	-0.407	-0.389	-0.397	-0.493	-0.495	-0.466	-0.408
	.300	-0.965	-0.961	-1.266	-1.020	-0.789	-0.790	-0.774	-0.765	-0.797	-0.961	-1.220	-0.947	-0.778
	.226	-0.423	-0.423	-0.427	-0.333	-0.163	-0.191	-0.217	-0.245	-0.270	-0.328	-0.425	-0.417	-0.368
	.153	-0.280	-0.281	-0.278	-0.224	-0.102	-0.124	-0.144	-0.164	-0.182	-0.220	-0.277	-0.277	-0.250
	Μ∞	0.600	0.598	0.702	0.797	0.948	0.925	0.901	0.876	0.853	0.802	0.700	0.599	0.399

			Sta	tic pressure c	Static pressure coefficients on nozzle top flap at $y/Y = 0.50$	n nozzle top	flap at $y/Y =$	0.50		
	.153	.226	.300	.337	.411	411 558	705	770	853	926
0.600	-0.253	-0.392	-0.937	-0.444	-0.196	-0.007	010	0 149	0 180	0.23
0.598	-0.254	-0.391	-0.933	-0.442	-0.195	-0.007	0.101	0.148	0.188	0.222
0.702	-0.251	-0.395	-1.213	-0.462	-0.198	-0.017	0.089	0.134	0.172	0.205
0.797	-0.208	-0.315	-1.049	-0.523	-0.266	-0.073	0.020	0.055	0.084	0.110
0.948	-0.094	-0.156	-0.793	-0.717	-0.329	-0.197	-0.153	-0.131	-0.113	-0.086
0.925	-0.116	0.185	-0.822	-0.496	-0.289	-0.189	-0.143	-0.118	-0.095	-0.067
0.901	-0.137	-0.206	-0.805	-0.422	-0.269	-0.176	-0.119	-0.091	6.064 4.0064	-0.034
0.876	-0.155	-0.233	-0.802	-0.413	-0.264	-0.154	-0.092	-0.061	-0.032	-0.001
0.853	-0.174	-0.257	-0.836	-0.426	-0.265	-0.134	-0.061	-0.029	0000	0.030
0.802	-0.207	-0.311	-0.992	-0.511	-0.267	-0.078	0.012	0.044	0.073	0.099
0.700	-0.251	-0.394	-1.175	-0.460	-0.194	-0.016	0.088	0.130	0.170	0.202
0.599	-0.252	-0.390	-0.923	-0.444	-0.192	-0.005	0.103	0.145	0.186	0.220
0.399	-0.229	-0.347	-0.760	-0.391	-0.173	0.003	0.100	0.139	0.177	0.208

Table 12. Continued

(a) Concluded

				\neg									٦	\neg
	926	0.220	0.219	0.202	0.114	-0.087	-0.068	-0.035	-0.001	0.032	0.102	0.196	0.214	0.198
	.853	0.183	0.182	0.167	0.086	-0.113	-0.100	-0.063	-0.030	0.003	0.073	0.162	0.180	0.167
0.75	6 <i>LL</i>	0.141	0.140	0.122	0.054	-0.136	-0.122	-0.095	-0.063	-0.029	0.045	0.120	0.140	0.131
lap at $y/Y = 0$.705	0.100	0.099	0.075	0.023	-0.156	-0.147	-0.120	-0.093	-0.060	0.011	0.073	0.096	0.100
nozzle top f	.558	-0.003	-0.003	-0.032	-0.074	-0.204	-0.192	-0.178	-0.157	-0.134	-0.077	-0.029	-0.002	0.023
efficients on nozzle top with values of x/l of—	.411	-0.169	-0.169	-0.166	-0.233	-0.329	-0.292	-0.272	-0.266	-0.259	-0.235	-0.162	-0.168	-0.148
Static pressure coefficients on nozzle top flap at $y/Y = 0.75$ with values of x/l of—	.337	-0.400	-0.399	-0.395	-0.494	-0.686	-0.496	-0.437	-0.432	-0.444	-0.492	-0.393	-0.399	-0.353
Stat	.300	1	1	1		1			ł	1	ſ	1	1	-
	.226	1	-		ı	1	1	ı		1	1	1		_
	.153	-0.242	-0.241	-0.241	-0.215	-0.111	-0.134	-0.151	-0.169		-0.215	-0.240	-0.240	-0.220
	M	0.600	0.598	0.702	0.797	0.948	0.925	0.901	0.876	0.853	0.802	0.700	0.599	0.399

M _{cos} .153 .226 .300 .337 .411 .558 .779 .853 .926 0.600 -0.227 -0.344 -0.836 -0.153 -0.009 0.091 0.137 0.179 0.214 0.598 -0.227 -0.344 -0.834 -0.356 -0.153 -0.009 0.091 0.136 0.177 0.214 0.702 -0.227 -0.346 -0.900 -0.153 -0.009 0.091 0.136 0.177 0.217 0.702 -0.227 -0.344 -0.834 -0.356 -0.153 -0.009 0.091 0.136 0.177 0.212 0.707 -0.207 -0.318 -0.971 -0.210 -0.049 0.015 0.015 0.015 0.016 0.115 0.015 0.016 0.013 0.013 0.013 0.013 0.013 0.013 0.013 0.013 0.014 0.014 0.014 0.014 0.014 0.014<				_				_			_	_			_
Static pressure coefficients on nozzle top flap at $y/Y = 0.875$ i.153 .226 .300 .337 .411 .558 .705 .779 -0.227 -0.344 -0.836 -0.395 -0.153 -0.009 0.091 0.137 -0.227 -0.344 -0.834 -0.395 -0.153 -0.009 0.091 0.136 -0.225 -0.346 -0.900 -0.356 -0.153 -0.009 0.091 0.136 -0.225 -0.346 -0.900 -0.356 -0.150 -0.053 0.058 0.113 -0.107 -0.171 -0.736 -0.371 -0.210 -0.098 0.015 0.055 -0.107 -0.171 -0.736 -0.347 -0.210 -0.099 0.0015 0.025 -0.107 -0.199 -0.761 -0.217 -0.218 -0.186 -0.153 -0.125 -0.146 -0.225 -0.764 -0.377 -0.278 -0.186 -0.153 -0.028 -0.178 -0.272 -0.386 -0.258 -0.137 -0.061 -0.098 -0.178 -0.272 -0.827 -0.386 -0.258 -0.137 -0.061 -0.028 -0.222 -0.342 -0.887 -0.386 -0.211 -0.099 0.008 0.046 -0.222 -0.342 -0.887 -0.354 -0.144 -0.050 0.059 0.112 -0.224 -0.341 -0.821 -0.390 -0.150 0.009 0.098 0.137 -0.229 -0.315 -0.390 -0.150 0.003 0.098 0.127		.926	0.214	0.212	0.196	0.115	-0.088	-0.072	-0.036	-0.002	0.031	0.103	0.193	0.212	0.191
Static pressure coefficients on nozzle top flap at $y/Y = 0.8$ with values of x/I of— 1.53226300337411558705 -0.2270.3440.8360.3950.1530.009 . 0.091 -0.2270.3440.8340.3950.1530.009 . 0.091 -0.2250.3460.9000.3560.1500.009 . 0.091 -0.2070.3180.9710.3710.2100.098 . 0.015 -0.1070.1710.7360.4950.2250.2440.1710.130 -0.1300.1990.7610.4110.2930.2120.1530.153 -0.1460.2250.7640.3770.2780.1860.1530.164 -0.1630.2250.7640.3740.2780.1860.1530.095 -0.1780.2270.8870.3860.2580.1370.0610.203 -0.2220.3420.8870.3540.1440.050 . 0.059 -0.2240.3410.8210.3900.1500.010 . 0.092 -0.2090.3150.7090.3600.135 . 0.098		.853	0.179	0.177	0.160	0.088	-0.113	-0.097	-0.063	-0.029	0.004	0.077	0.157	0.177	0.159
.153 .226 .300 -0.227 -0.344 -0.83 -0.227 -0.344 -0.83 -0.225 -0.346 -0.90 -0.207 -0.318 -0.90 -0.130 -0.199 -0.75 -0.146 -0.225 -0.76 -0.163 -0.225 -0.78 -0.178 -0.212 -0.82 -0.22 -0.342 -0.88 -0.224 -0.315 -0.80	.875	977.	0.137	0.136	0.113	0.055	-0.143	-0.125	960'0-	-0.063	-0.028	0.046	0.112	0.137	0.127
.153 .226 .300 -0.227 -0.344 -0.83 -0.227 -0.344 -0.83 -0.225 -0.346 -0.90 -0.207 -0.318 -0.90 -0.130 -0.199 -0.75 -0.146 -0.225 -0.76 -0.163 -0.225 -0.78 -0.178 -0.212 -0.82 -0.22 -0.342 -0.88 -0.224 -0.315 -0.80	ap at $y/Y = 0$.705	0.091	0.091	0.058	0.015	-0.171	-0.153	-0.124	-0.095	-0.061	800.0	0.059	0.092	0.098
.153 .226 .300 -0.227 -0.344 -0.83 -0.227 -0.344 -0.83 -0.225 -0.346 -0.90 -0.207 -0.318 -0.90 -0.130 -0.199 -0.75 -0.146 -0.225 -0.76 -0.163 -0.225 -0.78 -0.178 -0.212 -0.82 -0.22 -0.342 -0.88 -0.224 -0.315 -0.80	nozzle top fl of x/l of—	.558	-0.009	600.0-	-0.053	860.0-	-0.244	-0.212	-0.186	-0.164	-0.137	660'0-	-0.050	-0.010	0.023
.153 .226 .300 -0.227 -0.344 -0.83 -0.227 -0.344 -0.83 -0.225 -0.346 -0.90 -0.207 -0.318 -0.90 -0.130 -0.199 -0.75 -0.146 -0.225 -0.76 -0.163 -0.225 -0.78 -0.178 -0.212 -0.82 -0.22 -0.342 -0.88 -0.224 -0.315 -0.80	efficients on with values	.411	-0.153	-0.153	-0.150	-0.210	-0.325	-0.293	-0.278	-0.271	-0.258	-0.211	-0.144	-0.150	-0.135
.153 .226 .300 -0.227 -0.344 -0.83 -0.227 -0.344 -0.83 -0.225 -0.346 -0.90 -0.207 -0.318 -0.90 -0.130 -0.199 -0.75 -0.146 -0.225 -0.76 -0.163 -0.225 -0.78 -0.178 -0.212 -0.82 -0.22 -0.342 -0.88 -0.224 -0.315 -0.80	c pressure co	.337	-0.395	-0.395	-0.356	-0.371	-0.495	-0.411	-0.377	-0.374	-0.386	-0.380	-0.354	-0.390	-0.360
.153 -0.227 -0.227 -0.207 -0.107 -0.130 -0.146 -0.163 -0.178 -0.203 -0.203 -0.224 -0.224	Stati	300	-0.836	-0.834	-0.900	-0.971	-0.736	-0.761	-0.764	-0.787	-0.827	-0.940	-0.887	-0.821	-0.709
.153 .0.22 .0.22 .0.13 .0.13 .0.13 .0.22 .0.22		.226	-0.344	-0.344	-0.346	-0.318	-0.171	-0.199	-0.225	-0.250	-0.272	-0.312	-0.342	-0.341	-0.315
M _∞ 0.600 0.598 0.702 0.702 0.948 0.925 0.901 0.876 0.863 0.700 0.700 0.700		.153	-0.227	-0.227	-0.225	-0.207	-0.107			-0.163		-0.203	-0.222	-0.224	
		W	0.600	0.598	0.702	0.797	0.948	0.925	0.901	0.876	0.853	0.802	0.700	0.599	0,399

Table 12. Continued

(b) Static pressure coefficients on nozzle sidewall

			Static pres	Static pressure coefficients on corner between nozzle top flap and sidewall	ents on corner	between noz	zle top flap a	nd sidewall		
					with values	with values of x/l of-				
M _∞	.153	.226	300	.337	.411	.558	207.	622	.853	926
0.600	-0.227	1	-0.869	-0.386	-0.128	-0.007	0.085	0.129	0.170	0.208
0.598	-0.227	1	-0.867	-0.383	-0.127	-0.008	0.084	0.128	0.169	0.205
0.702	-0.223	+	-0.903	-0.315	0.141	-0.068	0.040	960'0	0.149	0.188
0.797	-0.207	1	-0.949	-0.352	-0.206	-0.114	-0.005	0.046	0.085	0.111
0.948	-0.106	1	-0.719	-0.445	-0.325	-0.262	-0.192	-0.156	-0.129	-0.101
0.925	-0.128	1	-0.737	-0.384	-0.293	-0.228	-0.162	-0.132	-0.107	-0.081
0.901	-0.146	-	-0.742	-0.358	-0.281	-0.197	-0.129	-0.099	-0.073	-0.046
0.876	-0.163	-	-0.766	-0.359	-0.273	_0.172	-0.097	-0.066	-0.037	-0.010
0.853	-0.179	1	-0.811	-0.368	-0.264	-0.143	-0.062	-0.029	0.000	0.023
0.802	-0.204		-0.923	-0.361	-0.207	0.114	-0.010	0.035	0.073	0.097
0.700	-0.220	1	-0.888	-0.314	-0.134	-0.065	0.038	0.093	0.144	0.182
0.599	-0.224	-	-0.852	-0.381	[-0.125	-0.008	0.085	0.125	0.167	0.204
0.399	-0.215	1	-0.751	-0.363	-0.107	0.039	0.089	0.115	0.147	0.181

			Stat	ic pressure c	oefficients or	Static pressure coefficients on nozzle sidewall at $z/Z = 0.50$	wall at $z/Z = -$	0.50		
					with value	with values of x/l of-				
M_{∞}	.153	.226	.300	.337	.411	.558	.705	<i>6LL</i> :	.853	.926
0.600	-0.218	-0.348	-0.745	-0.369	-0.144	-0.046	0.070	0.129	0.180	0.213
0.598	-0.217	-0.347	-0.739	-0.362	-0.144	-0.046	0.068	0.128	0.179	0.213
0.702	-0.210	-0.332	-0.660	-0.222	-0.161	-0.115	0.015	0.092	0.152	0.190
0.797	-0.195	-0.312	-0.746	-0.235	-0.199	-0.167	-0.029	0.045	0.097	0.131
0.948	-0.099	-0.167	-0.700	-0.365	-0.295	-0.275	-0.199	-0.157	-0.113	-0.068
0.925	-0.123	-0.195	-0.698	-0.310	-0.263	-0.246	-0.172	-0.130	-0.086	-0.044
0.901	-0.137	-0.220	-0.707	-0.295	-0.252	-0.218	-0.139	-0.095	-0.051	-0.009
0.876	-0.156	-0.246	-0.731	-0.297	-0.252	-0.207	-0.106	-0.056	-0.014	0.026
0.853	-0.170	-0.268	-0.770	-0.302	-0.248	-0.187	-0.074	-0.020	0.025	090.0
0.802	-0.195	-0.309	-0.742	-0.238	-0.198	-0.169	-0.037	0.040	0.089	0.125
0.700	-0.209	-0.329	-0.657	-0.223	-0.157	-0.112	0.013	0.088	0.148	0.186
0.599	-0.218	-0.345	-0.731	-0.361	-0.141	-0.049	890.0	0.130	0.179	0.213
0.399	-0.209	-0.335	-0.719	-0.467	880.0-	0.041	060'0	0.112	0.146	0.185

Table 12. Continued

(b) Concluded

926 ; 1 1 1 1 ı 1 ī ı 1 0.145 0.140 0.179 0.179 0.149 0.095 -0.088 0.026 -0.114 -0.053-0.0140.181 .853 -0.162 -0.136 -0.026 0.110 0.126 0.128 0.039 -0.064-0.100 0.083 0.033 -0.206 -0.117 0.066 -0.035 0.010 0.085 -0.1470.067 -0.041 705 Static pressure coefficients on nozzle sidewall at centerline 0.00 -0.240 -0.190 .632 -0.168-0.147-0.1170.0059 0.066 -0.111 with values of x/l of--0.210 -0.263 -0.237 -0.218 -0.052-0.166-0.172-0.1130.042 -0.053-0.057 9.1.9 .558 -0.224 -0.220 -0.106 -0.234 -0.223 -0.108-0.264-0.149-0.190 -0.146-0.110 -0.191 0.001 .484 -0.152 -0.176 -0.212 -0.148 -0.149 -0.219 -0.150-0.253-0.209 -0.174-0.0774. -0.226 -0.213 -0.210 -0.165 -0.167 -0.174 -0.277-0.267-0.267-0.172-0.471 337 -0.641 -0.597 -0.575 -0.552 -0.558 -0.566 -0.502 -0.571 -0.739 -0.687 -0.687 300 -0.366 -0.365-0.342 -0.276-0.319 -0.336-0.358-0.365-0.174-0.225.226 -0.201-0.251-0.232 -0.230 -0.218 -0.202 -0.203-0.218-0.100 -0.140-0.158-0.232-0.176-0.231-0.123.153 0.876 0.853 0.700 0.600 0.702 0.797 0.948 0.925 0.599 0.399 ×

	.926	0.209	0.209	0.187	0.135	-0.079	-0.059	-0.020	0.018	0.058	0.125	0.180	0.203	0.181
	.705	0.074	0.074	0.018	-0.036	-0.217	-0.192	-0.163	-0.128	-0.095	-0.043	0.016	0.073	0.092
3	.558	-0.042	-0.039	-0.110	-0.173	-0.264	-0.243	-0.230	-0.222	-0.205	-0.173	-0.110	-0.048	0.042
ot x/l ot—	.411	-	***		_		_	_	-		_		***	1
with values	.337	-0.386	-0.399	-0.238	-0.210	-0.292	-0.236	-0.210	-0.210	-0.207	-0.205	-0.232	-0.376	-0.468
	300	-0.765	0.770	-0.697	-0.694	-0.668	-0.632	-0.611	-0.615	-0.618	629.0-	8/9.0-	-0.747	-0.729
	.226	-0.346	-0.345	-0.330	-0.305	-0.161	-0.190	-0.213	-0.240	-0.262	-0.304	-0.324	-0.340	-0.336
	.153	-0.221	-0.221	-0.213	-0.197	-0.095	-0.116	-0.134	-0.152	-0.166	-0.190	-0.208	-0.216	-0.210
	M	0.600	0.598	0.702	0.797	0.948	0.925	0.901	0.876	0.853	0.802	0.700	0.599	0.399
	with values of x/l of—	.153 .226 .300 .337 .411 .558 .705	.153 .226 .300 .337 .411 .558 .7050.221 -0.346 -0.765 -0.386 - 0.042 0.074	153 .226 .300 .337 .411 .558 .705 .0521 .0.346 .0.765 .0.386 . 0.042 0.074 .0.345 .0.770 .0.399 . 0.039 0.074 .0.042 .0.042 .0.042 .0.042 .0.044 .0.042 .0.044	153 .226 .300 .337 .411 .558 .705 .226 .226 .0.366 .0.386	153 .226 .300 .337 .411 .558 .705 .205 .226 .300 .337 .411 .558 .705 .205 .226 .0.346 .0.765 .0.386 0.042 0.074 .0.221 .0.345 .0.770 .0.399 0.039 0.074 .0.213 .0.330 .0.697 .0.238 0.110 0.018 .0.197 .0.305 .0.694 .0.210 0.173 .0.036 .	153 .226 .300 .337 .411 .558 .705 .226 .226 .200 .337 .411 .558 .705 .226 .226 .0.366 0.042 0.074 .0.221 .0.345 .0.770 .0.399 0.039 0.074 .0.213 .0.330 .0.697 .0.238 0.110 0.018 .0.197 .0.305 .0.694 .0.210 0.173 .0.036 .0.095 0.161 .0.668 .0.292 0.264 .0.217	153 .226 .300 .337 .411 .558 .705 .2021 .0.346 .0.765 .0.386	153 .226 .300 .337 .411 .558 .705 .226 .300 .337 .411 .558 .705 .226 .226 .226 .2366 .2366 .237 .411 .558 .705 .226 .221 .0.345 .0.770 .0.399 0.039 0.074 .0.213 .0.330 .0.697 .0.238 0.110 0.018 .2019 .0.197 .0.305 .0.694 .0.210 0.173 .0.036 .0.095 .0.161 .0.668 .0.292 0.264 .0.217 .0.217 .0.116 .0.190 .0.632 .0.236 .0.243 .0.192 .0.134 .0.213 .0.210 0.230 .0.163 .0.163 .0.210 0.230 .0.163 .0.230 .0.163 .0.230 .0.230 .0.235 .0.264 .0.26	with values of xif of— .153 .226 .300 .337 .411 .558 .705 -0.221 -0.346 -0.765 -0.386 - -0.042 0.074 -0.221 -0.345 -0.770 -0.399 - -0.039 0.074 -0.213 -0.330 -0.697 -0.238 - -0.110 0.018 -0.197 -0.305 -0.694 -0.210 - -0.173 -0.036 -0.095 -0.161 -0.668 -0.292 - -0.264 -0.217 -0.116 -0.190 -0.632 -0.236 - -0.243 -0.192 -0.134 -0.213 -0.210 - -0.243 -0.163 -0.163 -0.134 -0.213 -0.210 - -0.230 -0.163 -0.163	with values of xif of— .153 .226 .300 .337 .411 .558 .705 -0.221 -0.346 -0.765 -0.386 - -0.042 0.074 -0.221 -0.345 -0.770 -0.399 - -0.039 0.074 -0.213 -0.305 -0.694 -0.210 - -0.110 0.018 -0.197 -0.161 -0.668 -0.292 - -0.173 -0.036 -0.116 -0.190 -0.632 -0.236 - -0.244 -0.192 -0.113 -0.191 -0.611 -0.210 - -0.243 -0.192 -0.134 -0.213 -0.611 -0.210 - -0.230 -0.163 -0.152 -0.240 -0.611 -0.210 - -0.230 -0.163 -0.156 -0.240 -0.618 -0.207 - -0.222 -0.128	with values of xif of— .153 .226 .300 .337 .411 .558 .705 -0.221 -0.346 -0.765 -0.386 - -0.042 0.074 -0.221 -0.345 -0.770 -0.399 - -0.039 0.074 -0.213 -0.305 -0.697 -0.238 - -0.110 0.018 -0.197 -0.305 -0.694 -0.210 - -0.173 -0.036 -0.095 -0.161 -0.668 -0.292 - -0.173 -0.197 -0.154 -0.190 -0.632 -0.236 - -0.244 -0.197 -0.134 -0.213 -0.611 -0.210 - -0.243 -0.163 -0.155 -0.240 -0.615 -0.210 - -0.230 -0.163 -0.166 -0.262 -0.618 -0.207 - -0.222 -0.128 -0.166 -0.267 -0.205 - -0.205 -0.095 <t< td=""><td>with values of xif of— .153 .226 .300 .337 .411 .558 .705 -0.221 -0.346 -0.765 -0.386 - -0.042 0.074 -0.221 -0.345 -0.770 -0.399 - -0.039 0.074 -0.213 -0.30 -0.694 -0.210 - -0.110 0.018 -0.197 -0.305 -0.688 -0.292 - -0.173 -0.036 -0.116 -0.668 -0.292 - -0.264 -0.217 - -0.134 -0.190 -0.632 -0.236 - -0.163 - -0.134 -0.213 -0.611 -0.210 - -0.243 -0.192 -0.155 -0.240 -0.613 -0.210 - -0.230 -0.163 -0.156 -0.240 -0.618 -0.207 - -0.222 -0.128 -0.166 -0.262 -0.618 -0.205 - -0.205 -0.095 <t< td=""><td>with values of xif of— .153 .226 .300 .337 .411 .558 .705 -0.221 -0.346 -0.765 -0.386 - -0.042 0.074 -0.221 -0.345 -0.770 -0.399 - -0.039 0.074 -0.213 -0.305 -0.694 -0.238 - -0.110 0.018 -0.197 -0.305 -0.694 -0.292 - -0.173 -0.036 -0.161 -0.668 -0.292 - -0.264 -0.217 - -0.134 -0.190 -0.632 -0.292 - -0.264 -0.192 -0.134 -0.213 -0.611 -0.210 - -0.244 -0.192 -0.152 -0.240 -0.615 -0.210 - -0.230 -0.163 -0.156 -0.262 -0.618 -0.207 - -0.222 -0.128 -0.156 -0.304 -0.678 -0.205 - -0.173 -0.043</td></t<></td></t<>	with values of xif of— .153 .226 .300 .337 .411 .558 .705 -0.221 -0.346 -0.765 -0.386 - -0.042 0.074 -0.221 -0.345 -0.770 -0.399 - -0.039 0.074 -0.213 -0.30 -0.694 -0.210 - -0.110 0.018 -0.197 -0.305 -0.688 -0.292 - -0.173 -0.036 -0.116 -0.668 -0.292 - -0.264 -0.217 - -0.134 -0.190 -0.632 -0.236 - -0.163 - -0.134 -0.213 -0.611 -0.210 - -0.243 -0.192 -0.155 -0.240 -0.613 -0.210 - -0.230 -0.163 -0.156 -0.240 -0.618 -0.207 - -0.222 -0.128 -0.166 -0.262 -0.618 -0.205 - -0.205 -0.095 <t< td=""><td>with values of xif of— .153 .226 .300 .337 .411 .558 .705 -0.221 -0.346 -0.765 -0.386 - -0.042 0.074 -0.221 -0.345 -0.770 -0.399 - -0.039 0.074 -0.213 -0.305 -0.694 -0.238 - -0.110 0.018 -0.197 -0.305 -0.694 -0.292 - -0.173 -0.036 -0.161 -0.668 -0.292 - -0.264 -0.217 - -0.134 -0.190 -0.632 -0.292 - -0.264 -0.192 -0.134 -0.213 -0.611 -0.210 - -0.244 -0.192 -0.152 -0.240 -0.615 -0.210 - -0.230 -0.163 -0.156 -0.262 -0.618 -0.207 - -0.222 -0.128 -0.156 -0.304 -0.678 -0.205 - -0.173 -0.043</td></t<>	with values of xif of— .153 .226 .300 .337 .411 .558 .705 -0.221 -0.346 -0.765 -0.386 - -0.042 0.074 -0.221 -0.345 -0.770 -0.399 - -0.039 0.074 -0.213 -0.305 -0.694 -0.238 - -0.110 0.018 -0.197 -0.305 -0.694 -0.292 - -0.173 -0.036 -0.161 -0.668 -0.292 - -0.264 -0.217 - -0.134 -0.190 -0.632 -0.292 - -0.264 -0.192 -0.134 -0.213 -0.611 -0.210 - -0.244 -0.192 -0.152 -0.240 -0.615 -0.210 - -0.230 -0.163 -0.156 -0.262 -0.618 -0.207 - -0.222 -0.128 -0.156 -0.304 -0.678 -0.205 - -0.173 -0.043

Table 12. Continued

(c) Static pressure coefficients on nozzle bottom flap

	.926	0.212	0.210	0.197	0.140	-0.049	-0.038	-0.011	0.025	090.0	0.132	0.194	0.208	0.192
	.853	0.174	0.173	0.158	0.106	-0.103	-0.082	-0.045	-0.010	0.026	0.096	0.155	0.172	0.158
= 0.875	677.	0.132	0.131	0.109	0.063	-0.169	-0.133	-0.088	-0.050	-0.012	0.059	0.109	0.133	0.128
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.875$ with values of x/I of—	705.	0.088	0.087	0.057	0.013	-0.237	-0.199	-0.146	-0.101	-0.063	0.007	0.054	0.085	0.091
cients on nozzle botton with values of x/l of—	.558	-0.010	-0.009	-0.045	-0.109	-0.300	-0.288	-0.257	-0.219	-0.183	-0.115	-0.046	-0.010	0.016
fficients on r	.411	-0.158	-0.158	-0.150	-0.219	-0.305	-0.267	-0.263	-0.269	-0.267	-0.220	-0.147	-0.155	-0.147
pressure coe	.337	-0.404	-0.403	-0.374	-0.383	-0.400	-0.321	-0.301	-0.310	-0.327	-0.376	-0.363	-0.393	-0.371
Static	.300	-0.853	-0.846	-0.939	-0.915	-0.706	-0.643	-0.628	-0.656	-0.697	-0.873	-0.915	-0.836	-0.731
	.226	-0.332	-0.331	-0.334	-0.301	-0.160	-0.188	-0.211	-0.236	-0.256	-0.298	-0.328	-0.327	-0.303
	.153	-0.222	-0.222	-0.218	-0.201	-0.100	-0.123	-0.139	-0.157	-0.171	-0.197	-0.214	-0.219	-0.208
	M∞	0.600	0.598	0.702	0.797	0.948	0.925	0.901	0.876	0.853	0.802	0.700	0.599	0.399

0.50 .779 .853 .926 0.139 0.181 0.223 0.138 0.180 0.222 0.127 0.171 0.213 0.078 0.116 0.149 -0.095 -0.057 -0.027 -0.091 -0.056 -0.027 -0.072 -0.037 -0.008 -0.043 -0.003 0.026 -0.004 0.003 0.065 0.070 0.108 0.140 0.125 0.169 0.211	H	0 204
25 25 27 27 27 27 25	<u>ي</u>	
.50 .0.139 0.138 0.078 0.078 0.095 0.095 0.091 0.043 0.043 0.043 0.043	0.180	0 168
	0.138	0 133
705 -705 0.093 0.093 0.081 0.036 -0.137 -0.128 -0.104 -0.078 -0.043 0.029	0.092	060
icients on nozzle botton with values of x/l of— .411 .558 .0.200 .0.016 .0.199 .0.015 .0.205 .0.026 .0.289 .0.072 .0.459 .0.243 .0.371 .0.221 .0.371 .0.190 .0.371 .0.190 .0.371 .0.190 .0.371 .0.190 .0.371 .0.190 .0.370 .0.190 .0.370 .0.190	-0.018	0.01
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.50$ with values of x/l of— 0 .337 .411 .558 .705 .77 09 .0.443 .0.200 .0.016 0.093 0.1 24 .0.441 .0.199 .0.015 0.093 0.1 24 .0.465 .0.205 .0.026 0.081 0.1 24 .0.586 .0.289 .0.072 0.036 0.0 25 .0.747 .0.371 .0.243 .0.137 .0.0 26 .0.576 .0.371 .0.221 .0.128 .0.0 27 .0.576 .0.330 .0.190 .0.104 .0.0 28 .0.525 .0.317 .0.170 .0.078 .0.0 29 .0.526 .0.291 .0.145 .0.078 .0.0 20 .0.569 .0.291 .0.086 0.029 0.0	961.0-	-0.179
.337 -0.443 -0.441 -0.465 -0.586 -0.882 -0.747 -0.576 -0.525 -0.525 -0.526	-0.437	-0.390
Static -0.909 -0.904 -1.164 -1.144 -0.806 -0.856 -0.856 -0.931 -0.965 -1.090 -1.090	-0.893	-0.747
.226 -0.387 -0.386 -0.397 -0.321 -0.162 -0.190 -0.214 -0.240 -0.264 -0.317 -0.394	-0.383	-0.342
.153 		1
0.600 0.508 0.702 0.797 0.948 0.925 0.901 0.876 0.876 0.876 0.802	0.599	0.399

Table 12. Concluded

(c) Concluded

0.598 -0.267	ŀ		() 	with values of 1// of—			
	977	.300	.337	.411	.558	.705	.926
\forall	7 -0.397	-0.908	-0.454	-0.218	-0.026	0.086	0.229
t	7 –0.396	-0.907	-0.454	-0.218	-0.027	0.086	0.229
	1 -0.414	-1.179	-0.492	-0.227	-0.030	0.081	0.224
0.797 -0.223	3 –0.335	-1.185	-0.643	-0.303	890:0-	0.042	0.158
L	7 -0.177	-0.815	-0.889	-0.697	-0.205	-0.110	-0.014
┢	6 -0.198	-0.869	-0.868	-0.402	-0.199	-0.111	-0.020
┢	8 -0.222	-0.907	-0.592	-0.351	-0.190	-0.102	-0.004
t	6 -0.247	-0.935	-0.540	-0.337	-0.168	-0.074	0.029
H	0 -0.273	-0.975	-0.549	-0.329	-0.144	-0.038	0.070
0.802 -0.217	7 -0.330	-1.130	-0.620	-0.310	-0.080	0.035	0.144
t		-1.137	-0.486	-0.227	-0.032	0.080	0.221
\vdash		-0.893	-0.448	-0.216	-0.028	0.086	0.225
	9 –0.348	-0.741	-0.390	-0.197	-0.027	0.078	0.211

(d) Force data

c_{Df}	0.0115	0.0112	0.0110	0.0108	0.0108	0.0109	0.0109	0.0110	0.0111	0.0113	0.0116	0.0123
$C_{D,p}$	0.0684	0.0902	0.1307	0.2333	0.2092	0.1888	0.1730	0.1595	0.1317	0.0881	0.0674	0.0520
a_{2}	0.0482	2290.0	0.1146	0.2365	0.2054	0.1822	0.1648	0.1475	0.1147	0.0677	0.0473	0.0325
M	0.598	0.702	0.797	0.948	0.925	106.0	928.0	0.853	0.802	0.700	0.599	0.399

Table 13. Pressure and Force Data for Nozzle 8 With $\beta_{t,top/bot} = 15.0^{\circ}/\beta_{t,side} = 22.4^{\circ}$ and Plume Off

(a) Static pressure coefficients on nozzle top flap

					Str	tic pressure	coefficients c	efficients on nozzle top with values of v/l of—	Static pressure coefficients on nozzle top flap at centerline with values of $y/$ of	line			
M	α, deg	.153	.226	300	.337	114.	.484	.558	.632	.705	<i>6LL</i> :	.853	.926
0.952	0.001	-0.098	-0.158	-0.787	-0.771	-0.390	-0.232	-0.188	-0.165	-0.148	-0.127	-0.109	-0.085
0.923	-0.007	-0.125	-0.192	-0.801	-0.535	-0.294	-0.224	-0.187	-0.162	-0.141	-0.115	-0.092	-0.063
0.901	0.010	-0.144	-0.217	-0.774	-0.416	-0.265	-0.211	-0.179	-0.152	-0.128	-0.101	-0.073	-0.040
0.898	-2.990	-0.135	-0.204	-0.835	-0.524	-0.306	-0.238	-0.204	-0.175	-0.149	-0.119	-0.089	-0.052
0.900	0.013	-0.146	-0.218	-0.779	-0.416	-0.269	-0.216	-0.184	-0.154	-0.129	40.104	-0.077	-0.043
0.898	3.014	-0.155	-0.231	-0.776	-0.416	-0.274	-0.221	-0.186	-0.154	-0.124	-0.090	-0.059	-0.021
0.898	5.999	-0.159	-0.233	998.0-	-0.550	-0.337	-0.266	-0.218	-0.171	-0.127	-0.084	-0.043	0.005
0.901	9.018	-0.161	-0.226	606:0-	-1.002	-0.484	-0.302	-0.232	-0.166	-0.104	-0.048	0.001	0.050
0.877	-0.016	-0.162	-0.242	7777	-0.394	-0.256	-0.202	-0.163	-0.129	-0.101	-0.070	-0.044	-0.012
0.849	-0.003	-0.186	-0.275	-0.814	-0.405	-0.262	-0.190	-0.141	-0.101	690:0-	-0.039	600:0-	0.022
0.801	-0.010	-0.219	-0.325	086.0-	-0.502	-0.281	-0.170	-0.098	-0.043	-0.002	0.032	0.063	0.089
0.703	0.004	-0.282	-0.430	-1.294	-0.539	-0.238	-0.111	-0.035	0.025	0.070	0.109	0.143	0.172
0.603	-0.006	-0.285	-0.431	-0.988	-0.491	-0.233	-0.111	-0.034	0.026	0.072	0.110	0.143	0.174
0.603	-2.990	-0.303	-0.463	-1.111	-0.552	-0.281	-0.153	-0.072	-0.010	0.041	0.084	0.123	0.161
0.603	0.018	-0.286	-0.432	-0.987	-0.491	-0.234	-0.112	-0.034	0.025	0.071	0.109	0.141	0.172
0.602	3.028	-0.267	-0.403	-0.896	-0.446	-0.203	-0.087	-0.013	0.042	0.085	0.117	0.145	0.173
0.601	5.994	-0.253	-0.385	698.0-	-0.431	-0.195	-0.081	-0.009	0.042	0.083	0.110	0.134	0.159
0.602	8.988	-0.247	-0.384	-0.924	-0.453	-0.210	-0.094	-0.022	0.028	0.068	0.093	0.115	0.140
0.400	0.018	-0.259	-0.382	-0.799	-0.429	-0.211	-0.103	-0.030	0.025	0.067	0.102	0.134	0.163

Table 13. Continued

0.009 -0.0120.026 0.162 0.159 0.143 -0.019 0.161 -0.0390.040 0.171 -0.089926 -0.063-0.0510.066 0.123 -0.074-0.059-0.0380.000 -0.045 0.144 0.144 0.127 0.14 0.137 -0.095-0.074 0.147 -0.091.853 -0.076 0.110 0.113 0.112 0.119 0.099 0.110 -0.094 -0.049-0.0390.035 0.090 0.112 -0.122-0.102 -0.134-0.123622 9.10 -0.081Static pressure coefficients on nozzle top flap at y/Y = 0.500.045 0.075 -0.104 -0.108 -0.074 0.070 0.074 0.085 -0.126-0.124-0.150 -0.147-0.156-0.001 0.081 -0.131705 -0.13 with values of x/l of--0.014 -0.189 -0.064 -0.188 -0.033 -0.006 -0.185 -0.224-0.173-0.147 -0.0946.08 -0.187 -0.186-0.211 .558 -0.192-0.426 -0.178-0.193-0.354-0.429-0.280 -0.289-0.183-0.290-0.297-0.279-0.218-0.212-0.212-0.336-0.287-0.261<u>4</u>. -0.410 -0.426 -0.443-0.675 -1.020 -0.447 -0.530-0.420-0.832 -0.478 -0.676 -0.432-0.472-0.501-0.465-0.467-0.467.337 -0.964 -0.965 -0.937 -0.913 -0.925 -0.869-1.023 -1.256 -0.904 -0.838 -0.840-0.838 -0.892 -0.793-0.831-0.406 -0.374-0.354 -0.366-0.359-0.247 -0.232 -0.265 -0.404 -0.435 -0.183 -0.210-0.314-0.404-0.149 -0.198 -0.223-0.232.226 -0.186 -0.154 -0.207 -0.258 -0.176-0.260-0.243-0.233 -0.235 -0.150-0.163 -0.118-0.138-0.276-0.137-0.129-0.261-0.091 .153 α, deg -0.010-0.006 0.018 5.994 8.988 0.018 3.014 9.018 0.004 -2.9903.028 -2.990 -0.003 -0.016 0.010 0.013 0.001 -0.007 0.400 0.898 0.898 0.877 0.703 0.603 0.603 0.602 0.602 0.898 0.601 0.901 0.801 0.952 M 8 0.90

Table 13. Continued

	_	$\overline{}$	_	_	T -	_		_	_	_	~	_	_	-	_	_		_	_	_
	926	7000	9900	-0.042	-0.052	-0.043	-0.022	0.008	0.041	-0.013	0.028	0.092	0.172	0.171	0.163	0.170	0.168	0.156	0.143	0.157
	.853	-0.123	-0.098	-0.073	-0.087	-0.073	-0.060	-0.038	-0.006	-0.043	-0.005	0.066	0.142	0.144	0.133	0.143	0.146	0.138	0.130	0.134
0.75	677.	-0.143	-0.126	-0.104	-0.123	-0.104	-0.096	-0.082	-0.052	-0.076	-0.038	0.035	0.106	0.113	960.0	0.113	0.119	0.116	0.113	0.108
Static pressure coefficients on nozzle top flap at y/Y = 0.75 with values of y/ of—	.705	-0.161	-0.149	-0.133	-0.155	-0.134	-0.127	-0.124	-0.102	-0.109	-0.071	0.001	990.0	0.078	0.054	0.077	0.086	0.085	0.085	0.083
	.558	-0.213	-0.199	-0.188	-0.220	-0.191	-0.190	-0.211	-0.223	-0.175	-0.146	-0.088	-0.036	-0.016	-0.053	-0.016	-0.001	0.005	0.010	0.002
	.411	-0.379	-0.313	-0.293	-0.346	-0.290	-0.305	-0.362	-0.432	-0.286	-0.282	-0.267	-0.193	-0.188	-0.243	-0.190	-0.157	-0.145	-0.135	-0.167
	.337	-0.791	-0.619	-0.502	-0.696	-0.489	-0.493	809:0-	-0.831	-0.464	-0.474	-0.536	-0.438	-0.422	-0.499	-0.425	-0.363	-0.339	-0.332	-0.374
	300	1			-	1	-	-	ı	1	1	1	-	ı	_	-	_	1	ı	1
	.226	-0.150	-0.183	-0.208	-0.193	-0.211	-0.237	-0.252	-0.265	-0.231	-0.263	-0.303	-0.368	-0.360	-0.385	-0.363	-0.339	-0.332	-0.338	-0.321
	.153	-0.105	-0.131	-0.151	-0.152	-0.153	-0.168	-0.182	-0.196	-0.166	-0.186	-0.213	-0.246	-0.248	-0.263	-0.249	-0.241	-0.241	-0.247	-0.223
	α, deg	0.001	-0.007	0.010	-2.990	0.013	3.014	5.999	9.018	-0.016	-0.003	-0.010	0.004	-0.006	-2.990	0.018	3.028	5.994	8.988	0.018
	M_{∞}	0.952	0.923	0.901	0.898	0.900	0.898	0.898	0.901	0.877	0.849	0.801	0.703	0.603	0.603	0.603	0.602	0.601	0.602	0.400

Table 13. Continued

(a) Concluded

a, deg .153 .226 .300 .337 0.001 -0.104 -0.167 -0.732 -0.607 -0.007 -0.130 -0.200 -0.786 -0.491 0.010 -0.149 -0.225 -0.813 -0.447 -2.990 -0.156 -0.226 -0.845 -0.447 -2.990 -0.156 -0.226 -0.845 -0.447 0.013 -0.156 -0.226 -0.845 -0.447 0.013 -0.156 -0.226 -0.845 -0.447 0.013 -0.156 -0.226 -0.845 -0.447 0.014 -0.126 -0.226 -0.843 -0.435 0.018 -0.183 -0.247 -0.869 -0.514 0.004 -0.183 -0.247 -0.896 -0.439 0.004 -0.235 -0.360 -0.990 -0.409 0.006 -0.235 -0.360 -0.990 -0.409 0.018 -0.235 -0.360 -0.990 -0.409 0.018 -0.236 -0.360 -0.990 -0.420			_	 -	 -	_	_	_		 -	_			_	_	-		_	_	_	
a. deg .153 .226 .300 .378 .411 .588 .779 0.001 -0.104 -0.167 -0.732 -0.607 -0.169 -0.192 -0.160 -0.106 -0.116 -0.116 -0.115 -0.106 -0.116 -0.116 -0.115 -0.120 -0.120 -0.120 -0.106 -0.118 -0.120 -0.125 -0.124 -0.254 -0.206 -0.139 -0.116 -0.116 -0.116 -0.118 -0.126 -0.125 -0.124 -0.244 -0.246 -0.246 -0.139 -0.139 -0.118 -0.139 -0.139 -0.139 -0.139 -0.139 -0.139 -0.139 -0.140 -0.244 -0.236 -0.139 -0.139		.926	-0.100	-0.069	-0.042	-0.054	-0.044	-0.019	0.007	0.035	-0.012	0.026	0.094	0.170	0.171	0.166	0.169	0.171	0.160	0.145	0.154
α, deg Static pressure coefficients on nozzle top flap at y/Y = 0.8 α, deg .153 .226 .300 .337 .411 .558 .705 0.001 -0.104 -0.167 -0.732 -0.607 -0.362 -0.269 -0.192 -0.007 -0.130 -0.200 -0.786 -0.491 -0.322 -0.269 -0.192 -0.007 -0.130 -0.225 -0.813 -0.447 -0.322 -0.233 -0.164 -2.990 -0.156 -0.226 -0.845 -0.342 -0.238 -0.139 -2.990 -0.156 -0.226 -0.845 -0.342 -0.255 -0.162 0.013 -0.156 -0.226 -0.845 -0.247 -0.326 -0.139 0.013 -0.156 -0.226 -0.813 -0.244 -0.206 -0.139 0.018 -0.18 -0.271 -0.789 -0.144 -0.294 -0.207 -0.130 0.016 -0.164 -0.279 -0.269 -0.279 <t< td=""><td></td><td>.853</td><td>-0.129</td><td>-0.099</td><td>-0.074</td><td>-0.086</td><td>-0.075</td><td>-0.057</td><td>-0.037</td><td>-0.010</td><td>-0.043</td><td>-0.004</td><td>0.068</td><td>0.142</td><td>0.146</td><td>0.139</td><td>0.145</td><td>0.151</td><td>0.147</td><td>0.140</td><td>0.135</td></t<>		.853	-0.129	-0.099	-0.074	-0.086	-0.075	-0.057	-0.037	-0.010	-0.043	-0.004	0.068	0.142	0.146	0.139	0.145	0.151	0.147	0.140	0.135
a, deg .153 .226 .300 0.001 -0.104 -0.167 -0.73 -0.007 -0.130 -0.200 -0.78 0.010 -0.149 -0.225 -0.81 -2.990 -0.156 -0.226 -0.81 0.013 -0.156 -0.226 -0.81 0.013 -0.156 -0.226 -0.81 0.013 -0.168 -0.251 -0.78 9.018 -0.185 -0.267 -0.78 -0.016 -0.194 -0.279 -0.86 -0.003 -0.164 -0.279 -0.84 -0.004 -0.235 -0.247 -0.89 -0.006 -0.235 -0.360 -0.99 -0.006 -0.235 -0.360 -0.99 -0.018 -0.235 -0.360 -0.99 -0.018 -0.235 -0.360 -0.99 -0.290 -0.235 -0.360 -0.99 -0.290 -0.236 -0.355 -0.86 -0.344 -0.344 -0.62 8.988 -0.247	0.875	677.	-0.160	-0.135	-0.110	-0.125	-0.108	-0.098	-0.084	-0.056	-0.078	-0.038	0.034	0.102	0.114	0.102	0.113	0.121	0.122	0.122	0.113
a, deg .153 .226 .300 0.001 -0.104 -0.167 -0.73 -0.007 -0.130 -0.200 -0.78 0.010 -0.149 -0.225 -0.81 -2.990 -0.156 -0.226 -0.81 0.013 -0.156 -0.226 -0.81 0.013 -0.156 -0.226 -0.81 0.013 -0.168 -0.251 -0.78 9.018 -0.185 -0.267 -0.78 -0.016 -0.194 -0.279 -0.86 -0.003 -0.164 -0.279 -0.84 -0.004 -0.235 -0.247 -0.89 -0.006 -0.235 -0.360 -0.99 -0.006 -0.235 -0.360 -0.99 -0.018 -0.235 -0.360 -0.99 -0.018 -0.235 -0.360 -0.99 -0.290 -0.235 -0.360 -0.99 -0.290 -0.236 -0.355 -0.86 -0.344 -0.344 -0.62 8.988 -0.247	Tap at $y/Y = 0$.705	-0.192	-0.164	-0.139	-0.162	-0.139	-0.132	-0.130	-0.100	-0.110	-0.074	-0.001	0.055	0.078	0.060	0.077	0.085	0.090	960.0	0.084
a, deg .153 .226 .300 0.001 -0.104 -0.167 -0.73 -0.007 -0.130 -0.200 -0.78 0.010 -0.149 -0.225 -0.81 -2.990 -0.156 -0.226 -0.81 0.013 -0.156 -0.226 -0.81 0.013 -0.156 -0.226 -0.81 0.013 -0.168 -0.251 -0.78 9.018 -0.185 -0.267 -0.78 -0.016 -0.194 -0.279 -0.86 -0.003 -0.164 -0.279 -0.84 -0.004 -0.235 -0.247 -0.89 -0.006 -0.235 -0.360 -0.99 -0.006 -0.235 -0.360 -0.99 -0.018 -0.235 -0.354 -0.86 -0.247 -0.344 -0.62 8.988 -0.247 -0.344 -0.62	nozzle top f	.558	-0.269	-0.233	-0.208	-0.255	-0.206	-0.207	-0.230	-0.227	-0.185	-0.151	-0.100	-0.051	-0.018	-0.050	-0.018	9000-	0.005	0.018	0.003
a, deg .153 .226 .300 0.001 -0.104 -0.167 -0.73 -0.007 -0.130 -0.200 -0.78 0.010 -0.149 -0.225 -0.81 -2.990 -0.156 -0.226 -0.81 0.013 -0.156 -0.226 -0.81 0.013 -0.156 -0.226 -0.81 0.013 -0.168 -0.251 -0.78 9.018 -0.185 -0.267 -0.78 -0.016 -0.194 -0.279 -0.86 -0.003 -0.164 -0.279 -0.84 -0.004 -0.235 -0.247 -0.89 -0.006 -0.235 -0.360 -0.99 -0.006 -0.235 -0.360 -0.99 -0.018 -0.235 -0.354 -0.86 -0.247 -0.344 -0.62 8.988 -0.247 -0.344 -0.62	pefficients on with values	.411	-0.362	-0.322	-0.302	-0.382	-0.297	-0.294	-0.343	-0.396	-0.290	-0.279	-0.244	-0.173	-0.172	-0.227	-0.174	-0.144	-0.132	-0.119	-0.158
a, deg .153 .226 .300 0.001 -0.104 -0.167 -0.73 -0.007 -0.130 -0.200 -0.78 0.010 -0.149 -0.225 -0.81 -2.990 -0.156 -0.226 -0.81 0.013 -0.156 -0.226 -0.81 0.013 -0.156 -0.226 -0.81 0.013 -0.168 -0.251 -0.78 9.018 -0.185 -0.267 -0.78 -0.016 -0.194 -0.279 -0.86 -0.003 -0.164 -0.279 -0.84 -0.004 -0.235 -0.247 -0.89 -0.006 -0.235 -0.360 -0.99 -0.006 -0.235 -0.360 -0.99 -0.018 -0.235 -0.354 -0.86 -0.247 -0.344 -0.62 8.988 -0.247 -0.344 -0.62	ic pressure co	.337	-0.607	-0.491	-0.447	-0.543	-0.435	-0.404	-0.422	-0.514	-0.429	-0.439	-0.458	-0.409	-0.417	-0.504	-0.420	-0.351	-0.323	-0.311	-0.378
α, deg .153 0.001 -0.104 -0.007 -0.130 0.010 -0.149 -2.990 -0.156 0.013 -0.156 3.014 -0.185 9.018 -0.185 9.018 -0.184 -0.000 -0.185 -0.000 -0.185 -0.000 -0.185 -0.000 -0.208 0.004 -0.235 -2.990 -0.235	Stati	.300	-0.732	-0.786	-0.813	-0.845	-0.813	-0.782	-0.788	698.0-	-0.843	-0.896	-1.014	-0.990	-0.864	-1.055	-0.869	-0.709	-0.629	-0.637	-0.738
a, deg 0.001 -0.007 0.010 -2.990 0.013 3.014 5.999 9.018 -0.003 -0.004 -0.004 -0.006 -2.990 0.004 -2.990 0.004 8.998		.226	-0.167	-0.200	-0.225	-0.220	-0.226	-0.251	-0.267	-0.279	-0.247	-0.279	-0.316	-0.360	-0.354	-0.380	-0.355	-0.347	-0.344	-0.338	-0.325
		.153									-0.164	-0.183	-0.208	-0.235	-0.235	-0.253	-0.236	-0.241	-0.247	-0.248	-0.219
0.603 0.603 0.603 0.603 0.603 0.603		α, deg	0.001	-0.007	0.010	-2.990	0.013	3.014	5.999	9.018	-0.016	-0.003	-0.010	0.004	-0.006	-2.990	0.018	3.028	5.994	8.988	0.018
		M	0.952	0.923	0.901	0.898	0.900	0.898	868.0	0.901	0.877	0.849	0.801	0.703	0.603	0.603	0.603	0.602	0.601	0.602	0.400

Table 13. Continued

(b) Static pressure coefficients on nozzle sidewall

	.926	-0.117	-0.082	-0.053	-0.066	-0.054	-0.033	-0.012	-0.007	-0.021	610.0	880'0	0.164	0.165	0.161	0.164	0.168	0.157	0.141	0.147
	.853	-0.154	-0.115	-0.084	-0.098	-0.083	-0.071	-0.055	-0.051	-0.053	-0.011	0.063	0.135	0.139	0.131	0.136	0.144	0.139	0.133	0.123
nd sidewall	621.	-0.186	-0.145	-0.116	-0.131	-0.113	-0.109	-0.099	-0.088	-0.082	-0.041	0.031	0.094	0.109	0.098	0.108	0.116	0.118	0.120	0.106
zle top flap ar	.705	-0.225	-0.182	-0.152	-0.170	-0.148	-0.150	-0.149	-0.127	-0.115	-0.075	-0.009	0.047	0.077	0.061	0.076	0.085	0.095	0.102	0.083
between noz.	.558	-0.292	-0.248	-0.217	-0.255	-0.213	-0.221	-0.256	-0.249	-0.188	-0.154	-0.110	-0.057	110.0-	-0.036	-0.010	-0.001	010'0	0.027	0.023
Static pressure coefficients on corner between nozzle top flap and sidewal with values of x/l of—	.411	-0.357	-0.329	-0.315	-0.381	-0.309	-0.319	-0.366	-0.386	-0.303	-0.292	-0.245	-0.157	-0.147	-0.186	-0.147	-0.124	-0.118	-0.111	-0.130
sure coefficie	.337	-0.522	-0.448	-0.420	-0.493	-0.411	-0.406	866.0–	-0.416	-0.412	-0.424	-0.441	-0.382	-0.416	-0.490	-0.418	-0.352	806.0-	-0.301	-0.388
Static press	.300	-0.720	-0.770	-0.799	-0.825	-0.798	-0.781	-0.733	-0.736	-0.827	-0.879	-0.995	-1.007	-0.905	-1.070	-0.911	-0.803	-0.718	-0.630	-0.783
	.226	-0.166	-0.199	-0.225	-0.223	-0.227	-0.251	-0.269	-0.280	-0.246	-0.275	-0.314	-0.355	-0.352	-0.379	-0.353	-0.347	-0.348	-0.341	-0.323
	.153	-0.102	-0.128	-0.149	-0.159	-0.150	691.0-	-0.198	-0.217	-0.163	-0.182	-0.207	-0.231	-0.235	-0.254	-0.236	-0.243	-0.262	-0.275	-0.220
	α, deg	0.001	-0.007	0.010	-2.990	0.013	3.014	5.999	9.018	-0.016	-0.003	-0.010	0.004	-0.006	-2.990	0.018	3.028	5.994	8.988	0.018
	M	0.952	0.923	0.901	868.0	0.900	0.898	0.898	0.901	0.877	0.849	0.801	0.703	0.603	0.603	0.603	0.602	0.601	0.602	0.400

Table 13. Continued

(b) Continued

				Store	o outrosoure of	Static arrange coefficients on nozzle sidewall at $7/7 = 0.50$	unzzie sideu	J = I/I = I/I = I	05 (
				. Jia	וור אורפפחור כו	with values of x/l of—	—Jo //x Jo				
×	a. deg	.153	.226	.300	.337	.411	.558	.705	<i>6LL</i> :	.853	.926
2500	0.001	-0.004	-0.163	-0.711	-0.435	-0.334	1	-0.224	-0.184	-0.147	-0.103
0.932	0.00	0.07	961 0-	-0.745	-0.373	-0.304	i	-0.182	-0.144	-0.103	-0.056
0.923	0.00	5 130	-0.222	-0.768	-0.352	-0.288	1	-0.151	-0.112	-0.068	-0.029
0.508	2 990	-0.147	-0.227	-0.795	-0.412	-0.331		-0.175	-0.131	-0.081	-0.030
0.000	0.013	-0.141	-0.224	-0.764	-0.342	-0.284	1	-0.152	-0.108	-0.065	-0.025
0.500	3.015	-0.154	-0.236	-0.784	-0.372	-0.317		-0.152	660'0-	-0.049	-0.007
0.020	\$ 000	0.178	-0.254	-0.818	-0.415	-0.360	ı	-0.146	060.0-	-0.034	0.012
0.020	0.018	0.205	-0.279	-0.861	-0.477	-0.398		-0.188	-0.117	-0.040	0.021
0.901	0.010	0.155	-0.244	-0.791	-0.345	-0.287	1	-0.123	-0.073	-0.031	0.003
0.970	0.010	0.174	20.274	-0.848	-0.362	-0.288	1	-0.079	-0.027	0.013	0.047
0.045	0.00	0 100	-0.315	068 0-	-0.326	-0.248	1	-0.023	0.039	0.080	0.106
0.501	0.010	-0.223	-0.355	792.0-	-0.288	-0.192	-	0.027	0.098	0.147	0.176
0.703	900	0 229	998 0-	-0.811	-0.452	-0.156		0.077	0.120	0.158	0.183
0.003	2 990	-0.245	-0.388	-0.849	-0.491	-0.161		0.081	0.119	0.150	0.172
0.00	0.018	-0.232	-0.368	-0.815	-0.452	-0.159	1	0.077	0.119	0.157	0.183
0,602	3.028	-0.237	-0.366	-0.797	-0.432	-0.163	1	0.075	0.119	0.156	0.181
1090	5 004	_0.253	-0.377	-0.819	-0.444	-0.167	1	0.083	0.121	0.148	0.162
0,607	8 988		-0.391	-0.822	-0.471	-0.162	t	0.087	0.114	0.126	0.129
0.000	0.018		-0.350	-0.759	-0.514	-0.127		860.0	0.118	0.137	0.156

Table 13. Continued

(b) Continued

					Sta	tic pressure	coefficients o	Static pressure coefficients on nozzle sidewall at centerline	wall at center	line			
							with value	with values of x/l of-					
	α, deg	.153	.226	.300	.337	.411	.484	.558	.632	.705	671.	.853	.926
0.952	0.001	-0.097	-0.166	-0.695	0.337	-0.292	-0.301	-0.294	-0.268	-0.230	-0.191	-0.146	-
0.923	-0.007	-0.124	-0.201	699.0-	-0.279	-0.258	-0.270	-0.260	-0.234	-0.195	-0.148	-0.097	***
0.901	0.010	-0.142	-0.227	-0.657	-0.261	-0.251	-0.253	-0.240	-0.205	-0.160	-0.113	-0.066	1
0.898	-2.990	-0.148	-0.229	-0.721	-0.308	-0.292	-0.291	-0.280	-0.242	-0.189	-0.129	-0.066	
0.600	0.013	-0.144	-0.228	-0.650	-0.251	-0.245	-0.248	-0.238	-0.204	-0.161	-0.114	-0.063	-
868.0	3.014	-0.147	-0.227	-0.694	-0.294	-0.284	-0.278	-0.256	-0.209	-0.156	-0.102	-0.047	
0.898	5.999	-0.160	-0.239	-0.811	-0.424	-0.357	-0.318	-0.286	-0.230	-0.164	-0.096	-0.033	
0.901	9.018	0.180	-0.257	-0.859	-0.484	-0.378	-0.356	-0.350	-0.311	-0.244	-0.148	-0.048	ı
0.877	-0.016	-0.160	-0.252	-0.660	-0.258	-0.249	-0.251	-0.225	-0.184	-0.130	-0.079	-0.029	1
0.849	-0.003	-0.178	-0.284	-0.683	-0.266	-0.256	-0.249	0.213	-0.155	-0.090	-0.031	0.018	ı
0.801	-0.010	-0.205	-0.323	-0.635	-0.224	-0.225	-0.227	-0.189	-0.121	-0.037	0.034	980.0	-
0.703	0.004	-0.232	-0.365	-0.642	-0.213	-0.187	-0.172	-0.125	-0.055	0.023	0.098	0.153	***
0.603	900.0-	-0.245	-0.388	-0.768	-0.336	-0.171	-0.113	-0.051	0.010	0.067	0.118	0.159	1
0.603	-2.990	-0.251	-0.397	-0.821	-0.369	-0.166	-0.107	-0.044	0.017	0.074	0.121	0.156	-
0.603	0.018	-0.247	-0.389	-0.776	-0.341	-0.172	-0.112	-0.049	0.012	990:0	0.119	0.160	ı
0.602	3.028	-0.253	-0.396	-0.804	-0.345	-0.175	-0.121	-0.059	0.009	0.068	0.122	0.160	1
0.601	5.994	-0.266	-0.409	-0.824	-0.372	-0.184	-0.123	-0.054	0.018	0.078	0.122	0.142	-
0.602	8.988	-0.285	-0.424	-0.838	-0.411	-0.204	-0.141	-0.069	9000	0.051	0.067	0.067	1
0.400	0.018	-0.239	-0.384	-0.793	-0.534	-0.124	-0.014	0.041	0.073	960'0	0.114	0.133	1

Table 13. Continued

(b) Concluded

	_	_	_	_	_	_	_	_	_	_	_	$\overline{}$	_			_	_			
	.926	-0.107	-0.059	-0.025	-0.021	-0.027	-0.005	0.016	0.021	0.008	0.052	0.112	0.171	0.178	0.172	0.175	0.160	0.130	0.115	0.154
0.50	705	-0.234	-0.202	-0.171	-0.196	-0.171	-0.164	-0.188	-0.262	-0.137	-0.095	-0.039	0.029	0.077	0.078	0.078	0.077	0.054	-0.013	0.097
Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$.558	-0.284	-0.257	-0.242	-0.269	-0.241	-0.258	-0.319	-0.362	-0.235	-0.219	-0.195	-0.117	-0.035	-0.035	-0.032	-0.039	-0.041	-0.078	0.035
nozzle sidew	.411	1	ı	1	-	-	-	I	-	1	1	ı	-	1	I	ı	l	ı	ı	1
efficients on nozzle sid	.337	-0.379	-0.290	-0.261	-0.291	-0.250	-0.292	-0.330	-0.310	-0.248	-0.251	-0.241	-0.292	-0.455	-0.438	-0.468	-0.484	-0.497	-0.458	-0.510
c pressure co	300	80Z O	-0.699	-0.680	-0.717	-0.674	-0.701	869.0-	-0.580	-0.681	-0.703	-0.761	-0.779	-0.825	-0.818	-0.833	-0.867	-0.902	-0.897	-0.765
Stati	226	0.160	-0 194	-0.217	-0.230	-0.219	-0.218	-0.235	-0.266	-0.240	-0.268	-0.309	-0.349	-0.365	-0.364	-0.369	-0.389	-0.418	-0.451	-0.352
	153	080 0	-0.116	-0.135	-0.149	-0.136	-0.140	-0.163	-0.202	-0.153	-0.172	-0.195	-0.217	-0.227	-0.229	-0.227	-0.243	-0.270	-0.309	7170
	o dea	1000	0.007	0100	-2.990	0.013	3.014	\$ 999	9.018	0.016	-0.003	0100	0000	9000	-2.990	8100	3.028	5 994	8.988	0.018
	N	87.7	0.073	0 001	868.0	0060	808 0	808 0	1090	0.877	0.849	1080	0.703	0.603	0 603	0.603	0 602	1090	0 602	280

Table 13. Continued (c) Static pressure coefficients on nozzle bottom flap

				Static	Static pressure coefficients on nozzle bottom flap at $v/Y = 0.875$	fficients on n	ozzle bottom	flap at $v/Y =$	- 0.875		
		-				with values	with values of x/l of-				
M	α, deg	.153	.226	.300	.337	.411	.558	501.	622.	.853	.926
0.952	0.001	-0.096	-0.156	-0.742	-0.522	-0.353	-0.300	-0.246	-0.195	-0.138	-0.083
0.923	-0.007	-0.122	-0.190	-0.717	-0.381	-0.306	-0.294	-0.207	-0.142	-0.087	-0.040
0.901	0.010	-0.142	-0.215	-0.684	-0.341	-0.288	-0.272	-0.171	-0.109	-0.061	-0.019
0.898	-2.990	-0.164	-0.245	-0.651	-0.329	-0.287	-0.286	-0.175	-0.101	-0.042	0.004
0.900	0.013	-0.144	-0.217	-0.680	-0.334	-0.286	-0.272	-0.167	-0.106	-0.059	-0.018
0.898	3.014	-0.152	-0.210	-0.734	-0.380	-0.323	-0.297	6/11/0-	-0.108	-0.050	0.000
0.898	5.999	-0.194	-0.238	-0.745	-0.410	-0.367	-0.355	-0.198	-0.109	-0.042	0.016
0.901	9.018	-0.268	-0.290	-0.696	-0.382	-0.362	-0.420	-0.267	-0.145	-0.051	0.027
0.877	-0.016	-0.155	-0.233	-0.698	-0.342	-0.293	-0.239	-0.119	-0.068	-0.027	0.010
0.849	-0.003	-0.177	-0.262	-0.755	-0.372	-0.302	-0.199	-0.075	-0.024	0.016	0.050
0.801	-0.010	-0.200	-0.301	-0.924	-0.432	-0.264	-0.127	-0.004	0.044	0.080	0.108
0.703	0.004	-0.226	-0.346	-1.007	-0.408	-0.174	-0.050	0.052	0.099	0.137	0.168
0.603	-0.006	-0.228	-0.343	-0.885	-0.426	-0.178	-0.021	0.070	0.108	0.139	0.168
0.603	-2.990	-0.234	-0.334	-0.696	-0.350	-0.145	-0.004	0.084	0.120	0.147	0.171
0.603	0.018	-0.230	-0.345	-0.887	-0.427	-0.178	-0.022	0.071	0.109	0.139	0.167
0.602	3.028	-0.250	-0.370	-1.054	-0.510	-0.238	-0.065	0.043	0.091	0.127	0.163
0.601	5.994	-0.294	-0.409	-1.170	-0.595	-0.315	-0.122	0.013	0.076	0.120	0.159
0.602	8.988	-0.362	-0.462	-1.265	9/9/0-	-0.393	-0.181	-0.027	0.050	0.103	0.153
0.400	0.018	-0.213	-0.314	-0.755	-0.388	-0.165	-0.002	0.079	0.108	0.133	0.154

Table 13. Continued

(c) Continued

0.036 0.164 0.165 0.166 0.164 0.116 0.024 0.00 0.047 0.153 -0.048 -0.012 0.010 900.0 0.107 -0.0120.151 926 -0.046 -0.048-0.026 -0.0250.016 0.134 0.138 0.144 0.137 0.118 0.100 0.080 0.128 -0.086-0.060 -0.018 -0.034-0.024.853 -0.079 0.078 0.056 0.18 -0.083 -0.083 -0.084 -0.080 -0.059-0.0200.047 0.115 0.104 0.034 -0.1270.19 977. Static pressure coefficients on nozzle bottom flap at y/Y = 0.50-0.015-0.168 0.006 0.066 0.065 0.035 -0.094-0.122-0.138-0.172-0.127 -0.097 0.067 -0.121 -0.061.705 0.140 with values of x/l of--0.212 -0.236 -0.036-0.237 -0.213 -0.208 -0.270-0.166-0.013-0.038 -0.079-0.139-0.316-0.190 -0.112-0.030-0.272-0.1050.04 .558 -0.327 -0.297 -0.443 -0.364-0.560-0.346 -0.344-0.212-0.260-0.195-0.618 -0.499 -0.422-0.3690.178 -0.410-0.21114. -0.725 -0.715 -0.850-0.959-0.982-0.608 -0.576-0.459-0.460-0.606 -0.874-0.525-0.890 -0.613-0.486-0.415-0.573-0.407300 ı 1 1 1 -0.366 -0.438 -0.182 -0.237 -0.317-0.395 -0.425-0.156 -0.190-0.215 -0.228 -0.164 -0.401-0.217-0.351-0.199.226 .153 1 a, deg 0.010 -2.9900.013 3.014 5.999 9.018 -0.010 0.04 900.0 -2.990 0.018 3.028 5.994 8.988 0.018 -0.007 -0.016 -0.003 0.00 0.849 0.602 0.898 868.0 0.602 0.703 0.603 0.603 M_{∞} 0.952 0.923 0.901 0.898 0.901 0.877 0.801 0.603 0.601

Table 13. Continued

(c) Concluded

	.705 .926	-0.042	-0.016	-0.001	0.017	-0.005	0.013	33	4	9	2	9	4	3	5	03	9	Li	∞	7
	35			┗	L	9	0.0	0.033	0.044	0.016	0.052	0.106	0.164	0.163	0.165	091'0	0.146	0.127	0.108	0.152
erlin	7.	-0.145	-0.115	-0.104	-0.076	-0.106	-0.102	-0.111	-0.128	-0.091	-0.057	0.007	0.055	0.056	0.073	0.056	0.025	0000	-0.021	0.052
Static pressure coefficients on nozzle bottom flap at centerline with values of xl of—	.558	-0.254	-0.205	-0.191	-0.192	-0.193	-0.201	-0.238	-0.274	-0.187	-0.164	-0.106	-0.049	-0.049	-0.023	-0.049	-0.086	-0.115	-0.137	-0.045
ficients on nozzle botton with values of x/l of—	.411	-0.785	-0.510	-0.391	-0.472	-0.387	-0.460	-0.686	-0.879	-0.366	-0.362	-0.345	-0.242	-0.234	-0.202	-0.234	-0.277	-0.308	-0.329	-0.214
efficients on with value	.337	-0.875	-0.948	-0.895	-1.025	-0.860	-0.984	-1.011	-1.000	-0.641	-0.602	-0.658	-0.511	-0.470	-0.430	-0.472	-0.521	-0.557	-0.582	-0.410
c pressure co	.300	-0.805	-0.874	-0.924	-0.935	-0.926	-0.926	-0.921	-0.907	996:0-	-1.030	-1.165	-1.220	-0.932	-0.867	-0.935	-1.002	-1.064	-1.114	-0.768
Stati	.226	-0.176	-0.203	-0.226	-0.235	-0.229	-0.220	-0.208	-0.192	-0.248	-0.282	-0.336	-0.422	-0.409	-0.383	-0.411	-0.440	-0.456	-0.461	-0.362
	.153	-0.104	-0.130	-0.147	-0.156	-0.149	-0.139	-0.127	-0.110	-0.164	-0.192	-0.225	-0.273	-0.274	-0.255	-0.274	-0.291	-0.298	-0.294	-0.246
	α, deg	0.001	-0.007	0.010	-2.990	0.013	3.014	5.999	9.018	-0.016	-0.003	-0.010	0.004	-0.006	-2.990	0.018	3.028	5.994	8.988	0.018
	M∞	0.952	0.923	0.901	0.898	0.900	0.898	0.898	0.901	0.877	0.849	0.801	0.703	0.603	0.603	0.603	0.602	0.601	0.602	0.400

Table 13. Concluded

(d) Force data

M	α, deg	c_D
0.952	0.001	0.2739
0.923	-0.007	0.2360
106.0	0.010	0.2123
868.0	-2.990	0.2328
0.900	0.013	0.2105
868.0	3.014	0.2216
868.0	5.999	0.2446
106'0	9.018	0.2797
228.0	-0.016	0.1938
0.849	-0.003	0.1722
0.801	-0.010	0.1435
0.703	0.004	0.0923
0.603	-0.006	0.0745
0.603	-2.990	0.0730
0.603	0.018	0.0741
0.602	3.028	0.0771
0.601	5.994	0.0827
0.602	8.988	0.0919
0.400	0.018	0.0531

Table 14. Pressure and Force Data for Nozzle 9 With $\beta_{t,lop/bot} = 17.9^{\circ}/\beta_{t,side} = 0^{\circ}$, Plume On, and $\alpha = 0^{\circ}$

(a) Static pressure coefficients on nozzle top flap

				Si	itic pressure	coefficients c	on nozzle top	Static pressure coefficients on nozzle top flap at centerline	line			
						with value	with values of x/l of-					
M∞	.153	.226	.300	.337	.411	.484	.558	.632	705	677.	.853	.926
0.600	1	-0.482	-1.061	-0.527	-0.223	-0.092	-0.008	0.057	0.108	0.154	0.191	0.219
0.697	1	-0.476	-1.414	-0.557	-0.211	080.0-	0.003	0.064	0.112	0.151	0.183	0.205
0.799	1	-0.355	-0.795	-0.350	-0.240	-0.174	-0.125	-0.080	-0.047	-0.012	0.020	0.050
1.251	1	-0.016	-0.385	-0.522	-0.493	-0.408	-0.167	-0.149	-0.136	-0.123	-0.106	-0.085
1.198	-	-0.032	-0.431	-0.575	-0.537	-0.352	-0.182	-0.164	-0.151	-0.136	-0.121	-0.097
1.149	١	-0.060	-0.488	-0.648	-0.605	-0.322	-0.211	-0.190	-0.174	-0.161	-0.142	-0.122
0.954	ł	-0.183	-0.730	-0.432	-0.303	-0.256	-0.234	-0.212	-0.198	-0.181	-0.160	-0.135
0.927	I	-0.219	-0.672	-0.346	-0.263	-0.232	-0.211	-0.192	-0.174	-0.155	-0.133	-0.107
0.897	1	-0.255	-0.640	-0.311	-0.249	-0.225	-0.203	-0.181	-0.158	-0.131	-0.108	-0.076
0.877	I	-0.279	-0.654	-0.313	-0.255	-0.222	-0.195	-0.168	-0.142	-0.113	-0.087	-0.051
0.848	I	-0.309	-0.678	-0.323	-0.252	-0.211	-0.177	-0.143	-0.113	-0.082	-0.051	-0.015
0.802	1	-0.363	-0.788	-0.357	-0.253	-0.186	-0.136	-0.093	-0.062	-0.031	0.003	0.033
0.700	1	-0.473	-1.376	-0.563	-0.217	-0.082	0.002	0.063	0.109	0.147	0.176	0.199
0.601	ı	-0.481	-1.054	-0.526	-0.222	-0.092	-0.008	0.057	0.107	0.153	0.187	0.215
0.401	١	-0.435	-0.868	-0.474	-0.214	-0.093	-0.012	0.052	0.098	0.145	0.182	0.211

	_		т-	_	_	_	T .	_	_				_	_		_
	.926	0.221	0.207	0.048	-0.086	-0.100	-0.125	-0.136	-0.109	-0.080	-0.055	-0.014	0.033	0.200	0.216	0.213
	.853	0.191	0.181	0.020	-0.105	-0.122	-0.145	-0.160	-0.135	-0.111	-0.087	-0.051	0.003	0.177	0.186	0.183
0.25	621.	0.153	0.149	-0.011	-0.121	-0.134	-0.161	-0.180	-0.155	-0.135	-0.116	-0.081	-0.025	0.145	0.150	0.145
flap at $y/Y = 0$.705	0.105	0.108	-0.044	-0.135	-0.152	-0.174	-0.199	-0.175	-0.163	-0.144	-0.115	-0.058	0.104	0.103	0.097
fficients on nozzle top with values of x/l of—	.558	-0.011	-0.004	-0.123	-0.176	-0.187	-0.214	-0.232	-0.211	-0.205	-0.195	9/1.0-	-0.134	-0.005	-0.011	-0.012
oefficients or with values	.411	-0.221	-0.213	-0.245	-0.490	-0.537	-0.602	-0.309	-0.265	-0.255	-0.256	-0.255	-0.254	-0.213	-0.221	-0.208
Static pressure coefficients on nozzle top flap at $y/Y = 0.25$ with values of x/l of—	.337	-0.522	-0.550	-0.370	-0.522	-0.578	-0.643	-0.446	-0.354	-0.319	-0.321	-0.336	-0.387	-0.559	-0.521	-0.470
Sta	300	-1.041	-1.394	-0.838	-0.377	-0.424	-0.481	-0.733	-0.682	-0.658	-0.672	-0.705	-0.842	-1.359	-1.037	-0.856
	.226	-0.462	-0.458	-0.344	-0.012	-0.025	-0.055	-0.176	-0.209	-0.246	-0.269	-0.298	-0.350	-0.458	-0.461	-0.414
	.153	-0.290	-0.286	-0.221	0.002	-0.004	-0.029	-0.105	-0.132	-0.159	-0.176	-0.192	-0.227	-0.284	-0.292	-0.271
	M∞	0.600	0.697	0.799	1.251	1.198	1.149	0.954	0.927	0.897	0.877	0.848	0.802	0.700	0.601	0.401

Table 14. Continued

(a) Concluded

			d			The state of	A/ *	0.50		
			Stal	ne pressure c	with values	with values of x/l of—	Static pressure cocilicients on nozzie top fiap at yrr = 0.50 with values of x/l of—	00.0		
M	.153	.226	.300	.337	.411	.558	.705	<i>6LL</i> :	.853	.926
0090	-0.263	-0.412	-0.976	-0.494	-0.217	-0.030	0.085	0.132	0.180	0.216
0.697	-0.262	-0.420	-1.290	-0.518	-0.218	-0.023	0.090	0.134	0.173	0.206
0.799	-0.209	-0.325	-0.963	-0.436	-0.239	-0.105	-0.030	-0.003	0.031	0.070
1 251	-0.003	-0.012	-0.383	-0.527	-0.442	-0.268	-0.125	-0.114	-0.099	-0.071
861	-0.005	-0.023	-0.431	-0.578	-0.480	-0.237	-0.142	-0.128	-0.114	-0.087
1 149	-0.032	-0.054	-0.489	-0.644	-0.540	-0.236	-0.166	-0.151	-0.137	-0.108
0.954	10.104	-0.168	-0.760	-0.487	-0.322	-0.233	-0.197	-0.180	-0.158	-0.131
7,000	-0.129	-0.202	-0.726	-0.384	-0.274	-0.211	-0.175	-0.154	-0.132	-0.103
0.897	-0.156	-0.239	-0.717	-0.357	-0.267	-0.201	-0.158	-0.131	-0.103	-0.069
0.877	-0.171	-0.257	-0.735	-0.359	-0.266	-0.191	-0.137	-0.109	-0.078	-0.040
0.848	-0.188	-0.284	-0.781	-0.377	-0.266	-0.165	-0.103	-0.073	-0.035	0.004
0 802	-0.220	-0.334	-0.947	-0.450	-0.255	-0.119	-0.046	-0.016	0.016	0.054
0.700	-0.261	-0.421	-1.270	-0.519	-0.218	-0.022	0.087	0.130	0.166	0.198
0.601	-0.262	-0.416	-0.972	-0.495	-0.219	-0.030	0.082	0.131	0.176	0.210
0.401	-0.243	-0.377	-0.803	-0.442	-0.200	-0.023	0.074	0.121	0.170	0.207

	926	07.0	0.140	0.128	0.048	-0.070	-0.077	-0.087	-0.118	-0.087	-0.056	-0.036	-0.005	0.032	0.120	0.134	0.134
	853	CCO.	0.079	0.070	900.0	-0.151	-0.147	-0.163	-0.143	-0.114	-0.084	-0.062	-0.031	-0.007	0.063	0.074	0.076
.75	770	611.	1	1	1	ı	1	-	ŀ	ļ	-	-	_		i	1	_
$\int \int dx dx = 0$	705	co/.	-0.010	-0.005	-0.056	-0.270	-0.264	-0.279	-0.187	-0.164	-0.141	-0.122	-0.095	-0.067	-0.010	-0.010	-0.007
nozzle top f	-10 1/1 10	occ.	1	1	1	1	1	-	ŀ	1		1	1		ı	-	1
pefficients on nozzle top	WIIII VAIUCS	114.	-0.300	-0.314	-0.261	-0.354	-0.391	-0.446	-0.307	-0.255	-0.244	-0.239	-0.239	-0.270	-0.313	-0.300	-0.270
Static pressure coefficients on nozzle top flap at $y/Y = 0.75$	200	.337	-0.462	605.0-	-0.459	-0.357	-0.395	-0.451	-0.658	-0.567	-0.499	-0.481	-0.473	-0.471	-0.506	-0.461	-0.403
Stat	986	.300	-0.763	-0.899	-0.923	-0.277	-0.315	-0.369	-0.616	-0.668	-0.728	-0.770	-0.822	-0.918	-0.890	-0.758	-0.642
	280	977.	-0.307	-0.323	-0.281	-0.008	-0.018	-0.052	-0.154	-0.188	-0.222	-0.236	-0.257	-0.291	-0.322	-0.307	-0.277
		.153	-0.204	-0.211	-0.184	-0.002	-0.005	-0.033	-0.095	121	-0.145	-0.158	-0.171	-0.193	-0.213	-0.205	-0.189
		Moo	0.600	769.0	0.799	1.251	198	1.149	0.954	7,000	0.897	0.877	0.848	0.802	002.0	0,00	0.401

Table 14. Continued

(b) Static pressure coefficients on nozzle sidewall

Static pressure coefficients on corner between nozzle top flap and sidewall	with values of	00 .337 .411 .558 .705 .779 .853 .926	358 -0.382 -0.275 -0.206 -0.170 -0.114 -0.059 0.040	-0.426 -0.297 -0.211 -0.160 -0.098 -0.040	-0.467 -0.287 -0.204 -0.164 -0.110 -0.070	-0.190 -0.217 -0.296 -0.422 -0.464 -0.478	-0.220 -0.247 -0.330 -0.469 -0.510 -0.449	-0.268 -0.296 -0.360 -0.507 -0.551 -0.469	-0.468 -0.446 -0.286 -0.166 -0.131 -0.136	-0.513 -0.382 -0.198 -0.15¢ 0.142 0.142	-0.540 -0.310 0.187 0.173 0.143	1717 7147 7010 0 000 0 123 0 121	0.2.0 -0.200 -0.1/3	424 -0.524 -0.275 -0.202 -0.166 -0.119 -0.088 -0.043	-0.472	-0.421 -0.293 -0.211 -0.158 -0.097 -0.041	-0.376 -0.272 -0.204 -0.170 -0.114 -0.063	-0.326 -0.240 -0.186 -0.167 -0.123 -0.070
nozzle top		2.	9	9	9	4.0-	9.0	0.5	٩	9			7	-0.1	-0.1	9	9	9
r between	S OF X/I OF	.558	-0.206	-0.211	-0.204	-0.296	-0.330	-0.360	-0.286	901	781	100	37.7	-0.202	-0.211	-0.211	-0.204	0.186
ents on come	with value	.411	-0.275	-0.297	-0.287	-0.217	-0.247	-0.296	-0.446	-0.382	-0.310	2000	0.200	-0.275	-0.295	-0.293	-0.272	-0.240
sure coefficie		.337	-0.382	-0.426	-0.467	-0.190	-0.220	-0.268	-0.468	-0.513	-0.549	0.557	1000	-0.524	-0.472	-0.421	-0.376	-0.326
Static pres		.300	-0.358	-0.399	-0.433	-0.089	-0.110	-0.156	-0.313	-0.351	-0.390	1179		-0.424	-0.436	-0.395	-0.352	-0.307
	ì	977.	ı	1	1	1	-	1	1	1					ſ	ı	ı	ı
		.133	-0.170	-0.177	-0.167	0.000	-0.004	-0.037	-0.093	-0.118	-0.141	1510	1510	101.0	-0.177	-0.177	-0.167	-0.152
	,	Moo	0.600	0.697	0.799	1.251	1.198	1.149	0.954	0.927	0.897	0.877	0 0 0	0.040	0.802	0.700	0.601	0.401

with values of xI of $-$ with values of xI of $-$ 153 .226 .300 .337 .411 .558 .705 .779 .853 .926 -0.147 -0.178 -0.212 -0.211 -0.197 -0.153 -0.095 -0.060 -0.008 - -0.157 -0.196 -0.237 -0.216 -0.159 -0.095 -0.009 -0.009 -0.009 -0.009 -0.026 -0.226 -0.226 -0.026 -0				Sta	tic pressure c	oefficients o	n nozzle side	wall at 7/7 =	0.50		
.226 .300 .337 .411 .558 .705 .779 .853 -0.178 -0.212 -0.211 -0.197 -0.153 -0.095 -0.060 -0.008 -0.196 -0.237 -0.216 -0.159 -0.092 -0.050 -0.008 -0.201 -0.265 -0.269 -0.232 -0.108 -0.072 -0.026 -0.002 -0.031 -0.053 -0.116 -0.286 -0.325 -0.354 -0.026 -0.011 -0.049 -0.074 -0.142 -0.286 -0.354 -0.400 -0.049 -0.093 -0.117 -0.189 -0.286 -0.354 -0.139 -0.129 -0.214 -0.261 -0.265 -0.347 -0.184 -0.129 -0.103 -0.160 -0.279 -0.284 -0.284 -0.285 -0.347 -0.146 -0.122 -0.108 -0.199 -0.279 -0.280 -0.286 -0.225 -0.134 -0.120 -0.033 -					•	with value	-s of x/l of-				
-0.178 -0.212 -0.211 -0.197 -0.153 -0.095 -0.060 -0.008 -0.196 -0.237 -0.235 -0.216 -0.159 -0.092 -0.050 0.004 -0.201 -0.265 -0.269 -0.232 -0.108 -0.072 -0.026 -0.002 -0.031 -0.053 -0.116 -0.286 -0.325 -0.354 -0.036 -0.049 -0.074 -0.189 -0.28 -0.354 -0.364 -0.400 -0.049 -0.093 -0.117 -0.189 -0.28 -0.354 -0.139 -0.103 -0.129 -0.214 -0.261 -0.365 -0.347 -0.184 -0.129 -0.103 -0.160 -0.246 -0.289 -0.340 -0.177 -0.146 -0.122 -0.108 -0.185 -0.291 -0.329 -0.280 -0.186 -0.141 -0.122 -0.093 -0.199 -0.294 -0.241 -0.120 -0.092 -0.034 -0.215		.153	.226	.300	.337	.411	.558	.705	977.	.853	926
-0.196 -0.237 -0.235 -0.216 -0.159 -0.092 -0.050 -0.201 -0.265 -0.269 -0.232 -0.170 -0.092 -0.050 -0.002 -0.031 -0.053 -0.116 -0.205 -0.286 -0.322 -0.011 -0.048 -0.074 -0.142 -0.236 -0.325 -0.364 -0.049 -0.093 -0.117 -0.189 -0.236 -0.354 -0.354 -0.129 -0.214 -0.261 -0.365 -0.347 -0.184 -0.129 -0.160 -0.246 -0.298 -0.349 -0.134 -0.129 -0.185 -0.279 -0.329 -0.340 -0.146 -0.120 -0.199 -0.291 -0.280 -0.186 -0.141 -0.110 -0.205 -0.234 -0.284 -0.289 -0.247 -0.186 -0.092 -0.213 -0.279 -0.279 -0.243 -0.179 -0.120 -0.092 -0.135 -0.136	_	-0.147	-0.178	-0.212	-0.211	-0.197	-0.153	-0.095	90,00	800 9	
-0.201 -0.265 -0.232 -0.170 -0.108 -0.072 -0.002 -0.031 -0.053 -0.116 -0.205 -0.286 -0.032 -0.011 -0.048 -0.074 -0.142 -0.236 -0.325 -0.325 -0.049 -0.093 -0.117 -0.189 -0.258 -0.354 -0.394 -0.129 -0.214 -0.261 -0.365 -0.347 -0.184 -0.129 -0.160 -0.246 -0.288 -0.344 -0.255 -0.134 -0.129 -0.185 -0.279 -0.329 -0.340 -0.177 -0.146 -0.122 -0.199 -0.291 -0.280 -0.280 -0.146 -0.120 -0.120 -0.199 -0.294 -0.247 -0.186 -0.128 -0.092 -0.092 -0.205 -0.213 -0.279 -0.247 -0.180 -0.120 -0.092 -0.155 -0.155 -0.158 -0.095 -0.095 -0.060 -0.060		-0.157	-0.196	-0.237	-0.235	-0.216	-0.159	-0.092	0.050	0.00	
-0.002 -0.031 -0.053 -0.116 -0.205 -0.286 -0.322 -0.049 -0.048 -0.074 -0.142 -0.236 -0.325 -0.354 -0.049 -0.093 -0.117 -0.189 -0.258 -0.354 -0.394 -0.129 -0.214 -0.261 -0.365 -0.347 -0.184 -0.129 -0.160 -0.246 -0.286 -0.349 -0.134 -0.129 -0.129 -0.185 -0.279 -0.340 -0.177 -0.146 -0.122 -0.199 -0.291 -0.280 -0.280 -0.146 -0.122 -0.199 -0.294 -0.247 -0.186 -0.141 -0.110 -0.205 -0.234 -0.247 -0.186 -0.092 -0.092 -0.213 -0.279 -0.247 -0.189 -0.020 -0.082 -0.155 -0.156 -0.158 -0.095 -0.082 -0.176 -0.176 -0.158 -0.095 -0.060		-0.156	-0.201	-0.265	-0.269	-0.232	-0.170	-0.108	-0.072	70.02	
-0.011 -0.048 -0.074 -0.142 -0.236 -0.325 -0.364 -0.049 -0.093 -0.117 -0.189 -0.258 -0.354 -0.364 -0.129 -0.214 -0.261 -0.365 -0.347 -0.184 -0.129 -0.160 -0.246 -0.288 -0.384 -0.225 -0.134 -0.129 -0.185 -0.279 -0.340 -0.177 -0.146 -0.122 -0.199 -0.291 -0.280 -0.280 -0.186 -0.141 -0.110 -0.205 -0.284 -0.289 -0.247 -0.186 -0.141 -0.110 -0.213 -0.279 -0.247 -0.180 -0.128 -0.092 -0.155 -0.279 -0.247 -0.189 -0.092 -0.092 -0.155 -0.238 -0.238 -0.238 -0.036 -0.095 -0.082 -0.176 -0.176 -0.154 -0.154 -0.095 -0.060 -0.060 -0.153 -0.175		0.002	-0.002	-0.031	-0.053	-0.116	-0.205	-0.286	-0322	0.256	
-0.049 -0.093 -0.117 -0.189 -0.258 -0.354 -0.394 -0.129 -0.214 -0.261 -0.365 -0.347 -0.184 -0.394 -0.160 -0.246 -0.298 -0.384 -0.225 -0.134 -0.129 -0.185 -0.279 -0.329 -0.340 -0.177 -0.146 -0.122 -0.199 -0.291 -0.380 -0.280 -0.186 -0.141 -0.110 -0.205 -0.284 -0.299 -0.247 -0.180 -0.128 -0.092 -0.213 -0.279 -0.247 -0.243 -0.179 -0.120 -0.092 -0.195 -0.279 -0.277 -0.243 -0.179 -0.120 -0.092 -0.195 -0.238 -0.238 -0.236 -0.158 -0.095 -0.052 -0.176 -0.177 -0.194 -0.151 -0.095 -0.060 -0.060 -0.153 -0.177 -0.178 -0.134 -0.055 -0.065		-0.006	-0.011	-0.048	-0.074	-0.142	-0.236	-0.325	10.364	0400	
-0.129 -0.214 -0.261 -0.365 -0.347 -0.184 -0.129 -0.160 -0.246 -0.298 -0.384 -0.225 -0.134 -0.129 -0.185 -0.279 -0.329 -0.340 -0.177 -0.146 -0.122 -0.199 -0.291 -0.380 -0.186 -0.141 -0.110 -0.205 -0.294 -0.247 -0.180 -0.128 -0.092 -0.213 -0.277 -0.243 -0.179 -0.120 -0.082 -0.195 -0.238 -0.235 -0.216 -0.158 -0.095 -0.052 -0.176 -0.211 -0.207 -0.194 -0.151 -0.095 -0.060 -0.176 -0.177 -0.178 -0.134 -0.055 -0.065		-0.039	-0.049	-0.093	-0.117	-0.189	-0.258	-0.354	-0.394	-0.431	
-0.160 -0.246 -0.298 -0.384 -0.225 -0.134 -0.122 -0.185 -0.279 -0.329 -0.340 -0.177 -0.146 -0.122 -0.199 -0.291 -0.380 -0.286 -0.141 -0.110 -0.205 -0.284 -0.287 -0.247 -0.186 -0.128 -0.092 -0.213 -0.279 -0.247 -0.180 -0.128 -0.092 -0.195 -0.238 -0.243 -0.179 -0.120 -0.082 -0.176 -0.211 -0.207 -0.18 -0.095 -0.052 -0.176 -0.217 -0.194 -0.151 -0.095 -0.060 -0.177 -0.177 -0.158 -0.134 -0.065 -0.065		-0.092	-0.129	-0.214	-0.261	-0.365	-0.347	-0.184	-0.129	-0 103	
-0.185 -0.279 -0.329 -0.340 -0.177 -0.146 -0.122 -0.199 -0.291 -0.280 -0.280 -0.186 -0.141 -0.110 -0.205 -0.284 -0.289 -0.247 -0.180 -0.128 -0.092 -0.213 -0.279 -0.243 -0.179 -0.120 -0.082 -0.195 -0.238 -0.243 -0.179 -0.052 -0.082 -0.176 -0.211 -0.207 -0.194 -0.158 -0.095 -0.052 -0.176 -0.217 -0.175 -0.168 -0.134 -0.095 -0.060	_	-0.117	-0.160	-0.246	-0.298	-0.384	-0.225	-0.134	-0.122	801.0	
-0.199 -0.291 -0.330 -0.280 -0.186 -0.141 -0.110 -0.205 -0.284 -0.299 -0.247 -0.180 -0.128 -0.092 -0.213 -0.279 -0.243 -0.179 -0.120 -0.082 -0.195 -0.238 -0.235 -0.216 -0.158 -0.095 -0.052 -0.176 -0.207 -0.194 -0.151 -0.098 -0.060 -0.153 -0.177 -0.175 -0.168 -0.134 -0.065		-0.141	-0.185	-0.279	-0.329	-0.340	-0.177	-0.146	-0.122	0.003	
-0.205 -0.284 -0.299 -0.247 -0.180 -0.128 -0.092 -0.213 -0.279 -0.277 -0.243 -0.179 -0.120 -0.082 -0.195 -0.238 -0.235 -0.216 -0.158 -0.095 -0.052 -0.176 -0.207 -0.194 -0.151 -0.098 -0.060 -0.153 -0.177 -0.175 -0.168 -0.134 -0.065		-0.149	-0.199	-0.291	-0.330	-0.280	-0.186	-0.141	0.110	9200	
-0.213 -0.279 -0.277 -0.243 -0.179 -0.120 -0.082 - -0.195 -0.238 -0.235 -0.216 -0.158 -0.095 -0.052 -0.176 -0.207 -0.194 -0.151 -0.098 -0.060 -0.153 -0.177 -0.175 -0.168 -0.134 -0.095 -0.065	_	-0.155	-0.205	-0.284	-0.299	-0.247	-0.180	-0.128	-0.002	-0.054	
-0.195 -0.238 -0.235 -0.216 -0.158 -0.095 -0.052 -0.176 -0.207 -0.194 -0.151 -0.098 -0.060 -0.153 -0.177 -0.175 -0.168 -0.134 -0.065		-0.167	-0.213	-0.279	-0.277	-0.243	-0.179	-0.120	-0.082	0.038	
-0.176 -0.211 -0.207 -0.194 -0.151 -0.098 -0.060 -		-0.158	-0.195	-0.238	-0.235	-0.216	-0.158	2000	-0.052	200.0	
-0.153 -0.177 -0.175 -0.168 -0.134 -0.095		-0.147	-0.176	-0.211	-0.207	-0.194	-0.151	-0.098	0900	7000	
	-	-0.130	-0.153	-0.177	-0.175	-0.168	-0134	2000	9000	0.00	-

Table 14. Continued

(b) Concluded

				Sta	tic pressure c	oefficients or	Static pressure coefficients on nozzle sidewall at centerline	wall at center	line			
					-	with values	with values of x/l of-					
7	153	226	300	.337	114.	.484	.558	.632	.705	627.	.853	.926
88	001.0	0 140		-0.147	-0.139	-0.122	-0.106	-0.078	-0.050	-0.017	0.029	0.080
0.000	0.135	0.156		-0.170	-0.154	-0.133	-0.113	-0.081	-0.048	-0.010	0.037	0.090
0.097	0170	0.133		-0.203	-0.185	-0.157	-0.130	-0.103	-0.070	-0.035	9000	0.052
1.051		0003		-0.002	-0.056	-0.100	-0.146	-0.185	-0.222	-0.255	-0.292	-0.328
107.1	0.00	0.00		-0.042	080	-0.129	-0.179	-0.223	-0.258	-0.295	-0.337	-0.348
1.198	9.6	210.0-		5 083	121	-0.157	-0.194	-0.240	-0.280	-0.321	-0.363	-0.364
1.149	0.00	61.0		0000	786	-0.357	-0.374	-0.292	-0.179	-0.117	-0.082	-0.059
0.934	-0.000	0.121		0.243	0.317	-0 346	-0.230	-0.130	-0.107	-0.097	-0.079	-0.053
0.92/	-0.112	-0.149		0.543	2000	0100	0.156	0.135	-0.115	190 0-	-0.063	-0.028
0.897	-0.134	-0.175	<u>'</u>	-0.209	-0.502	-0.210	0.1.0	251.0	200	1900	0.046	1100
0.877	-0.142	-0.184	1	-0.263	-0.252	-0.189	-0.138	-0.133	201.02	-0.001	200	
0.848	-0.147	-0.184	1	-0.234	-0.211	-0.178	-0.151	-0.122	-0.092	90.0	-0.020	0.014
0.00	0.153	186	,	-0.216	-0.199	-0.172	-0.142	-0.113	-0.081	-0.047	-0.006	0.041
0.002	0133	0.156		-0.171	-0.157	-0.135	-0.112	-0.080	-0.048	-0.012	0.036	0.088
30.0	-0.137	0.130		0 148	921.0	9119	-0.102	-0.079	-0.048	-0.016	0.029	0.081
0.001	-0.122	-0.139				201	7000	0.065	0.042	-0.014	0.023	0.070
0.401	-0.101	-0.116		-0.124	11.7	-0.1W	-0.000	CONTO	725.0	1	2	

		Stati	Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$	efficients on	nozzle sidew	- all at $z/Z = -$	0.50	
				with values of x/l of-	—Jo <i>I/x</i> Jo			
M	.153	.226	300	.337	.411	.558	.705	.926
0090		-0.174	-0.224	-0.203	_	-0.144	-0.087	4
0.697		-0.192	-0.251	-0.230	1	-0.153	-0.081	ı
0.799		-0.203	-0.291	-0.273	1	-0.171	-0.100	
1.251	1	0.004	-0.057	-0.063	1	-0.200	-0.274	
198	,	-0.017	-0.076	-0.086	-	-0.234	-0.316	
149	1	-0.053	-0.117	-0.128	1	-0.259	-0.344	_
0.054	1	-0.130	-0.239	-0.265	1	-0.398	-0.178	-
0 927	1	-0.161	-0.275	-0.303	1	-0.235	-0.124	I
0.897	١	-0.189	-0.306	-0.333	1	-0.179	-0.138	ı
0.877	1	-0.196	-0.319	-0.334	1	-0.186	-0.130	ţ
0.848	,	-0.206	-0.311	-0.310	1	-0.184	-0.119	1
0.802		-0.217	-0.303	-0.285		-0.181	-0.113	1
0.700	,	-0.195	-0.252	-0.231	t	-0.153	-0.083	-
0.601	\ -	-0.175	-0.222	-0.201	1	-0.144	-0.083	1
0.401	,	-0.150	-0.187	-0.167	1	-0.126	-0.081	l
,								

Table 14. Continued

(c) Static pressure coefficients on nozzle bottom flap

	·		_	_		r		_	_	_		_	_	_	_	
	.926	1	1	1	1	I	-		ı		1	1	1	1	ļ	
	.853	0.082	0.074	0.023	-0.155	-0.149	-0.158	-0.115	-0.087	-0.057	-0.041	-0.016	0.008	0.070	0.081	0.084
= 0.75	671.	0.033	0.030	-0.013	-0.227	-0.219	-0.234	-0.150	-0.115	-0.088	-0.071	-0.044	-0.025	0.028	0.034	0.041
n flap at y/Y :	.705	-0.005	-0.006	-0.039	-0.325	-0.310	-0.309	-0.179	-0.142	-0.119	-0.102	-0.075	-0.050	-0.007	-0.005	-0.001
ozzle botton	.558	-0.117	-0.113	-0.122	-0.351	066.0-	-0.430	-0.241	-0.202	-0.188	-0.175	-0.153	-0.134	-0.112	-0.116	-0.110
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.75$ with values of x/I of—	.411	-0.308	-0.324	-0.304	-0.374	-0.418	-0.477	-0.425	-0.302	-0.294	-0.284	-0.275	-0.314	-0.323	-0.307	-0.279
pressure coc	.337	ı	1	ı	ļ	1	-	-	-	_	-	_	****	_	-	l
Static	.300	689.0-	-0.794	-0.762	-0.193	-0.231	-0.282	-0.492	-0.542	-0.595	-0.629	-0.677	-0.757	-0.787	-0.682	-0.588
	.226	-0.293	-0.307	-0.277	-0.006	-0.024	-0.063	-0.156	-0.186	-0.218	-0.234	-0.251	-0.286	-0.309	-0.293	-0.265
	.153	-0.199	-0.206	-0.185	0.009	-0.012	-0.042	-0.098	-0.124	-0.148	-0.160	-0.173	-0.196	-0.205	-0.199	-0.180
	M_{∞}	0.600	0.697	0.799	1.251	1.198	1.149	0.954	0.927	0.897	0.877	0.848	0.802	0.700	0.601	0.401

		Static	Static pressure coefficients on nozzle bottom flap at $y/Y = 0.50$	efficients on	nozzle bottor	n flap at y/Y	= 0.50		
				with value	with values of x/l of-				
	.226	300	.337	.411	.558	207.	622	.853	.926
	-0.407	-0.931	-0.474	-0.217	-0.033	0.085	0.138	0.182	0.215
	-0.418	-1.163	-0.498	-0.216	-0.028	0.090	0.139	0.179	0.212
	-0.333	[-1.035	-0.542	-0.282	-0.083	0.016	0.054	0.084	0.119
	-0.010	-0.385	-0.515	-0.445	-0.374	-0.141	-0.106	-0.079	-0.053
	-0.031	-0.434	-0.569	-0.486	-0.366	-0.149	-0.119	-0.090	-0.065
	-0.068	-0.492	-0.631	-0.550	-0.338	-0.170	-0.138	-0.110	-0.081
	-0.180	-0.761	-0.612	-0.383	-0.257	-0.183	-0.150	-0.117	-0.084
-0.134	-0.209	-0.750	-0.446	-0.316	-0.227	-0.158	-0.129	-0.094	-0.065
	-0.246	-0.771	-0.440	-0.322	-0.215	-0.130	-0.094	-0.056	-0.022
-0.173	-0.264	-0.795	-0.442	-0.318	-0.198	-0.111	-0.070	-0.032	9000
-0.190	-0.293	-0.839	-0.454	-0.312	-0.165	-0.067	-0.029	0.008	0.045
-0.219	-0.342	-1.010	-0.548	-0.297	-0.103	0.000	0.036	690'0	0.103
-0.258	-0.416	-1.161	-0.499	-0.219	-0.030	0.089	0.136	0.175	0.206
-0.257	-0.406	-0.927	-0.472	-0.215	-0.034	0.083	0.134	0.178	0.211
	-0.371	-0.781	-0.425	-0.197	-0.033	0.078	0.130	0.175	0.209

Table 14. Concluded

(c) Concluded

		Static	pressure coe	fficients on 1	nozzle botton	Static pressure coefficients on nozzle bottom flap at centerline	rline	
				with values of x/l of-	—to //v. jo			
N	.153	.226	.300	.337	.411	.558	.705	.926
0090	-0.280	-0.445	-1.003	-0.516	-0.231	-0.022	0.098	-
0.000	-0.288	-0.453	-1.305	-0.544	-0.230	-0.013	0.102	I
0 700	-0.228	-0.351	-0.999	-0.505	-0.285	-0.102	0.003	1
1 251	0 004	-0.017	-0.385	-0.509	-0.486	-0.206	-0.158	1
107:1	-0.015	-0.038	-0.434	-0.566	-0.534	-0.220	-0.172	ł,
0/11	-0.045	-0.071	-0.494	-0.631	-0.601	-0.253	-0.202	l
0.054	-0.115	-0.195	-0.755	-0.520	-0.358	-0.263	-0.201	1
0.00	0130	_0.223	-0.716	-0.402	-0.302	-0.230	-0.172	Ì,
0.927	910	_0.253	-0.714	-0.383	-0.297	-0.223	-0.149	١
0.077	0.100	0.276	-0.741	-0.396	-0.301	-0.212	-0.127	ı
0.07	000	10 304	-0.806	-0.417	-0.301	-0.178	-0.083	1
0.040	0.236	-0.359	-0.968	-0.499	-0.296	-0.121	-0.014	
2007	060 0	-0.454	-1.290	-0.548	-0.231	-0.016	0.102	-
1090	-0.289	44.6	-0.995	-0.515	-0.231	-0.024	0.098	-
0401	-0.267	-0.400	-0.830	-0.457	-0.217	-0.026	0.091	-
104.0	10.50	22.00						

(d) Force data

															_
cDf	0.0136	0.0133	0.0130	0.0121	0.0122	0.0123	0.0127	0.0128	0.0129	0.0129	0.0130	0.0131	0.0134	0.0137	0.0146
$C_{D,p}$	0.0422	0.0538	0.1086	0.2036	0.2154	0.2383	0.2091	0.1808	0.1651	0.1551	0.1386	0.1192	0.0555	0.0432	0.0343
$a_{\mathcal{O}}$	0.0460	0.0543	0.1061	0.2412	0.2564	0.2708	0.2065	0.1771	0.1584	0.1456	0.1301	0.1026	0.0554	0.0504	0.0414
M ₈	0.600	0.697	0.799	1.251	1.198	1.149	0.954	0.927	0.897	0.877	0.848	0.802	0.700	0.601	0.401

Table 15. Pressure and Force Data for Nozzle 9 With $\beta_{t,lop/bot} = 17.9^{\circ}/\beta_{t,side} = 0^{\circ}$ and Plume Off

(a) Static pressure coefficients on nozzle top flap

	7	_	_	_	•	,	_	_	_	_	_		_	_		_		_		_			
	.926	-0.100	0.189	0.184	0.187	0.190	0.190	0.169	0.180	-0.048	-0.018	0.039	0.184	-0.143	-0.086	-0.121	-0.103	-0.078	-0.090	-0.080	-0.066	-0.064	-0.056
	.853	-0.119	0.153	0.138	0.154	0.153	0.145	0.116	0.142	-0.075	-0.049	0.009	0.156	-0.160	-0.133	-0.141	-0.125	-0.106	-0.115	-0.102	-0.097	-0.104	-0.099
	677.	-0.128	0.113	0.091	0.113	0.112	0.103	0.072	0.103	-0.101	-0.078	-0.017	0.122	-0.171	-0.214	-0.151	-0.137	-0.124	-0.133	-0.122	-0.128	-0.143	-0.141
line	.705	-0.140	0.069	0.044	890.0	690'0	090'0	0:030	0.057	-0.124	-0.103	-0.048	080'0	-0.189	-0.392	-0.160	-0.148	-0.139	-0.146	-0.138	-0.154	-0.177	-0.178
Static pressure coefficients on nozzle top flap at centerline with values of .x/l of—	.632	-0.154	0.020	-0.011	0.019	0.023	0.014	-0.015	0.014	-0.144	-0.129	-0.081	0.031	-0.209	-0.503	691.0-	-0.160	-0.158	-0.161	-0.155	-0.181	-0.212	-0.218
efficients on nozzle top with values of x/l of—	.558	-0.196	-0.042	-0.076	-0.041	-0.034	-0.040	-0.068	-0.044	-0.168	-0.158	-0.119	-0.030	-0.405	-0.504	-0.185	-0.175	-0.175	-0.178	-0.171	-0.206	-0.245	-0.257
coefficients o	.484	-0.447	-0.122	-0.161	-0.124	-0.111	-0.116	-0.143	-0.122	-0.194	-0.187	-0.165	-0.114	-0.518	-0.513	-0.206	-0.194	-0.195	-0.195	-0.189	-0.228	-0.277	-0.297
itic pressure o	.411	-0.494	-0.253	-0.296	-0.252	-0.234	-0.234	-0.262	-0.240	-0.223	-0.221	-0.222	-0.249	-0.540	-0.557	-0.246	-0.222	-0.219	-0.222	-0.211	-0.254	-0.313	-0.343
Sta	.337	-0.520	-0.549	-0.610	-0.554	-0.523	-0.520	-0.558	-0.501	-0.274	-0.275	-0.317	-0.636	-0.575	-0.572	-0.345	-0.291	-0.268	-0.289	-0.266	-0.316	-0.405	-0.449
	.300	-0.387	-1.087	-1.212	-1.094	-1.025	-1.014	-1.090	-0.902	-0.603	-0.608	-0.726	-1.405	-0.426	-0.433	-0.655	-0.608	-0.578	-0.616	-0.580	-0.627	-0.721	-0.771
	.226	-0.018	-0.497	-0.526	-0.499	-0.477	-0.465	-0.471	-0.450	-0.268	-0.293	-0.351	-0.480	-0.030	-0.036	-0.179	-0.209	-0.242	-0.221	-0.238	-0.254	-0.259	-0.256
	.153	1	ı	1	ı	-	ı	1	1	1	1	1	1	ı	1	I	1	ı	1	1	1	-	ŧ
	α, deg	0.002	0.005	-2.990	0.035	3.003	6.007	9.020	0.020	-0.018	0.000	-0.020	-0.035	-2.991	2.974	0.012	-0.086	-0.131	-3.040	0.085	2.836	6.572	9.226
	M∞	1.251	0.600	0.601	0.603	0.600	0.601	0.601	0.402	0.874	0.851	0.800	0.702	1.200	1.200	0.952	0.927	0.901	0.903	0.902	0.898	0.899	0.897

Table 15. Continued
(a) Continued

				Stal	Static pressure coefficients on nozzle top flap at $y/Y = 0.25$	oefficients or	nozzle top	flap at $y/Y =$	0.25		
					•	with values of x/l of	—Jo 1/x Jo				
М	a, deg	.153	.226	300	.337	.411	.558	501.	6 <i>LL</i>	.853	.926
1.251	0.002	-0.002	-0.012	-0.377	-0.520	-0.491	-0.223	-0.139	-0.127	-0.115	-0.100
0.600	0.005	-0.303	-0.477	-1.074	-0.550	-0.247	-0.047	0.063	0.108	0.148	0.184
0.601	-2.990	-0.317	-0.505	-1.193	-0.612	-0.287	8/0.0-	0.037	0.085	0.134	0.179
0.603	0.035	-0.304	-0.480	-1.078	-0.554	-0.246	-0.046	0.063	0.108	0.149	0.186
0.600	3.003	-0.291	-0.459	-1.022	-0.524	-0.228	-0.039	0.063	0.106	0.146	0.187
0.601	6.007	-0.281	-0.445	-1.016	-0.522	-0.233	-0.047	0.051	960'0	0.137	0.183
0.601	9.020	-0.281	-0.450	-1.079	-0.562	-0.263	920'0-	0.016	0.061	0.104	0.157
0.402	0.020	-0.285	-0.437	-0.890	-0.502	-0.237	-0.049	0.052	0.097	0.138	0.177
0.874	-0.018	-0.166	-0.261	-0.625	-0.290	-0.228	-0.171	-0.122	660'0-	-0.075	-0.046
0.851	0000	-0.182	-0.285	-0.649	-0.297	-0.227	-0.159	-0.101	9/0.0-	-0.049	-0.018
0.800	-0.020	-0.221	-0.342	-0.788	-0.346	-0.225	-0.117	-0.046	-0.014	0.013	0.040
0.702	-0.035	-0.293	-0.465	-1.394	-0.628	-0.248	-0.036	0.072	0.118	0.154	0.183
1.200	-2.991	-0.014	-0.026	-0.419	-0.573	-0.539	-0.434	-0.190	-0.171	-0.157	-0.138
1.200	2.974	-0.008	-0.030	-0.425	-0.574	-0.558	-0.466	-0.391	-0.278	-0.154	-0.095
0.952	0.012	-0.099	-0.170	-0.660	-0.358	-0.250	-0.185	-0.161	-0.151	-0.139	-0.122
0.927	-0.086	-0.123	-0.200	-0.610	-0.296	-0.221	-0.174	-0.149	-0.138	-0.121	-0.103
0.901	-0.131	-0.148	-0.234	-0.598	-0.283	-0.221	-0.173	-0.142	-0.125	-0.103	-0.080
0.903	-3.040	-0.134	-0.212	-0.624	-0.293	-0.222	-0.178	-0.145	-0.132	-0.116	-0.093
0.905	0.085	-0.147	-0.230	-0.610	-0.288	-0.221	-0.176	-0.138	-0.122	-0.102	-0.079
0.898	2.836	-0.158	-0.244	-0.663	-0.341	-0.261	-0.208	-0.156	-0.128	-0.095	-0.064
0.899	6.572	-0.166	-0.250	-0.741	-0.427	-0.320	-0.247	-0.179	-0.144	-0.104	-0.063
0.897	9.226	-0.170	-0.251	-0.777	-0.459	-0.347	-0.260	-0.182	-0.143	-0.097	-0.054

Table 15. Continued

(a) Continued

				Sta	tic pressure	coefficients o	fficients on nozzle top	Static pressure coefficients on nozzle top flap at $y/Y = 0.50$	0.50		
M	α, deg	.153	.226	.300	.337	411	.558	.705	<i>6LL</i> :	.853	.926
1.251	0.002	-0.002	-0.010	-0.383	-0.524	-0.445	-0.319	-0.141	-0.121	-0.111	-0.099
0.600	0.005	-0.274	-0.430	-1.001	-0.521	-0.246	-0.063	0.037	0.082	0.128	0.170
0.601	-2.990	-0.283	-0.453	-1.120	-0.577	-0.280	-0.088	0.013	0.062	0.110	0.157
0.603	0.035	-0.272	-0.434	-1.008	-0.522	-0.246	-0.063	0.039	0.082	0.130	0.171
0.600	3.003	-0.262	-0.408	-0.952	-0.483	-0.228	-0.064	0.032	0.074	0.119	0.159
0.601	6.007	-0.258	-0.392	-1.004	-0.490	-0.229	-0.076	0.012	0.054	0.098	0.142
0.601	9.020	-0.275	-0.413	-1.068	-0.521	-0.248	-0.096	-0.019	0.018	090'0	0.108
0.402	0.020	-0.257	-0.395	-0.833	-0.467	-0.226	-0.059	0.032	0.072	0.117	0.159
0.874	-0.018	-0.161	-0.248	-0.692	-0.327	-0.236	-0.167	-0.118	-0.097	-0.072	-0.042
0.851	0.000	-0.175	-0.270	-0.731	-0.341	-0.236	-0.152	-0.092	-0.069	-0.041	-0.014
0.800	-0.020	-0.207	-0.321	-0.904	-0.413	-0.222	-0.099	-0.034	-0.011	0.015	0.038
0.702	-0.035	-0.268	-0.425	-1.343	-0.559	-0.247	-0.054	0.051	0.094	0.136	0.170
1.200	-2.991	-0.016	-0.024	-0.423	-0.572	-0.496	-0.405	-0.212	-0.167	-0.148	-0.134
1.200	2.974	-0.013	-0.028	-0.434	-0.595	-0.508	-0.392	-0.349	-0.306	-0.259	-0.199
0.952	0.012	-0.096	-0.161	-0.691	-0.380	-0.256	-0.186	-0.159	-0.151	-0.137	-0.122
0.927	-0.086	-0.120	-0.191	-0.646	-0.317	-0.230	-0.176	-0.149	-0.137	-0.121	-0.104
0.901	-0.131	-0.145	-0.225	-0.651	-0.312	-0.230	-0.174	-0.140	-0.121	-0.102	-0.078
0.903	-3.040	-0.130	-0.206	-0.681	-0.323	-0.234	-0.178	-0.142	-0.129	-0.113	-0.096
0.902	0.085	-0.143	-0.224	-0.660	-0.315	-0.232	-0.176	-0.139	-0.123	-0.101	-0.078
0.898	2.836	-0.156	-0.239	-0.714	-0.375	-0.280	-0.207	-0.149	-0.119	-0.086	-0.053
0.899	6.572	-0.169	-0.247	-0.800	-0.455	-0.344	-0.245	-0.174	-0.134	-0.092	-0.050
0.897	9.226	-0.188	-0.265	-0.815	-0.474	-0.359	-0.257	-0.177	-0.135	-0.091	-0.047

Table 15. Continued

(a) Concluded

0.005 -0.066 -0.0790.076 0.009 -0.068-0.318-0.069-0.0840.089 0.074 -0.072-0.157-0.047 -0.192-0.117-0.095-0.0700.077 0.070 926 -0.245 -0.089 0.026 -0.0160.026 -0.133-0.096 -0.114-0.109-0.0450.027 0.028 -0.118-0.067 -0.112 -0.091 -0.188-0.045-0.117.853 1 Static pressure coefficients on nozzle top flap at y/Y = 0.75-0.046 -0.124-0.354-0.128-0.127-0.306 -0.048-0.144 -0.048 -0.109 -0.089 -0.368-0.153-0.137-0.176-0.050-0.102-0.056-0.134-0.177-0.051 -0.158705 with values of x/l of-.558 ı 1 ı ı 1 I 1 -0.219 -0.214-0.326 -0.294 -0.294 -0.296-0.212 -0.211 -0.339-0.398-0.238-0.215-0.252 -0.313 -0.358-0.212-0.321-0.369-0.323-0.241 -0.311 41 -0.437 -0.535 -0.412 -0.426 -0.442 -0.426 -0.349 -0.458 -0.448 -0.468 -0.435-0.452-0.443-0.499-0.484-0.429-0.361 -0.481 .337 -0.726 -0.729 -0.705 -0.748-0.782 -0.688 -0.623 -0.650 -0.758 -0.304 -0.612-0.709-0.695-0.277 -0.858 -0.672-0.902 -0.935 -0.342-0.658 .300 -0.225 -0.332 -0.148-0.176 -0.189-0.203-0.235-0.253-0.265-0.316-0.323-0.279-0.050-0.207-0.009 -0.319 -0.328-0.292-0.318.226 -0.317-0.238 -0.186 -0.023-0.135-0.129 -0.153-0.185-0.226-0.222-0.171-0.220-0.152-0.089-0.1120.000 -0.215-0.217 -0.222 -0.021-0.163.153 a, deg 2.836 9.226 0.005 0.035 -0.018 -0.020 -0.0352.974 0.012 0.085 6.572 3.003 9.020 0.002 000 -0.086-0.131-3.040 -2.991 0.899 0.600 0.874 $0.851 \\ 0.800$ 0.702 1.200 0.952 0.927 0.903 0.902 0.898 0.897 0.603 0.402 Z 8 0.600 0.601 0.601 0.6011.251

Table 15. Continued

(b) Static pressure coefficients on nozzle sidewall

-0.076-0.066 -0.046 -0.045 -0.059-0.034 -0.065 -0.092-0.039 -0.313-0.017-0.093-0.079-0.090-0.387-0.117-0.0730.081 -0.07-0.502-0.152 -0.123-0.166-0.168-0.173-0.083-0.068 -0.062-0.121 -0.085 -0.094 -0.166-0.153-0.122-0.122-0.351-0.150.853 -0.157-0.101669.9 Static pressure coefficients on corner between nozzle top flap and sidewall -0.132 -0.180 -0.230-0.270-0.188-0.158-0.099-0.479-0.422-0.088 -0.104-0.203611: -0.471-0.177-0.277-0.127-0.103-0.091 -0.091 0.102 -0.143-0.207.705 -0.218-0.349-0.216-0.129-0.284-0.129 -0.205-0.383-0.548 -0.143 -0.114-0.105 -0.217-0.137-0.240-0.165-0.361 -0.173-0.237-0.121 with values of x/l of--0.361 -0.216-0.297 -0.188-0.235-0.296-0.165-0.175 -0.238-0.398 -0.187-0.278-0.142-0.205-0.256-0.168-0.153-0.155-0.231-0.271 .558 -0.264 -0.254 -0.306 -0.219 -0.260-0.395-0.254-0.275-0.314-0.286 -0.366 -0.476-0.453-0.293-0.337-0.234-0.235-0.284-0.291-0.385<u>4</u>. -0.386 -0.396 -0.454-0.424-0.449 -0.349-0.523 -0.454-0.220-0.393-0.502-0.442 -0.458-0.494-0.534-0.570-0.191 -0.523-0.547 -0.251-0.523-0.581-0.370 -0.416 -0.089 -0.370-0.325-0.402 -0.414-0.144 -0.306 -0.342 -0.378 -0.376-0.374-0.385-0.413-0.427-0.398-0.443300 -0.425-0.411 -0.112 226 1 ı ١ 1 -0.183-0.209 -0.163-0.024 0.168 -0.184 0.003 -0.222-0.143-0.152-0.085-0.129 -0.145-0.187-0.108-0.192-0.168-0.130.153 -0.1289.05 α, deg 0.002 0.005 9.020 0.000 -2.991 2.974 3.003 -0.018-0.086 -3.040 9.226 0.035 0.012 2.836 -0.035-0.1316.572 0.600 0.603 0.600 0.601 0.874 0.851 0.702 1.200 0.952 0.902 0.601 0.927 0.903 0.898 0.899 \mathbf{z}_{8} .251 0.90 0.897

Table 15. Continued

(b) Continued

				—,							_									—	_		
	.926	-			1	1				-		1	1			1	I		1		1		1
	.853	-0.357	-0.057	-0.029	-0.061	-0.110	-0.188	-0.290	-0.069	-0.068	-0.056	-0.040	-0.046	-0.348	-0.444	-0.130	-0.094	-0.078	-0.099	-0.080	-0.115	-0.205	-0.258
0.50	622.	-0.323	-0.103	690.0-	-0.103	-0.161	-0.245	-0.344	-0.105	-0.092	-0.084	-0.077	-0.093	-0.314	-0.414	-0.148	-0.102	-0.100	-0.102	-0.099	-0.143	-0.237	-0.293
Static pressure coefficients on nozzle sidewall at $z/Z = 0.50$ with values of x/l of—	.705	-0.288	-0.132	-0.100	-0.132	-0.190	-0.273	-0.365	-0.129	-0.121	-0.117	-0.110	-0.127	-0.282	-0.374	-0.187	-0.119	-0.123	-0.118	-0.122	-0.171	-0.257	-0.311
of x/l of—	.558	-0.207	-0.174	-0.142	-0.176	-0.232	-0.308	-0.390	-0.159	-0.168	-0.170	-0.170	-0.184	-0.206	-0.288	-0.280	-0.229	-0.172	-0.181	-0.173	-0.207	-0.277	-0.322
oefficients on nozzle sid with values of x/l of—	.411	-0.119	-0.211	-0.191	-0.213	-0.258	-0.320	-0.386	-0.187	-0.263	-0.241	-0.233	-0.233	-0.135	-0.178	-0.342	-0.338	-0.320	-0.279	-0.323	-0.403	-0.495	-0.539
ic pressure c	.337	-0.054	-0.223	-0.216	-0.225	-0.255	-0.300	-0.350	-0.194	-0.317	-0.300	-0.271	-0.252	-0.076	-0.097	-0.254	-0.287	-0.315	-0.324	-0.315	-0.335	-0.368	-0.409
Stat	300	-0.035	-0.224	-0.224	-0.223	-0.246	-0.287	-0.333	-0.196	-0.283	-0.282	-0.272	-0.255	-0.057	-0.074	-0.210	-0.243	-0.271	-0.275	-0.264	-0.281	-0.312	-0.351
	.226	-0.004	-0.188	-0.193	-0.191	-0.208	-0.236	-0.275	-0.166	-0.191	-0.198	-0.206	-0.207	-0.024	-0.040	-0.123	-0.150	-0.173	-0.180	-0.173	-0.191	-0.223	-0.255
	.153	0.002	-0.159		-0.159	_	-0.201	-0.231	-0.140		-0.145	-0.161			-0.029	-0.085	-0.108	-0.128	-0.134	-0.126	-0.143	-0.172	-0.197
	α, deg	0.002	0.005	-2.990	0.035	3.003	6.007	9.020	0.020	-0.018	0.000	-0.020	-0.035	-2.991	2.974	0.012	-0.086	-0.131	-3.040	0.085	2.836	6.572	9.226
	M	1.251	0.600	0.601	0.603	0.600	0.601	0.601	0.402	0.874	0.851	0.800	0.702	1.200	1.200	0.952	0.927	0.901	0.903	0.902	0.898	0.899	0.897

Table 15. Continued

(b) Continued

_	_	_	_	_	_	_	_	_		_	_		_	_	_	_		_	_		_	_
.926	-0.326	9:00	0.037	0.035	0.029	0.011	-0.015	0.027	60.0-	-0.022	0.003	0.045	-0.356	-0.363	-0.107	-0.081	-0.058	980:0-	-0.058	-0.049	090:0-	290'0-
.853	-0.294	-0.015	-0.017	-0.013	-0.021	-0.044	-0.081	-0.019	-0.068	-0.054	-0.038	-0.008	-0.330	-0.335	-0.137	-0.101	-0.086	-0.118	-0.084	-0.079	-0.099	-0.118
6LL:	-0.257	-0.050	-0.054	-0.051	-0.060	-0.085	-0.126	-0.050	-0.099	-0.087	-0.071	-0.047	-0.291	-0.298	-0.193	-0.109	-0.106	-0.139	-0.105	-0.102	-0.128	-0.153
.705	-0.221	-0.078	-0.083	-0.077	-0.087	-0.112	-0.153	-0.071	-0.122	-0.112	-0.099	-0.079	-0.256	-0.263	-0.263	-0.138	-0.127	-0.152	-0.121	-0.120	-0.146	-0.174
.632	-0.189	-0.101	-0.107	-0.101	-0.110	-0.137	-0.176	-0.092	-0.143	-0.137	-0.126	-0.107	-0.222	-0.229	-0.321	-0.214	-0.143	-0.185	-0.140	-0.137	-0.160	-0.189
.558	-0.146	-0.124	-0.131	-0.124	-0.133	-0.154	-0.190	-0.109	-0.168	-0.163	-0.154	-0.135	-0.180	-0.185	-0.355	-0.309	-0.194	-0.248	-0.188	-0.168	-0.209	-0.237
.484	-0.101	-0.140	-0.147	-0.140	-0.149	-0.170	-0.204	-0.119	-0.206	-0.188	-0.176	-0.154	-0.134	-0.139	-0.340	-0.341	-0.281	-0.289	-0.277	-0.277	-0.330	-0 345
.411	-0.055	-0.154	-0.160	-0.153	-0.161	-0.178	-0.211	-0.129	-0.269	-0.232	-0.204	-0.174	-0.085	-0.092	-0.277	-0.306	-0.313	-0.315	-0.316	-0.332	-0.355	-0 381
.337	-0.024	-0.162	-0.168	-0.162	-0.168	-0.189	-0.219	-0.136	-0.261	-0.244	-0.219	-0.187	-0.048	-0.061	-0.204	-0.236	-0.261	-0.267	-0.257	-0.267	-0.293	-0 330
.300		1	1	ļ	,	1	ı	1	ı		ı	1				: 1	-	-	1	1		
.226	0.002	-0.148	-0.155	-0.149	-0.157	-0.177	-0.209	-0.124	-0.176	-0.180	-0.183	-0.168	-0.018	-0.031	-0.116	-0.143	-0.166	-0.172	-0.162	-0.172	-0.196	0.230
.153	0.003	-0.132	-0.142	-0.135	-0.143	-0.163	-0.196	-0.112	-0.135	-0.139	-0.150	-0.145	-0.016	-0.030	-0.083	-0.108	-0.128	-0.133	-0.124	-0.132	-0.157	2 190
α, deg	0.002	0.005	-2.990	0.035	3.003	6.007	9.020	0.020	-0.018	0.000	-0.020	-0.035	-2.991	2.974	0.012	-0.086	-0.131	-3.040	0.085	2.836	6.572	9000
M	1.251	0.600	0.601	0.603	0.600	0.601	0.601	0.402	0.874	0.851	0.800	0.702	1.200	1.200	0.952	0.927	0.901	0.903	0.905	0.898	0.899	0 807
	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - -0.024 -0.055 -0.101 -0.146 -0.189 -0.221 -0.294	α , deg.153.226.300.337.411.484.558.632.705.779.8530.0020.0030.0020.024-0.055-0.101-0.146-0.189-0.221-0.257-0.2940.005-0.1480.162-0.154-0.140-0.124-0.101-0.078-0.050-0.015	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - 0.024 -0.055 -0.101 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - 0.162 -0.154 -0.124 -0.101 -0.078 -0.050 -0.015 -2.990 -0.142 -0.165 -0.160 -0.147 -0.131 -0.107 -0.083 -0.054 -0.017	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - 0.024 -0.055 -0.101 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - -0.154 -0.140 -0.124 -0.101 -0.078 -0.050 -0.015 -2.990 -0.142 -0.162 -0.147 -0.147 -0.131 -0.107 -0.054 -0.015 0.035 -0.148 - -0.168 -0.160 -0.147 -0.101 -0.083 -0.054 -0.017	α , deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - -0.024 -0.055 -0.101 -0.146 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - -0.162 -0.154 -0.101 -0.078 -0.050 -0.015 -2.990 -0.142 -0.153 -0.147 -0.131 -0.107 -0.083 -0.054 -0.017 0.035 -0.149 - -0.162 -0.153 -0.140 -0.101 -0.077 -0.051 -0.013 3.003 -0.143 -0.140 -0.124 -0.101 -0.051 -0.051 -0.013 -0.135 -0.149 -0.153 -0.140 -0.101 -0.007 -0.051 -0.013 -0.035 -0.149 -0.133 -0.101 -0.060 -0.060 -0.021	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - -0.024 -0.055 -0.101 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - -0.162 -0.154 -0.101 -0.078 -0.050 -0.015 -2.990 -0.142 -0.142 -0.107 -0.083 -0.054 -0.017 0.035 -0.149 - -0.162 -0.153 -0.140 -0.107 -0.083 -0.054 -0.017 0.035 -0.149 - -0.164 -0.163 -0.101 -0.077 -0.051 -0.013 3.003 -0.143 -0.168 -0.161 -0.149 -0.101 -0.107 -0.060 -0.051 4.007 -0.143 -0.164 -0.164 -0.137 -0.085 -0.044	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - -0.024 -0.055 -0.101 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - -0.162 -0.154 -0.140 -0.101 -0.078 -0.050 -0.015 0.035 -0.142 -0.155 - -0.168 -0.160 -0.124 -0.107 -0.083 -0.051 -0.017 0.035 -0.149 - -0.168 -0.163 -0.149 -0.101 -0.077 -0.051 -0.013 3.003 -0.143 -0.149 -0.133 -0.110 -0.067 -0.060 -0.021 6.007 -0.163 -0.168 -0.161 -0.179 -0.137 -0.189 -0.044 9.020 -0.196 -0.209 -0.211 -0.190 -0.153 -0.132 -0.189 -0.085 -0.096	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - 0.024 -0.055 -0.101 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.132 -0.168 -0.164 -0.144 -0.107 -0.078 -0.050 -0.015 -2.990 -0.142 -0.155 - -0.168 -0.160 -0.147 -0.107 -0.083 -0.054 -0.017 0.035 -0.142 -0.140 -0.124 -0.101 -0.077 -0.051 -0.013 3.003 -0.143 -0.149 -0.133 -0.101 -0.067 -0.060 -0.013 6.007 -0.163 -0.168 -0.161 -0.149 -0.134 -0.112 -0.085 -0.044 9.020 -0.163 -0.219 -0.219 -0.170 -0.194 -0.185 -0.134 -0.195 -0.165 -0.085 -0.044 <	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - -0.024 -0.055 -0.101 -0.189 -0.227 -0.294 0.005 -0.132 -0.148 - -0.164 -0.140 -0.124 -0.101 -0.078 -0.050 -0.015 -2.990 -0.142 -0.145 - -0.168 -0.160 -0.147 -0.101 -0.077 -0.054 -0.017 0.035 -0.143 -0.149 - -0.149 -0.149 -0.101 -0.077 -0.051 -0.013 3.003 -0.143 -0.143 -0.161 -0.149 -0.134 -0.110 -0.087 -0.060 -0.013 6.007 -0.163 -0.178 -0.170 -0.154 -0.112 -0.087 -0.085 -0.044 9.020 -0.196 -0.219 -0.219 -0.219 -0.190 -0.154 -0.152	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - 0.024 -0.055 -0.101 -0.189 -0.227 -0.257 -0.294 0.005 -0.132 -0.148 - 0.162 -0.154 -0.140 -0.124 -0.101 -0.078 -0.055 -0.015 -2.990 -0.142 -0.155 - 0.168 -0.160 -0.147 -0.107 -0.007 -0.054 -0.017 0.035 -0.135 - 0.168 -0.161 -0.149 -0.107 -0.087 -0.051 -0.013 6.007 -0.143 -0.143 -0.154 -0.149 -0.134 -0.110 -0.087 -0.060 -0.021 6.007 -0.163 -0.219 -0.214 -0.134 -0.134 -0.135 -0.125 -0.087 -0.087 -0.044 9.020 -0.124 -0.219 -0.124 -0.194 -0.134 -0.135	α , deg.153.226.300.337.411.484.558.632.705.779.8530.0020.002-0.024-0.025-0.101-0.146-0.189-0.221-0.257-0.2940.005-0.132-0.1480.162-0.154-0.124-0.101-0.078-0.057-0.015-2.990-0.142-0.1550.168-0.160-0.147-0.131-0.107-0.053-0.054-0.0170.035-0.142-0.1550.168-0.163-0.149-0.124-0.101-0.087-0.051-0.0130.035-0.143-0.1570.168-0.163-0.154-0.137-0.107-0.060-0.0210.020-0.163-0.1770.189-0.178-0.170-0.137-0.125-0.085-0.0440.020-0.196-0.2090.219-0.204-0.190-0.137-0.125-0.026-0.0190.020-0.112-0.1240.261-0.269-0.266-0.168-0.143-0.122-0.099-0.0690.000-0.1800.244-0.232-0.163-0.163-0.124-0.124-0.136-0.137-0.122-0.099-0.0340.020-0.1800.020	a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - -0.024 -0.055 -0.101 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - -0.162 -0.154 -0.140 -0.124 -0.101 -0.078 -0.059 -0.015 -2.990 -0.142 -0.155 - -0.168 -0.167 -0.131 -0.077 -0.054 -0.015 0.035 -0.143 -0.157 - -0.168 -0.161 -0.149 -0.101 -0.087 -0.051 -0.013 0.035 -0.143 -0.157 - -0.168 -0.161 -0.149 -0.101 -0.087 -0.051 -0.011 0.007 -0.163 -0.177 - -0.189 -0.179 -0.134 -0.117 -0.087 -0.081 -0.044 0.020 -0.196 -0.229 -0.196	a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.002 - -0.024 -0.055 -0.101 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - -0.162 -0.154 -0.101 -0.078 -0.050 -0.015 -2.990 -0.142 -0.155 - -0.168 -0.160 -0.147 -0.101 -0.077 -0.054 -0.015 -2.990 -0.142 -0.149 - -0.168 -0.160 -0.144 -0.101 -0.083 -0.054 -0.015 0.035 -0.143 -0.157 - -0.168 -0.161 -0.149 -0.101 -0.087 -0.051 -0.013 0.035 -0.143 -0.157 - -0.168 -0.161 -0.144 -0.101 -0.087 -0.061 0.035 -0.143 -0.134 -0.134 -0.134 -0.134 -0.1	a. deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.002 0.002 -0.024 -0.055 -0.101 -0.146 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - -0.162 -0.164 -0.140 -0.101 -0.078 -0.050 -0.015 -2.990 -0.142 -0.155 - -0.168 -0.160 -0.147 -0.107 -0.077 -0.054 -0.015 -0.035 -0.142 -0.143 -0.157 - -0.169 -0.144 -0.107 -0.077 -0.054 -0.013 0.035 -0.143 -0.157 - -0.168 -0.161 -0.149 -0.107 -0.077 -0.051 -0.013 0.020 -0.163 -0.154 -0.169 -0.134 -0.104 -0.134 -0.107 -0.087 -0.041 0.020 -0.156 -0.219 -0.129	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.002 0.002 - 0.024 -0.055 -0.101 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - 0.162 -0.154 -0.101 -0.107 -0.078 -0.054 -0.015 -2.990 -0.142 -0.155 - 0.160 -0.147 -0.131 -0.107 -0.083 -0.054 -0.017 0.035 -0.142 - 0.155 - 0.162 -0.153 -0.140 -0.124 -0.101 -0.083 -0.054 -0.013 0.035 - 0.143 - 0.157 - 0.168 -0.161 -0.149 -0.131 -0.107 -0.087 -0.013 6.007 - 0.163 - 0.168 - 0.161 - 0.149 - 0.134 - 0.112 - 0.060 - 0.013 6.007 - 0.163 - 0.129 - 0.149 - 0.134 - 0.114 - 0.114 -	a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.002 0.003 0.002 - 0.024 -0.055 -0.101 -0.146 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - 0.162 -0.154 -0.140 -0.107 -0.078 -0.057 -0.057 -0.015 -2.990 -0.142 -0.155 - 0.168 -0.160 -0.147 -0.101 -0.077 -0.083 -0.054 -0.015 -2.990 -0.143 -0.154 -0.164 -0.140 -0.107 -0.083 -0.054 -0.015 0.035 -0.135 -0.149 -0.140 -0.124 -0.140 -0.107 -0.083 -0.054 -0.013 0.037 -0.166 -0.189 -0.189 -0.189 -0.189 -0.194 -0.197 -0.107 -0.081 -0.061 0.020 -0.112 -0.129 -0.189 <	α , deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - -0.024 -0.055 -0.101 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - -0.162 -0.154 -0.101 -0.107 -0.059 -0.015 -0.017 -0.078 -0.057 -0.057 -0.015 -2.990 -0.142 -0.168 -0.160 -0.147 -0.101 -0.077 -0.053 -0.017 -0.017 -0.053 -0.017 -0.017 -0.054 -0.017 -0.017 -0.054 -0.017 -0.017 -0.054 -0.017 -0.017 -0.051 -0.017 -0.017 -0.051 -0.017 -0.017 -0.051 -0.017 -0.017 -0.051 -0.017 -0.017 -0.017 -0.051 -0.017 -0.017 -0.051 -0.017 -0.017 -0.051 -0.017 -0.017 -0.017 -0.017<	α , deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - -0.024 -0.055 -0.101 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - -0.162 -0.154 -0.101 -0.077 -0.039 -0.050 -2.990 -0.142 -0.145 - -0.168 -0.160 -0.124 -0.101 -0.077 -0.053 -2.990 -0.142 -0.168 -0.160 -0.147 -0.101 -0.077 -0.051 -0.017 0.033 -0.145 -0.168 -0.160 -0.124 -0.101 -0.077 -0.081 -0.044 0.020 -0.196 -0.209 - -0.189 -0.178 -0.194 -0.197 -0.027 -0.081 0.020 -0.196 -0.209 - -0.219 -0.139 -0.134 -0.137 -0.112 -0.027 <	α , deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.002 0.002 0.002 0.002 0.0124 -0.016 -0.118 -0.027 -0.257 -0.294 0.005 -0.148 -0.162 -0.154 -0.101 -0.017 -0.018 -0.015 0.205 -0.142 -0.168 -0.160 -0.144 -0.107 -0.083 -0.017 0.205 -0.143 -0.145 - -0.168 -0.160 -0.124 -0.107 -0.083 -0.017 0.005 -0.145 - -0.168 -0.160 -0.124 -0.107 -0.017 -0.081 0.007 -0.163 -0.170 -0.134 -0.107 -0.107 -0.081 -0.001 0.007 -0.163 -0.124 -0.129 -0.109 -0.137 -0.107 -0.082 -0.081 0.000 -0.139 -0.124 -0.219 -0.129	α , deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - -0.024 -0.055 -0.101 -0.189 -0.221 -0.257 -0.294 0.005 -0.132 -0.148 - -0.162 -0.164 -0.104 -0.104 -0.007 -0.007 -0.055 -0.014 -0.107 -0.007 -0.015 -0.015 -0.017 -0.007 -0.007 -0.007 -0.007 -0.007 -0.007 -0.007 -0.007 -0.007 -0.013 -0.007 -0.007 -0.007 -0.001 -0.007 -0.001 -0.007 -0.007 -0.001 -0.007 -0.007 -0.001 -0.007 -0	α, deg 153 .256 .300 .337 .411 .484 .558 .632 .705 .779 .853 0.002 0.003 0.002 - -0.024 -0.055 -0.101 -0.189 -0.257 -0.294 0.005 -0.132 -0.148 - -0.165 -0.165 -0.101 -0.077 -0.057 -0.054 2.990 -0.142 -0.155 - -0.168 -0.160 -0.147 -0.107 -0.054 -0.017 0.035 -0.145 - -0.168 -0.160 -0.147 -0.107 -0.084 -0.017 0.035 -0.145 -0.145 -0.160 -0.149 -0.107 -0.007 -0.051 -0.011 0.035 -0.145 -0.166 -0.161 -0.149 -0.137 -0.117 -0.051 -0.011 0.030 -0.150 -0.150 -0.169 -0.150 -0.107 -0.061 -0.011 0.020 -0.196 -0.150 -0.1

Table 15. Continued

(b) Concluded

			Stati	c pressure co	Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$	nozzle sidew	vall at $z/Z = -$	0.50	
					with values of x/l of-	—jo //x jo			
M	α, deg	.153	.226	300	.337	.411	855.	.705	.926
1.251	0.002	1	0.000	-0.055	-0.063	1	-0.202	-0.276	+
0.600	0.005	-	-0.188	-0.238	-0.216	1	891.0-	-0.123	_
0.601	-2.990	-	-0.205	-0.260	-0.246	1	-0.216	-0.168	
0.603	0.035	1	-0.186	-0.239	-0.216		691.0-	-0.121	_
0.600	3.003	1	-0.193	-0.238	-0.206	1	-0.139	-0.092	l
0.601	6.007	-	-0.216	-0.250	-0.211	_	-0.129	-0.085	_
0.601	9.020	1	-0.261	-0.283	-0.234	_	-0.143	-0.105	_
0.402	0.020		-0.162	-0.203	-0.183	-	-0.154	-0.115	1
0.874	-0.018	ı	-0.194	-0.317	-0.343	I	-0.227	-0.189	_
0.851	0.000	ı	-0.202	-0.321	-0.336	1	-0.224	-0.179	
0.800	-0.020	1	-0.217	-0.318	-0.309	-	-0.220	-0.169	_
0.702	-0.035	1	-0.207	-0.271	-0.249	_	-0.182	-0.125	1
1.200	-2.991	,	-0.028	-0.091	-0.106	-	-0.276	-0.359	_
1.200	2.974	_	-0.039	-0.093	860.0-		-0.211	-0.286	-
0.952	0.012	1	-0.127	-0.237	0.263	_	-0.471	-0.375	-
0.927	-0.086	-	-0.156	-0.270	-0.300	1	-0.413	-0.210	1
0.901	-0.131	-	-0.181	-0.298	0.330	-	-0.246	-0.198	1
0.903	-3.040		-0.195	-0.313	-0.349	-	-0.389	-0.291	1
0.902	0.085	ı	-0.177	-0.293	-0.324	-	-0.246	-0.188	ı
0.898	2.836	I	-0.181	-0.304	-0.330	1	-0.178	-0.137	ı
0.899	6.572	I	-0.210	-0.342	-0.361	-	-0.190	-0.127	ı
0.897	9.226	ı	-0.257	-0.397	-0.413	1	-0.206	-0.144	1

Table 15. Continued

(c) Static pressure coefficients on nozzle bottom flap

				Static	pressure co	efficients on with value	icients on nozzle botto	Static pressure coefficients on nozzle bottom flap at $y/Y = 0.75$ with values of x/l of—	= 0.75		
M_{∞}	α, deg	.153	.226	.300	.337	.411	.558	207.	<i>6LL</i> :	.853	.926
1.251	0.002	0.005	-0.007	-0.195		-0.374	-0.351	-0.372	-0.316	-0.310	
0.600	0.005	-0.211	-0.306	-0.713	1	-0.338	-0.157	-0.050	-0.014	0.027	ı
0.601	-2.990	-0.215	-0.305	-0.636	1	-0.321	-0.151	-0.097	-0.075	-0.026	1
0.603	0.035	-0.211	-0.308	-0.716	ŀ	-0.339	-0.156	-0.052	-0.014	0.028	1
0.600	3.003	-0.216	-0.314	-0.760	1	-0.339	-0.162	-0.048	0.000	0.043	1
0.601	6.007	-0.221	-0.319	-0.782	ı	-0.326	-0.161	-0.049	-0.005	0.038	1
0.601	9.020	-0.233	-0.330	-0.800	1	-0.312	-0.158	-0.054	-0.013	0.030	1
0.402	0.020	-0.194	-0.281	-0.617	ı	-0.310	-0.148	-0.047	-0.009	0.029	1
0.874	-0.018	-0.157	-0.233	-0.633		-0.381	-0.237	-0.159	-0.125	-0.091	
0.851	0.000	-0.170	-0.251	-0.672	I	-0.352	-0.222	-0.140	-0.111	-0.076	
0.800	-0.020	-0.194	-0.288	-0.764	1	-0.383	-0.207	-0.111	-0.081	-0.040	1
0.702	-0.035	-0.217	-0.324	-0.835	****	-0.358	-0.158	-0.056	-0.022	0.020	ı
1.200	-2.991	-0.017	-0.048	-0.272	1	-0.392	-0.409	-0.342	-0.341	-0.327	1
1.200	2.974	-0.029	-0.035	-0.217	-	-0.421	-0.386	-0.399	-0.382	-0.281	1
0.952	0.012	-0.096	-0.156	-0.495	1	-0.696	-0.443	-0.305	-0.249	-0.202	1
0.927	-0.086	-0.122	-0.187	-0.543	-	-0.548	-0.319	-0.223	-0.183	-0.147	1
0.901	-0.131	-0.144	-0.214	-0.589	1	-0.434	-0.259	-0.182	-0.146	-0.113	1
0.903	-3.040	-0.156	-0.236	-0.624	1	-0.527	-0.310	-0.248	-0.219	-0.184	-
0.902	0.085	-0.137	-0.208	-0.585	1	-0.429	-0.253	-0.177	-0.143	-0.111	
0.898	2.836	-0.133	-0.198	-0.571	1	-0.360	-0.226	-0.156	-0.127	-0.095	1
0.899	6.572	-0.138	-0.198	-0.562	1	-0.382	-0.238	-0.157	-0.124	-0.090	
0.897	9.226	-0.149	-0.206	-0.567	1	-0.442	-0.256	-0.162	-0.122	-0.083	1

Table 15. Continued

(c) Continued

0.146 0.159 0.168 0.126 -0.056-0.2070.167 0.157 0.157 -0.020 0.012 0.067 0.165 -0.123-0.049-0.229-0.110 -0.056-0.055-0.087-0.061 -0.063.926 0.125 0.109 0.115 0.025 0.125 -0.143 -0.153-0.129-0.094 -0.096 -0.098 -0.102-0.2770.097 0.077 -0.057-0.101 0.126 -0.091.853 -0.271 -0.302 -0.191 -0.174 -0.143 -0.146 0.046 -0.196-0.3200.080 -0.099 -0.065 0.002 -0.139-0.139-0.1340.081 0.061 0.027 0.081 -0.141Static pressure coefficients on nozzle bottom flap at y/Y = 0.500.032 0.034 -0.1460.032 0.028 -0.1100.034 -0.333-0.295 -0.241 -0.190 -0.187-0.175-0.188 -0.198 -0.019-0.0016.04 140 -0.203.705 with values of x/l of--0.226 -0.382 -0.074 -0.095 -0.125 -0.255-0.409-0.344 -0.335 -0.073-0.298-0.262-0.071 -0.284.558 -0.441 -0.311-0.452 -0.246 -0.246 -0.230 -0.410-0.405 -0.253-0.483-0.506 -0.766 -0.425 -0.382-0.460 -0.227-0.487-0.287-0.301-0.494-0.421 -0.414<u>4</u>. -0.515-0.462-0.456 -0.594-0.590-0.541 -0.925 -0.626 -0.732 -0.620 -0.550-0.717-0.580-0.602-0.506-0.551 -0.687 -0.577-0.50599.0 .337 -0.384 -0.876 -0.766 -0.975-1.088 -1.173-1.240-0.906 -0.943-1.258-0.440-0.815-0.854 -0.852-0.869 -0.817 -1.103 -0.840-0.427-0.857300 -0.894-0.245 -0.234 -0.219 -0.426 -0.404 -0.446 -0.443-0.288-0.179-0.210-0.443-0.392-0.344 -0.034-0.240-0.203-0.192-0.010-0.263-0.4310.041 .226 -0.4270.004 -0.186-0.268-0.254-0.019 -0.026 -0.277 -0.274-0.170-0.103 -0.149 -0.140-0.221 -0.267-0.131-0.121 -0.261 -0.151-0.271.153 -0.161 α, deg 0.005 -2.990 0.035 3.003 9.020 0.020 -0.0180.000 -0.020 -0.0352.974 -0.086 0.085 2.836 6.572 9.226 0.002 6.007 0.012 -2.991-0.1310.603 200 0.600 0.874 0.800 0.702 .200 M 0.601 0.601 0.601 0.402 0.851 0.952 0.927 0.903 0.902 868.0 0.899 1.251 0.901

Table 15. Continued (c) Concluded

			Static	Static pressure coefficients on nozzle bottom flap at centerline with values of x/l of—	micients on with value	icients on nozzle botto with values of x/l of—	m Hap at ce	nterline	
M	α, deg	.153	.226	.300	.337	.411	.558	307.	.926
1.251	0.002	0.005	-0.016	-0.385	-0.508	-0.489	-0.480	-0.398	1
0.600	0.005	-0.303	-0.464	-1.045	-0.548	-0.262	-0.063	0.048	-
109:0	-2.990	-0.290	-0.446	-0.991	-0.516	-0.240	-0.050	0.055	-
0.603	0.035	-0.303	-0.466	-1.052	-0.550	-0.265	-0.061	0.048	1
0.600	3.003	-0.312	-0.484	-1.131	-0.592	-0.297	-0.087	0.027	1
0.601	6.007	-0.313	-0.491	-1.201	-0.621	-0.316	-0.109	0.012	1
0.601	9.020	-0.307	-0.491	-1.241	-0.640	-0.332	-0.127	-0.008	ı
0.402	0.020	-0.284	-0.420	-0.870	-0.486	-0.248	-0.062	0.043	ı
0.874	-0.018	-0.179	-0.271	-0.860	-0.524	-0.388	-0.268	-0.171	1
0.851	0.000	-0.197	-0.297	-0.909	-0.545	-0.391	-0.243	-0.133	1
0.800	-0.020	-0.236	-0.360	-1.074	-0.648	-0.405	-0.182	-0.055	-
0.702	-0.035	-0.297	-0.464	-1.378	-0.612	-0.269	-0.058	0.049	1
1.200	-2.991	-0.012	-0.036	-0.432	-0.562	-0.546	-0.535	-0.384	1
1.200	2.974	-0.021	-0.041	-0.431	-0.560	-0.544	-0.510	-0.207	_
0.952	0.012	-0.108	-0.192	-0.782	-0.911	-0.742	-0.389	-0.255	
0.927	980.0-	-0.133	-0.218	-0.817	-0.672	-0.453	-0.336	-0.246	1
0.901	-0.131	-0.156	-0.247	-0.830	-0.551	-0.407	-0.306	-0.211	1
0.903	-3.040	-0.162	-0.247	-0.882	-0.661	-0.474	-0.351	-0.236	1
0.902	0.085	-0.157	-0.244	-0.822	-0.540	-0.400	-0.295	-0.207	1
0.898	2.836	-0.150	-0.238	-0.782	-0.475	-0.355	-0.266	-0.190	1
0.899	6.572	-0.140	-0.227	-0.822	-0.542	-0.390	-0.283	-0.202	ŧ
0.897	9226	121 0-	-0.215	998 0-	0690	-0.435	0.315	81.0	

Table 15. Concluded

(d) Force data

C_D	0.2980	0.0808	0.0823	0.0791	0.0863	0.0999	0.1209	0.0640	0.1761	0.1656	0.1360	0.0917	0.3261	0.3360	0.2539	0.2159	0.1925	0.2226	0.1910	0.1877	0.2113	
a, deg	0.002	0.005	-2.990	0.035	3.003	6.007	9.020	0.020	-0.018	0.000	-0.020	-0.035	-2.991	2.974	0.012	-0.086	-0.131	-3.040	0.085	2.836	6.572	
M	1.251	0.600	0.601	0.603	0.600	0.601	0.601	0.402	0.874	0.851	0.800	0.702	1.200	1.200	0.952	0.927	0.901	0.903	0.905	0.898	0.899	

Table 16. Pressure and Force Data for Nozzle 10 With $\beta_{t,top/bot} = 17.3^{\circ}/\beta_{t,side} = 9.7^{\circ}$, Plume On, and $\alpha = 0^{\circ}$

(a) Static pressure coefficients on nozzle top flap

	_	$\overline{}$	_	_	T .	_	~	_	_	_	_	_	_	_	_	_
	.926	0.222	0.202	0.071	-0.076	-0.089	-0.112	-0.114	-0.092	-0.053	-0.023	0.011	0.061	0.196	0.218	0.212
	.853	0.196	0.182	0.041	-0.096	-0.113	-0.135	-0.141	-0.123	-0.089	-0.061	-0.027	0.027	0.175	0.189	0.182
	977.	0.158	0.153	0.008	-0.113	-0.127	-0.153	-0.161	-0.145	-0.113	-0.088	-0.055	-0.005	0.148	0.157	0.147
ine	.705	0.115	0.116	-0.025	-0.126	-0.142	-0.166	-0.173	-0.162	-0.134	-0.111	-0.081	-0.034	0.115	0.114	0.103
Static pressure coefficients on nozzle top flap at centerline with values of x/l of—	.632	0.065	0.073	-0.056	-0.138	-0.153	-0.182	-0.191	-0.179	-0.158	-0.140	-0.115	-0.067	0.071	0.065	0.056
efficients on nozzle top f with values of x/l of—	.558	0.001	0.014	-0.096	-0.174	-0.180	-0.204	-0.210	-0.195	-0.179	-0.166	-0.144	-0.106	0.012	0.001	-0.005
oefficients or with values	.484	-0.083	890'0-	-0.142	-0.444	-0.450	-0.402	-0.237	-0.216	-0.203	-0.193	-0.183	-0.151	-0.069	-0.083	-0.083
tic pressure c	114.	-0.213	-0.199	-0.206	-0.488	-0.526	-0.585	-0.283	-0.249	-0.231	-0.226	-0.225	-0.212	-0.201	-0.213	-0.204
Sta	.337	-0.514	-0.533	-0.336	-0.512	-0.560	-0.617	-0.417	-0.344	-0.301	-0.289	-0.299	-0.319	-0.526	-0.512	-0.461
	.300	-1.012	-1.349	-0.831	-0.387	-0.426	-0.487	-0.722	-0.674	-0.645	-0.639	-0.670	-0.785	-1.308	-1.004	-0.826
	.226	-0.441	-0.436	-0.328	-0.006	-0.019	-0.043	-0.161	-0.189	-0.222	-0.248	-0.276	-0.326	-0.438	-0.442	-0.400
	.153	-0.285	-0.280	-0.217	0.005	0.000	-0.024	-0.095	-0.118	-0.145	-0.163	-0.181	-0.214	-0.279	-0.284	-0.264
	M∞	0.598	0.700	0.797	1.249	1.202	1.149	0.951	0.930	0.900	0.876	0.850	0.803	0.700	0.600	0.402

	$\overline{}$	Т	_	_	Т	_	_	_	т-	_	Т	1	_	_	_	_
	.926	0.224	0.204	0.072	-0.076	-0.088	-0113	9,114	-0.093	20.056	-0.027	0.011	0.060	0.200	0.218	0.214
	.853	0.194	0.180	0.037	-0.096	-0.109	-0.135	-0.143	-0.124	6800	-0.061	-0.024	0.029	0.177	0.190	0.185
0.25	<i>6LL</i> :	0.156	0.152	9000	-0.111	-0.125	-0.151	-0.162	-0.146	-0.114	-0.088	-0.056	-0.001	0.150	0.155	0.147
flap at y/Y =	.705	0.112	0.115	-0.024	-0.127	-0.144	-0.167	-0.178	-0.165	-0.140	-0.114	-0.089	-0.033	0.114	0.111	0.103
Static pressure coefficients on nozzle top flap at $y/Y = 0.25$ with values of x/l of—	.558	-0.002	0.009	-0.102	-0.198	-0.187	-0.211	-0.212	-0.196	-0.181	-0.167	-0.148	-0.101	0.012	0.002	-0.003
oefficients o	.411	-0.209	-0.198	-0.217	-0.483	-0.521	-0.584	-0.286	-0.250	-0.235	-0.233	-0.230	-0.214	-0.195	-0.206	-0.198
tic pressure	.337	-0.502	-0.522	-0.347	-0.507	-0.558	-0.621	-0.417	-0.342	-0.307	-0.302	-0.309	-0.345	-0.520	-0.501	-0.450
Sta	.300	-1.006	-1.341	-0.844	-0.384	-0.423	-0.480	-0.720	-0.673	-0.655	-0.664	-0.687	-0.818	-1.303	-0.996	-0.825
	.226	-0.434	-0.429	-0.325	-0.004	-0.014	-0.042	-0.159	-0.187	-0.220	-0.246	-0.274	-0.321	-0.431	-0.434	-0.389
	.153	-0.276	-0.270	-0.211	9000	0.005	-0.019	-0.090	-0.113	-0.141	-0.159	-0.177	-0.207	-0.269	-0.274	-0.252
	M∞	0.598	0.700	0.797	1.249	1.202	1.149	0.951	0.930	0.900	0.876	0.850	0.803	0.700	0.600	0.402

Table 16. Continued

(a) Concluded

			Ctat	i presente	Static pressure coefficients on nozzle ton flan at $v/Y = 0.50$	nozzle ton t	Tan at $v/Y = v$	0.50		
			5	A Amesand an	with values	with values of x/l of—				
M	.153	.226	.300	.337	.411	.558	.705	6/1.	.853	.926
0.598	-0.251	-0.394	-0.955	-0.473	-0.196	-0.004	0.103	0.144	0.186	0.221
0.700	-0.252	-0.396	-1.270	-0.491	-0.190	900'0	0.109	0.144	0.178	0.206
0.797	-0.204	-0.309	-0.896	-0.404	-0.226	-0.091	-0.016	0.012	0.046	0.083
1 249	0.005	-0.003	-0.385	-0.513	-0.445	-0.297	-0.119	-0.107	-0.091	-0.068
1 202	0.003	-0.012	-0.427	-0.562	-0.485	-0.241	-0.136	-0.122	-0.108	-0.085
1 149	-0.025	-0.042	-0.487	-0.628	-0.540	-0.233	-0.162	-0.147	-0.130	-0.105
0.951	1000	-0.153	-0.739	-0.450	-0.300	-0.213	-0.180	-0.164	-0.147	-0.119
0630	-0 114	-0.181	-0.701	-0.376	-0.265	-0.198	-0.168	-0.147	-0.127	-0.096
0000	-0.139	-0.215	-0.675	-0.334	-0.247	-0.183	-0.139	-0.114	-0.089	-0.055
0.876	-0.155	-0.240	-0.688	-0.333	-0.248	-0.169	-0.117	-0.088	-0.060	-0.024
0.850	-0.173	-0.268	-0.721	-0.344	-0.245	-0.148	-0.089	-0.053	-0.024	0.015
0.803	-0.202	-0.309	-0.859	-0.389	-0.225	-0.096	-0.026	0.002	0.035	0.070
0.700	-0.251	-0.401	-1.240	-0.487	-0.189	0.007	0.107	0.144	0.173	0.200
0090	-0.252	-0.397	-0.952	-0.471	-0.195	-0.003	0.103	0.144	0.183	0.215
0.402	-0.232	-0.359	-0.787	-0.421	-0.181	-0.003	0.095	0.134	0.176	0.210

	T	Т	7	_[Т	7	٦	7	Ţ		П	\neg	\neg	1		7	٦
	3	.926	0.198	0.194	0.109	-0.047	-0.063	-0.074	-0.107	-0.078	-0.033	0.003	0.040	0.097	0.188	0.191	0.185
		.853	0.159	0.160	0.068	-0.085	-0.096	-0.110	-0.135	-0.111	690.0-	-0.037	0.002	0.057	0.157	0.157	0.148
0.75		.779	0.119	0.123	0.032	-0.118	-0.123	-0.142	-0.157	-0.139	-0.102	-0.072	-0.034	0.023	0.122	0.117	0.109
$lap\ at\ y/Y = 0$.705	0.074	0.082	0.002	-0.160	-0.154	-0.166	-0.173	-0.162	-0.127	-0.100	-0.065	900'0-	080'0	0.074	0.064
nozzle top f	IO 1/X IO	.558	-0.039	-0.029	-0.069	-0.329	-0.355	-0.376	-0.211	-0.201	-0.181	-0.160	-0.130	-0.076	-0.029	-0.039	-0.037
pefficients or	with values of x/i of—	.411	-0.211	-0.214	-0.192	-0.387	-0.424	-0.481	-0.299	-0.273	-0.262	-0.259	-0.239	-0.194	-0.215	-0.210	-0.191
Static pressure coefficients on nozzle top flap at $y/Y = 0.75$.337	-0.444	-0.480	-0.468	-0.435	-0.475	-0.539	-0.684	-0.554	-0.459	-0.443	-0.447	-0.463	-0.478	-0.442	-0.391
Stat		.300	-0.749	-0.906	-0.918	-0.265	-0.300	-0.353	-0.602	-0.646	-0.704	-0.751	-0.806	-0.907	-0.898	-0.748	-0.631
		.226	-0.321	-0,340	-0.295	-0.003	-0.012	-0.045	-0.147	-0.174	-0.206	-0.229	-0.253	-0.293	-0.339	-0.321	-0.287
		.153	-0.212	-0.219	-0.192	0.005	0.003	-0.027	-0.088	111	-0.136	-0.151	-0.168	-0.192	-0.221	-0.211	-0.191
		M	0.598	0.700	0.797	1.249	1 202	1.149	0.951	0.630	0060	0.876	0.850	0.803	0 700	0090	0.402

Table 16. Continued

(b) Static pressure coefficients on nozzle sidewall

	.926	0.179	0.183	960.0	0.042	0.04	0.058	\$600	0.073	0031	0.00	0.033	0.087	0.178	0 176	0.164
	.853	0.124	0.136	090.0	+	Ť.	r	0110	f	Ť	H	0.003	0.052	0.131	0.120	0.107
idewall	179	0.071	0.084	0.028	-0.221		-0.193	-0.124	H	Ť	-	-0.021	0.021	0.080	-	
flap and s	_	H	\vdash	-	H	Ė	Ė	H	H	╁	F.	Ė		H	H	├
ozzle top -	705	0.024	0.035	-0.002	-0.280	-0.272	-0.260	-0.140	-0.119	0.088	-0.066	0.041	-0.005	0.036	0.023	0.016
s on corner between no with values of x/l of—	.558	-0.062	-0.058	-0.065	-0.273	-0.304	-0.330	-0.185	-0.167	-0.132	-0.109	-0.088	-0.067	-0.057	-0.061	-0.054
ints on come with value	114.	-0.196	-0.206	-0.183	-0.324	-0.356	-0.409	-0.355	-0.287	-0.252	-0.224	-0.189	-0.181	-0.205	-0.196	-0.175
Static pressure coefficients on corner between nozzle top flap and sidewall with values of x/l of—	.337	-0.374	-0.409	-0.430	-0.371	-0.409	-0.468	-0.735	-0.747	-0.728	602.0-	-0.651	-0.443	-0.409	-0.373	-0.326
Static pres	300	-0.659	-0.777	-0.954	-0.287	-0.318	-0.378	-0.629	-0.672	-0.736	-0.786	-0.843	-0.941	-0.770	-0.653	-0.556
	.226	-		1	ı	I	1	1	_	ı	-		I	_	-	1
	.153	-0.201	-0.212	-0.193	0.005	0.001	-0.031	-0.090	-0.112	-0.136	-0.151	-0.166	-0.193	-0.212	-0.202	-0.183
	M_{∞}	0.598	0.700	0.797	1.249	1.202	1.149	0.951	0.930	0.900	0.876	0.850	0.803	0.700	0.600	0.402

			Sta	tic pressure	Static pressure coefficients on nozzle sidewall at z/7 = 0.50	opis elzzon (- 7/7 to Hew	0.50		
					with values	with values of x/l of—	waii al 2/2 =	00		
M∞	.153	.226	300	.337	.411	.558	.705	677.	.853	926
0.598	-0.192	-0.282	-0.529	-0.317	-0.178		0.005	0.067	0.118	071.0
0.700	-0.202	-0.307	-0.614	-0.351	-0.190		0.033	0.075	0.176	0.175
0.797	-0.188	-0.295	-0.935	-0.371	-0.182	1	0.003	0.032	0.072	0.116
1.249	0.007	-0.003	-0.299	-0.317	-0.299	1	-0.247	-0.238	-0.174	-0.045
1.202	-0.003	-0.017	-0.335	-0.351	-0.329	-	-0.272	-0.234	-0.132	562
1.149	-0.036	-0.056	-0.392	-0.409	-0.382	ŀ	-0.273	-0.226	-0.133	D 054
0.951	-0.094	-0.153	-0.645	-0.654	-0.499	 	9 113	-0.008	-0.073	600
0.930	-0.116	-0.179	-0.688	-0.697	-0.390	1	100 9	2000	0.053	
006:0	-0.138	-0.209	-0.749	-0.747	-0.274		8900	0.07	0.00	0.020
0.876	-0.154	-0.232	-0.799	-0.773	-0.211		0.000	200	0.021	0.010
0.850	-0.171	-0.255	-0.854	-0.711	-0.173		9200	-0.003	0.002	2200
0.803	-0.191	-0.295	-0.924	-0.379	-0.182		0000	0.032	0.000	0.113
0.700	-0.207	-0.308	-0.609	-0.349	-0.189		0.033	0.077	0.00%	0.174
0.600	-0.195	-0.284	-0.525	-0.317	-0.178	1	0.025	0.066	0.117	0.167
0.402	-0.174	-0.250	-0.449	-0.275	-0.158		0.023	0.059	0 106	0.158

Table 16. Continued (b) Concluded

				Σïς	itic pressure (coefficients of	efficients on nozzle sidev	Static pressure coefficients on nozzle sidewall at centerline $\frac{1}{2}$	line			į
2	153	326	300	337	411	.484	.558	.632	.705	<i>6LL</i> :	.853	.926
8 20	21.0	7900	0370	0.785	-0 164	660 0	-0.044	-0.009	0.031	0.070	0.116	1
0.298	-0.100	-0.204	0.578	0.215	-0.177	-0.103	-0.042	-0.005	0.038	0.078	0.124	ı
0.700	-0.198	0.510	0.520	0.340	221.0	-0.107	-0.052	-0.023	0.012	0.042	0.078	ι
16/.0	-0.189	-0.503	0.351	0.273	-0.779	-0.265	-0.245	-0.239	-0.230	-0.235	-0.184	ı
1.249	0.013	0.002	1000	0.356	0 308	10,00	-0.275	-0.265	-0.259	-0.248	-0.138	_
1.202	0.002	410.0	-0.394	0.330	0.361	0 333	-0.291	-0.277	-0.268	-0.241	-0.135	1
1.149	-0.036	-0.054		0.412	0.50	700.0	0 140	-0 105	-0.089	-0.072	-0.053	1
0.951	-0.090	10.151	-0.729	C+0.0-	1000	70.57	È i	2000	0.000	0300	0.038	
0.030	-0 112	-0.177	-0.775	-0.687	-0.487	-0.182	-0.104	-0.0/8	-0.0/2	-0.030	10.030	
0000	0 136	0000	0.844	D 744	-0.308	-0.119	-0.077	-0.064	-0.052	-0.033	-0.008	1
0.900	-0.133	-0.203	000	0 773	0.217	101	0200	-0.054	-0.037	-0.014	0.016	ı
0.876	-0.151	-0.232	-0.039		12.0		0.065	0000	8109	0000	0.043	1
0.850	-0.167	-0.256	-0.960	-0.662	-0.1/1	-0.099	C00.7	25.0	0100	2000	3500	
0.803	70107	-0.298	-0.933	-0.347	-0.178	-0.108	-0.057	-0.024	0.008	0.037	0.0/3	1
200.0	0000	0.307	865 0	-0.315	-0.179	-0.102	-0.045	-0.004	0.037	0.079	0.125	i
30.00	0.200	186.0	0.0461	-0.284	-0.166	-0.100	-0.048	-0.007	0.031	0.070	0.118	'
0.000	021.0	0.50	200	0.357	0.143	080	140	-0.008	0.027	0.065	0.107	1
0.402	89.7	-0.749	34.7	10.4.0	-	1000	210					

		Stati	c pressure co	Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$	nozzle sidew	/all at z/Z = -	0.50	
				WILLI VALUES	10 177 10			200
M	.153	.226	300	.337	.411	.558	.705	976.
3	-0 194	-0.281	-0.515	-0.301	1	-0.055	0.027	0.172
0 700	-0.208	-0.307	-0.599	-0.335	1	-0.054	0.034	0.180
0.707	-0.196	-0.295	-0.961	-0.369	1	-0.063	0.010	0.133
1 240	0.013	-0.002	-0.318	-0.315	1	-0.256	-0.251	-0.042
1 202	10.004	-0.021	-0.355	-0.351	1	-0.286	-0.278	-0.039
1 140	-0.038	-0.055	-0.414	-0.407	1	-0.304	-0.288	-0.049
0.951	060 0-	-0.152	-0.668	-0.644	1	-0.156	-0.090	-0.027
0.030	0110	-0.178	-0.712	-0.687	1	-0.120	-0.074	-0.010
0000	5 133	-0.210	-0.773	-0.743		-0.094	-0.055	0.033
9280	-0.148	-0.234	-0.823	-0.776		-0.081	-0.038	0.058
0.850	-0 163	-0.259	-0.880	-0.731		-0.071	-0.016	0.086
0.803	190	-0.297	-0.953	-0.379	i	-0.063	0.009	0.125
002.0	20,01	-0.308	-0.595	-0.335	1	-0.053	0.038	0.176
0090	-0.189	-0.284	-0.514	-0.303	1	-0.055	0.029	0.170
0402	20 168	-0.251	-0.444	-0.260	ì	-0.052	0.022	0.159

Table 16. Continued

(c) Static pressure coefficients on nozzle bottom flap

			Static	pressure co	Static pressure coefficients on nozzle bottom flap at $y/Y = 0.75$	nozzle bottor	m flap at y/Y	= 0.75		
					with value	with values of x/l of—				
M_{∞}	.153	.226	.300	.337	.411	.558	.705	622	.853	.926
0.598	-0.210	-0.316	1	-0.431	-0.201	-0.034	0.074	0.119	0.162	0.197
0.700	-0.220	-0.338	-	_0.468	-0.207	-0.027	0.083	0.126	0.166	0.196
0.797	-0.196	-0.298	-	-0.555	-0.209	-0.054	0.037	0.071	0.105	0.136
1.249	0.011	-0.004	1	-0.439	-0.392	-0.334	-0.197	-0.118	<i>-</i> 0.077	-0.044
1.202	-0.007	-0.022	-	-0.483	-0.429	-0.368	-0.175	-0.120	980'0-	-0.054
1.149	-0.038	-0.056	-	-0.545	-0.484	-0.406	-0.176	-0.131	-0.095	-0.059
0.951	-0.093	-0.154		-0.778	-0.360	-0.215	-0.147	-0.116	880'0-	-0.056
0.930	-0.115	-0.181	1	-0.659	-0.298	-0.204	-0.141	-0.109	8/0.0-	-0.045
0.900	-0.140	-0.211	J	-0.561	-0.283	-0.178	-0.104	-0.071	-0.036	0.000
0.876	-0.154	-0.233	-	-0.536	-0.273	-0.153	-0.071	-0.037	-0.001	0.036
0.850	-0.170	-0.257	-	-0.531	-0.250	-0.118	-0.033	0.003	9:00	0.072
0.803	-0.195	-0.298	-	-0.551	-0.215	-0.064	0.029	0.067	0.097	0.128
0.700	-0.219	-0.338	t	-0.464	-0.206	-0.028	0.083	0.127	0.163	0.194
0.600	-0.209	-0.317	1	-0.430	-0.201	-0.036	0.074	0.120	851.0	0.195
0.402	-0.192	-0.283	1	-0.382	-0.184	-0.038	0.069	0.112	0.150	0.189

	,	_				_										
	.926	0.216	0.212	0.125	-0.052	-0.066	-0.075	-0.064	-0.060	-0.017	0.019	0.053	0.115	0.207	0.211	0.205
	.853	0.184	0.182	0.095	-0.077	-0.087	-0.105	-0.093	680'0-	-0.048	-0.015	0.022	880.0	0.180	0.181	0.173
= 0.50	622.	0.144	0.148	0.065	-0.100	-0.115	-0.131	-0.128	-0.121	-0.084	-0.053	-0.013	0.057	0.145	0.143	0.135
n flap at y/Y	.705	0.099	0.105	0.030	-0.130	-0.139	-0.162	-0.159	-0.150	-0.117	-0.087	-0.050	0.020	0.104	0.097	0.091
icients on nozzle botton	.558	-0.010	-0.002	-0.072	-0.387	-0.369	-0.321	-0.240	-0.214	-0.195	-0.175	-0.149	-0.082	-0.002	-0.012	-0.014
fficients on 1	.411	-0.195	-0.194	-0.269	-0.456	-0.497	-0.553	-0.357	-0.295	-0.280	-0.278	-0.277	-0.270	-0.190	161.0-	-0.180
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.50$.337	-0.460	-0.483	-0.483	-0.510	-0.560	-0.621	-0.567	-0.415	-0.375	-0.375	-0.385	-0.470	-0.477	-0.457	-0.411
Static	300	-0.918	-1.177	-0.981	-0.381	-0.421	-0.482	_0.746	0.724	-0.716	-0.733	-0.772	-0.932	1.142	-0.910	-0.764
	.226	1	***	+	t		-		-	-	-	_	_	_		
	.153	-0.247	-0.251	-0.210	0.010	-0.005	-0.035	-0.098	-0.120	-0.144	-0.161	-0.178	-0.207	-0.252	-0.248	-0.225
	M∞	0.598	0.700	0.797	1.249	1.202	1.149	0.951	0.930	0.900	0.876	0.850	0.803	0.700	0.600	0.402

Table 16. Concluded

(c) Concluded

(d) Force data

Table 17. Pressure and Force Data for Nozzle 10 With $\beta_{t,top/bot} = 17.3^{\circ}/\beta_{t,side} = 9.7^{\circ}$ and Plume Off

(a) Static pressure coefficients on nozzle top flap

	1																		
.926	-0.107	-0.090	-0.059	-0.085	-0.063	-0.045	-0.024	-0.009	-0.036	-0.003	0.047	0.176	0.179	0.161	0.178	0.178	0.171	0.155	0 169
.853	-0.127	-0.112	-0.087	-0.115	-0.090	-0.075	-0.065	-0.055	-0.065	-0.034	0.019	0.149	0.147	0.120	0.146	0.147	0.139	0.119	0.138
<i>6LL</i> :	-0.139	-0.126	-0.105	-0.134	-0.108	-0.104	-0.108	-0.103	-0.088	-0.061	9000	0.117	0.113	0.078	0.110	0.117	0.109	0.087	0.101
.705	-0.150	-0.138	-0.122	-0.148	-0.124	-0.132	-0.149	-0.153	-0.109	-0.089	-0.034	0.080	0.071	0.032	0.067	0.081	0.074	0.052	0.056
.632	-0.158	-0.150	-0.140	-0.166	-0.145	-0.156	-0.189	-0.203	-0.132	-0.115	-0.064	0.034	0.025	-0.017	0.023	0.041	0.038	0.017	0.018
.558	-0.175	-0.165	-0.160	-0.185	-0.162	-0.178	-0.226	-0.250	-0.154	-0.143	-0.100	-0.024	-0.035	-0.078	-0.038	-0.014	-0.013	-0.033	-0.039
.484	-0.197	-0.182	-0.182	-0.209	-0.184	-0.200	-0.257	-0.292	-0.179	-0.173	-0.143	-0.108	-0.115	-0.162	-0.118	-0.086	-0.083	-0.100	-0.115
.411	-0.239	-0.212	-0.208	-0.243	-0.214	-0.223	-0.288	-0.337	-0.208	-0.207	-0.199	-0.241	-0.242	-0.293	-0.244	-0.207	-0.199	-0.217	-0.233
.337	-0.342	-0.283	-0.268	-0.317	-0.273	-0.287	-0.366	-0.438	-0.264	-0.272	-0.309	-0.591	-0.540	-0.611	-0.546	-0.489	-0.474	-0.500	-0.492
.300	-0.658	-0.610	-0.599	-0.660	-0.601	-0.620	-0.708	-0.780	-0.604	-0.630	-0.771	-1.372	-1.049	-1.190	-1.059	-0.961	-0.928	-0.980	-0.871
.226	-0.157	-0.188	-0.220	-0.203	-0.221	-0.231	-0.238	-0.234	-0.245	-0.276	-0.327	-0.450	-0.461	-0.492	-0.463	-0.430	-0.410	-0.408	-0.418
.153	-0.091	-0.118	-0.141	-0.127	-0.142	-0.151	-0.158	-0.160	-0.160	-0.182	-0.214	-0.288	-0.294	-0.311	-0.298	-0.277	-0.263	-0.257	-0.278
α, deg	-0.161	-0.125	-0.117	-3.120	-0.100	2.877	5.817	8.873	-0.145	-0.145	-0.144	-0.132	-0.139	-3.125	-0.141	2.842	5.868	8.847	-0.151
M _∞	0.952	0.927	0.899	0.900	0.899	0.900	0.900	0.899	0.877	0.847	0.800	0.698	0.602	0.600	0.602	0.602	0.601	0.602	0.401
	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.167 -0.167 -0.167 -0.157 -0.139 -0.139 -0.127	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.161 -0.157 -0.658 -0.342 -0.239 -0.197 -0.175 -0.158 -0.139 -0.139 -0.127 -0.125 -0.118 -0.188 -0.610 -0.283 -0.212 -0.182 -0.165 -0.138 -0.126 -0.112	a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.161 -0.091 -0.157 -0.658 -0.239 -0.197 -0.175 -0.158 -0.139 -0.139 -0.127 -0.125 -0.118 -0.610 -0.283 -0.212 -0.182 -0.165 -0.138 -0.126 -0.112 -0.117 -0.141 -0.220 -0.599 -0.208 -0.182 -0.160 -0.140 -0.122 -0.187 -0.160 -0.105	a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.161 -0.091 -0.157 -0.342 -0.239 -0.197 -0.175 -0.158 -0.139 -0.139 -0.127 -0.125 -0.118 -0.610 -0.283 -0.212 -0.165 -0.150 -0.138 -0.126 -0.112 -0.117 -0.141 -0.220 -0.268 -0.208 -0.182 -0.160 -0.122 -0.105	a. deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.161 -0.091 -0.157 -0.342 -0.139 -0.197 -0.156 -0.150 -0.139 -0.137 -0.125 -0.118 -0.188 -0.610 -0.283 -0.212 -0.165 -0.150 -0.138 -0.126 -0.117 -0.141 -0.220 -0.599 -0.268 -0.182 -0.160 -0.140 -0.122 -0.105 -3.120 -0.127 -0.203 -0.660 -0.317 -0.209 -0.185 -0.166 -0.148 -0.134 -0.115 -0.100 -0.142 -0.221 -0.273 -0.214 -0.184 -0.165 -0.145 -0.134 -0.199	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.342 -0.239 -0.197 -0.175 -0.158 -0.139 -0.139 -0.127 -0.125 -0.118 -0.610 -0.283 -0.212 -0.165 -0.150 -0.138 -0.126 -0.112 -0.117 -0.141 -0.220 -0.599 -0.208 -0.182 -0.160 -0.142 -0.105	a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.239 -0.197 -0.158 -0.150 -0.139 -0.127 -0.125 -0.118 -0.181 -0.283 -0.212 -0.182 -0.165 -0.150 -0.138 -0.127 -0.117 -0.141 -0.220 -0.288 -0.208 -0.182 -0.160 -0.132 -0.105 -3.120 -0.127 -0.203 -0.269 -0.243 -0.209 -0.185 -0.166 -0.105 -0.105 -0.100 -0.127 -0.203 -0.203 -0.214 -0.184 -0.164 -0.148 -0.134 -0.115 -0.100 -0.151 -0.221 -0.213 -0.214 -0.184 -0.145 -0.108 -0.109 -0.151 -0.231 -0.223 -0.200 -0.178 -0.145 -0.104 -0.104 -0.104 <	α, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.342 -0.239 -0.197 -0.158 -0.150 -0.139 -0.127 -0.125 -0.118 -0.188 -0.610 -0.283 -0.212 -0.165 -0.150 -0.138 -0.127 -0.117 -0.141 -0.220 -0.599 -0.268 -0.209 -0.182 -0.160 -0.122 -0.105 -3.120 -0.127 -0.203 -0.660 -0.317 -0.209 -0.185 -0.166 -0.148 -0.134 -0.115 -0.100 -0.142 -0.221 -0.601 -0.214 -0.214 -0.165 -0.145 -0.104 -0.108 -0.108 2.877 -0.151 -0.231 -0.287 -0.223 -0.257 -0.156 -0.149 -0.104 -0.104 5.817 -0.158 -0.234 -0.288 -0.257	a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.239 -0.197 -0.158 -0.150 -0.139 -0.127 -0.125 -0.118 -0.610 -0.283 -0.212 -0.182 -0.160 -0.138 -0.126 -0.116 -0.138 -0.126 -0.117 -0.150 -0.136 -0.117 -0.140 -0.127 -0.105	a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.239 -0.197 -0.158 -0.150 -0.139 -0.137 -0.125 -0.118 -0.168 -0.243 -0.212 -0.165 -0.150 -0.138 -0.126 -0.187 -0.160 -0.138 -0.127 -0.187 -0.160 -0.138 -0.169 -0.109 -0.127 -0.160 -0.189 -0.160 -0.189 -0.189 -0.160 -0.134 -0.187 -0.160 -0.134 -0.184 -0.160 -0.148 -0.105	a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.239 -0.197 -0.158 -0.150 -0.139 -0.137 -0.139 -0.127 -0.125 -0.18 -0.610 -0.239 -0.212 -0.165 -0.150 -0.138 -0.126 -0.137 -0.150 -0.138 -0.127 -0.127 -0.127 -0.127 -0.127 -0.127 -0.127 -0.127 -0.127 -0.127 -0.124 -0.124 -0.124 -0.134 -0.134 -0.145 -0.148 -0.145 -0.148 -0.145 -0.124 -0.134 -0.145 -0.124 -0.104 -0.148 -0.145 -0.124 -0.104 -0.124 -0.108 -0.144 -0.154 -0.124 -0.104 -0.124 -0.108 -0.144 -0.154 -0.124 -0.104 -0.144 -0.154 -0.144 -0.154 -0.145 -0.144 -0.154	a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.239 -0.197 -0.156 -0.150 -0.139 -0.127 -0.125 -0.118 -0.158 -0.150 -0.150 -0.138 -0.126 -0.137 -0.127 -0.127 -0.127 -0.182 -0.160 -0.148 -0.126 -0.182 -0.160 -0.148 -0.105 -0.105 -0.105 -0.117 -0.142 -0.122 -0.182 -0.160 -0.148 -0.132 -0.105 -0.105 -0.148 -0.118	a, deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.239 -0.197 -0.158 -0.150 -0.139 -0.127 -0.155 -0.118 -0.188 -0.610 -0.283 -0.212 -0.182 -0.165 -0.138 -0.126 -0.139 -0.127 -0.117 -0.141 -0.220 -0.589 -0.268 -0.203 -0.160 -0.122 -0.160 -0.122 -0.160 -0.122 -0.160 -0.122 -0.105 -0.160 -0.122 -0.105 -0.160 -0.122 -0.105 -0.149 -0.142 -0.122 -0.105 -0.145 -0.145 -0.145 -0.145 -0.145 -0.145 -0.145 -0.145 -0.145 -0.145 -0.145 -0.145 -0.144 -0.182 -0.124 -0.184 -0.125 -0.124 -0.184 -0.126 -0.124 -0.124 -0.126 -0.124	α , deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.239 -0.197 -0.175 -0.158 -0.130 -0.127 -0.125 -0.118 -0.157 -0.610 -0.283 -0.212 -0.185 -0.150 -0.138 -0.126 -0.112 -0.117 -0.141 -0.220 -0.589 -0.268 -0.209 -0.185 -0.160 -0.130 -0.136 -0.136 -0.136 -0.136 -0.136 -0.136 -0.136 -0.136 -0.136 -0.136 -0.137 -0.140 -0.122 -0.105 -0.148 -0.148 -0.148 -0.148 -0.148 -0.148 -0.149 -0.148 -0.148 -0.148 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149 -0.149	α , deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.342 -0.197 -0.175 -0.150 -0.139 -0.127 -0.125 -0.118 -0.188 -0.610 -0.229 -0.182 -0.150 -0.138 -0.126 -0.139 -0.127 -0.117 -0.141 -0.220 -0.288 -0.208 -0.182 -0.160 -0.148 -0.127 -0.149 -0.129 -0.129 -0.148 -0.129 -0.148 -0.129 -0.148 -0.129 -0.148 -0.129 -0.148 -0.129 -0.129 -0.148 -0.148 -0.129 -0.129 -0.148 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129 -0.129	α , deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.342 -0.197 -0.156 -0.150 -0.199 -0.159 -0.127 -0.159 -0.127 -0.159 -0.127 -0.159 -0.127 -0.159 -0.127 -0.165 -0.120 -0.139 -0.127 -0.127 -0.127 -0.127 -0.127 -0.127 -0.127 -0.127 -0.127 -0.127 -0.223 -0.260 -0.214 -0.125 -0.127	α , deg .153 .226 .300 .337 .411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.688 -0.232 -0.197 -0.175 -0.150 -0.139 -0.127 -0.125 -0.191 -0.184 -0.160 -0.283 -0.212 -0.182 -0.160 -0.139 -0.127 -0.117 -0.141 -0.220 -0.202 -0.182 -0.160 -0.134 -0.136 -0.105 -0.117 -0.141 -0.220 -0.243 -0.243 -0.244 -0.185 -0.166 -0.148 -0.134 -0.115 -0.100 -0.127 -0.223 -0.243 -0.243 -0.224 -0.226 -0.185 -0.149 -0.165 -0.199 -0.145 -0.189 -0.189 -0.149 -0.165 -0.189 -0.149 -0.165 -0.199 -0.149 -0.149 -0.169 -0.148 -0.166 -0.148 -0.166 -0.148 -0.116 -0.	α , deg .153 .226 .300 .337 411 .484 .558 .632 .705 .779 .853 -0.161 -0.091 -0.157 -0.658 -0.342 -0.197 -0.156 -0.139 -0.127 -0.120 -0.120 -0.139 -0.127 -0.127 -0.127 -0.127 -0.120

Table 17. Continued

(a) Continued

	_	-	_	_	-	_	_	_	1	т	Т		г	т	Т			Т	Т	Т			Ī	Т	٦
	926	-0.107	000	-0.088	-0.055	-0.081	-0.062	-0.043	0.004	20.0	-0.010	-0.033	1000		0.049	0.176	0.178	0.150		0.170	0.174	0.167	0.149	0 168	0.100
	.853	7,110	121.0	-0.10 9	-0.081	-0.110	-0.086	-0.077	0.067	10.00	-0.057	-0.062	500	CCO	0.022	0.148	0 145	0 117	100	0.142	0.145	0.135	0.113	0.123	0.1.0
.25	677.	0 140	21.0	-0.128	-0.106	-0.135	1119	801 9	1110	7:11	-0.109	-0.089	0.063	20.00	-0.006	0.114	0 111	0.077	0.077	0.109	0.116	0 108	0.085	00.0	0.100
ap at $y/Y = 0$	705	0310	201.70	-0.142	-0.127	-0.152	50100	0 136	25.5	-U.133	-0.159	-0.112	000	-0.09U	-0.035	0.076	0 060	0.00	0.031	0.067	0.079	0.073	0.00	0.049	0.060
Static pressure coefficients on nozzle top flap at $y/Y = 0.25$	558	0710	97:7	-0.168	-0.162	20 188	0.163	281.0	201.00	-0.231	-0.257	0510		-0.14 ₀	0.100	9000	0.024	-0.03#	-0.079	-0.039	-0.011	0.014	10.01	-0.034	-0.040
efficients on nozzle to	411	3000	-0.239	-0.212	-0.208	-0.245	6150	2000	-0.233	-0.302	-0.347	0.215	217.0	-0.216	-0.206	0 237	167.0	-0.234	-0.286	-0.237	000	0 103	0.133	-0.214	-0.227
pressure co	117	, C.C.	-0.347	-0.288	-0.275	0 331	2020	-0.203	203	-0.392	-0.448	0000	-0.202	-0.288	-0.329	1050	-0.30+	-0.531	-0.599	-0.533	0.481	101.0	-0.400	-0.491	-0.482
Static	300	ooc.	-0.659	-0.613	5090	0.00	6,0,7	-0.014	-0.638	-0.730	786	2070	-0.023	-0.657	790	1,266	-1.303	-1.045	-1.180	-1.051	0.062	-0.505	-0.931	-0.971	-0.863
	300	077	-0.154	-0.186	0.218	0.20	-0.201	-0.220	-0.228	-0.236	0 236	0.2.0	-0.244	-0.275	0.324	10.324	-0.443	-0.448	-0.478	J 450	0.110	-0.419	-0.398	-0.394	-0.408
	53.	cci.	-0.088		0 127	10.15/	-0.124	-0.139	-0.147	9510-	0 163	70.107	-0.157	-0.179	0000	-0.209	-0.280	-0.284	-0.300	0.787	0.50	-0.200	-0.251	-0.245	1920-
		α, deg	-0.161	3010	0.12	7110	-3.120	-0.100	2.877	5 817	0.073	8.8/3	-0.145	-0 145		-0.14 4	-0.132	-0.139	_3 125	1710	-0.141	2.842	5.868	8.847	1510
		M	0.952	0.007	0.927	0.899	0.600	0.899	0.600	0000	0.900	0.899	0.877	7780	0.047	0.800	0.698	0.602	0,600	200.0	0.007	0.602	0.601	0.602	0.401

Table 17. Continued

(a) Continued

-0.059-0.084-0.066 0.000 9.110 -0.0380.003 0.052 0.170 .926 -0.091 0.150 0.169 0.171 9.01 0.151 -0.130-0.113 -0.087-0.093 -0.072 -0.053 -0.062 0.114 -0.042.853 0.025 0.141 0.110 0.136 0.1200.102 0.124 0.137 -0.136 -0.143-0.113-0.106-0.099 -0.095 -0.061 0.106 977. -0.131 90.10 0.099 0.067 0.099 0.088 0.068 0.086 Static pressure coefficients on nozzle top flap at y/Y = 0.50-0.129 0.114 -0.152-0.146-0.136 -0.136-0.146 -0.150 0.066 -0.090.705 0.062 0.046 0.027 0.071 0.054 0.061 with values of x/l of--0.179 -0.166 -0.146 -0.096 -0.168-0.189 -0.232-0.255-0.034-0.171-0.072-0.036-0.014 .558 -0.161 -0.016-0.030-0.034-0.031-0.249 -0.261 -0.220 -0.266 -0.255-0.366 -0.230-0.231 -0.218 -0.224-0.221-0.332-0.222-0.172-0.182-0.206-0.1874. -0.536 -0.310 -0.300-0.370-0.308 -0.439-0.488 -0.315 -0.327 -0.367-0.380-0.341-0.563-0.438 -0.454.337 -0.498-0.447-0.431-0.636 -0.679-0.774 -0.635 -0.643-0.663-0.847 -0.699 -1.128 -0.995 -0.934 -0.905 -0.661 -0.991 -0.827-0.148 -0.214 -0.198 -0.218 -0.234 -0.235 -0.253 -0.182-0.314 -0.268 -0.406-0.431 -0.374 -0.375-0.407 -0.358-0.137 -0.185 -0.155 -0.086 -0.134 -0.122-0.163-0.175 -0.259 -0.272 -0.262 -0.245 -0.234 -0.245 0.113 -0.244.153 -0.261α, deg -0.125-0.161-3.120-0.1005.817 8.873 -0.145-0.145-0.144 -0.132-3.1252.842 5.868 2.877 -0.139-0.1418.847 -0.1510.899 0.900 0.900 0.952 0.927 0.800 \mathbf{z}_{8} 0.877 0.847 0.698 0.600 0.602 0.602 0.601

Table 17. Continued

(a) Concluded

				Ctof	i nrecente	Static pressure coefficients on nozzle top flap at $v/Y = 0.75$	nozzle ton	flap at $v/Y =$	0.75		
					a ameeand at	with values of x/l of-	—Jo //x Jo				
×	α. deg	.153	.226	.300	.337	.411	.558	.705	6 <i>LL</i> :	.853	.926
877	0.161	-0.083	-0 142	-0.592	-0.561	-0.259	-0.183	-0.152	-0.143	-0.131	-0.113
0.932	0.101	0110	-0.173	10.641	-0.435	-0.236	-0.176	-0.145	-0.129	-0.109	-0.092
0.927	0.12		0.00	0690	-0.403	-0.237	-0.167	-0.121	-0.100	-0.078	-0.057
0.099	3 130	124	-0.186	-0.681	-0.514	-0.282	-0.202	-0.152	-0.130	-0.108	-0.082
0.500	0.100	0.123	0.205	2690	-0.407	-0.239	-0.173	-0.127	-0.105	-0.083	-0.060
0.099	20.100	1510	0.235	669 0	-0.411	-0.251	-0.180	-0.117	-0.087	-0.054	-0.027
006.0	5 017	0 160	0.256	-0.703	-0.481	-0.312	-0.210	-0.106	-0.065	-0.028	-0.001
0.900	9.017	0.186	-0.271	-0.750	-0.513	-0.343	-0.219	-0.096	-0.047	-0.008	0.018
0.099	0.07	0.100	-0.227	-0.737	-0.412	-0.244	-0.156	-0.103	080'0-	-0.053	-0.029
0.07	0.145	0.147	-0.255	797 0-	-0.435	-0.235	-0.129	-0.069	-0.043	-0.016	0.008
0.047	14.1	0.10	0.205	8060	-0.462	-0.194	-0.074	-0.012	0.013	0.038	0.058
0.800	1.5	-0.132	0.257	0.050	0.511	-0.246	-0.063	0.043	0.083	0.119	0.148
0.698	-0.132	0.220	0.334	0.776	0.465	_0 233	890 0	0.035	0.075	0.112	0.146
0.602	2 195	0.227	0.348	0.770	5150	0.259	-0.095	0.00	0.050	0.091	0.130
0.000	-3.123	0.331	0.33	777.0	-0.467	-0.235	-0.071	0.034	0.073	0.111	0.145
0.002	70.141	0.221	0.334	-0.649	-0 404	-0.201	-0.042	0.048	0.081	0.108	0.132
0.007	2,042	0.210	0.302	9550	-0.357	-0.175	-0.038	0.034	0.062	0.093	0.123
0.001	5.000	0.224	0.304	0 \$69	-0.351	-0.171	-0.049	0.021	0.050	0.082	0.115
0.602	0.84/	-0.224	ا ا)			2200	0.030	0.065	0.102	0.135
0.401	-0.151	-0.199	-0.297	-0.656	-0.413	-0.212	-0.000	0.00	0,00	701.0	0.122

Table 17. Continued

(b) Static pressure coefficients on nozzle sidewall

				Static pres	sure coeffici	ents on come with value	is on comer between no with values of x/l of—	Static pressure coefficients on corner between nozzle top flap and sidewall with values of x/l of—	ind sidewall		
M	α, deg	.153	.226	300	.337	114.	.558	705.	677.	.853	.926
0.952	-0.161	-0.087	1	-0.623	-0.704	-0.283	-0.179	-0.159	-0.154	-0.147	-0.135
0.927	-0.125	-0.112	_	-0.675	-0.667	-0.248	-0.167	-0.132	6110	51.0	000 0
0.899	-0.117	-0.132	-	-0.732	-0.637	-0.239	-0.137	-0.096	-0.084	-0.065	0.051
0.900	-3.120	-0.133	ı	-0.722	-0.737	-0.286	-0.181	-0.133	120	0000	2800
0.899	-0.100	-0.135	ł	-0.734	-0.644	-0.241	-0.142	00100	0000	1200	0.057
0.900	2.877	-0.152	1	-0.754	-0.695	-0.248	-0.132	-0.091	-0.077	0.00	0.050
0.900	5.817	-0.174	ı	-0.776	-0.779	-0.297	-0.152	-0.105	0000	5,007	0.050
0.899	8.873	-0.192	1	-0.787	-0.724	-0.299	-0.153	-0.089	6900	000	0.030
0.877	-0.145	-0.151	1	-0.783	0.644	-0.226	5116	0000	-0.056	0000	0000
0.847	-0.145	-0.170		-0.847	-0.626	-0.193	0000	-0.044	8000	9000	1100
0.800	-0.144	-0.193	-	-0.949	-0.457	181	19067	0.007	0.020	0.000	110.0
0.698	-0.132	-0.221		-0.807	-0.435	-0.225	0.086	1000	0000	0.027	0000
0.602	-0.139	-0.210	1	-0.677	-0.391	-0.213	-0.084	-0.013	0.000	0.00	0.124
0.600	-3.125	-0.220	1	-0.756	-0.416	-0.222	880 9	9100	0.017	0.000	0.007
0.602	-0.141	-0.212	1	-0.680	-0.392	-0.215	-0.086	-0.015	0.001	0.00	0.067
0.602	2.842	-0.214	1	-0.625	-0.368	-0.209	-0.083	2000	0.048	0.000	0.112
0.601	5.868	-0.224	1	-0.583	-0.343	-0.195	1200	0.014	0.051	0.030	0.129
0.602	8.847	-0.231	ŀ	-0.512	-0.308	-0.175	70.062	0000	0.031	0.065	0.104
0.401	-0.151	-0.189	_	-0.578	-0.341	191	7200	0.000	7000	0.00	0.103

Table 17. Continued

(b) Continued

	\neg	7	П	_	1	П	٦		7		П			П	7	٦		П	П	_
	.926	-0.117	-0.068	-0.033	-0.065	-0.034	-0.020	-0.030	-0.025	-0.006	0.025	0.067	0.126	0.119	0.108	0.117	0.119	0.105	0.093	0.104
	.853	-0.139	-0.086	-0.050	-0.087	-0.053	-0.043	-0.067	-0.057	-0.025	0.003	0.041	0.079	0.072	0.067	0.070	0.076	0.057	0.039	0.062
).50	622.	-0.157	-0.103	-0.068	-0.107	690.0-	-0.068	-0.109	960:0-	-0.046	-0.021	0.013	0.035	0.029	0.028	0.026	0.027	0.007	-0.018	0.021
vall at $z/Z = 0$.705	-0.164	-0.116	-0.081	-0.120	-0.083	6/0'0-	-0.116	-0.111	090:0-	-0.040	-0.010	-0.001	-0.004	-0.004	900'0-	-0.010	-0.026	-0.044	-0.008
nozzle sidev of x/l of—	.558	ı	ı	ı	1	1	1	t	ı	1	-	ı		1	_	I	1	1	-	1
efficients on nozzle side with values of x/l of—	.411	-0.410	-0.323	-0.274	-0.330	-0.277	-0.293	-0.357	-0.328	-0.225	-0.182	-0.184	-0.207	-0.193	-0.198	-0.195	-0.198	-0.212	-0.220	-0.174
Static pressure coefficients on nozzle sidewall at $z/Z = 0.50$ with values of x/l of—	.337	-0.651	-0.695	-0.726	-0.765	-0.730	-0.762	-0.803	-0.839	-0.750	-0.703	-0.393	-0.367	-0.330	-0.345	-0.331	-0.329	-0.338	-0.340	-0.290
Stat	300	-0.640	-0.691	-0.748	-0.756	-0.747	-0.754	-0.774	-0.806	-0.796	-0.859	-0.937	-0.630	-0.545	-0.591	-0.548	-0.534	-0.536	-0.532	-0.466
ē	.226	-0.149	-0.180	-0.209	-0.205	-0.210	-0.226	-0.256	-0.293	-0.231	-0.258	-0.297	-0.319	-0.292	-0.307	-0.293	-0.295	-0.312	-0.332	-0.257
	.153	-0.089	-0.116	-0.137					-0.208	-0.153	-0.171	-0.195	-0.216	-0.201	-0.210	-0.199	-0.206	-0.223	-0.243	-0 178
	α, deg	-0.161	-0.125	-0.117	-3.120	0.100	2.877	5.817	8 873	-0.145	-0.145	-0 144	-0.132	-0.139	-3.125	-0.141	2.842	5.868	8.847	151 9
	M	0.952	0.927	0 899	0060	0.899	0060	0.900	080	0.877	0.847	0.800	869 0	0.602	0.600	0.602	0.602	0.601	0.602	0.401

Table 17. Continued

(b) Continued

	Т	Т	Т	Т	Т	T	Т	т	_	Т	Т	1	1	_	_	т-	_	Т	T	_
	.926	,	,	ı				,			,	,		1	1			,		
	.853	-0.120	-0.074	-0.043	-0.073	-0.042	-0.032	-0.050	-0.060	-0.021	9000	0.040	0.083	0.074	0.074	0.071	0.070	0.055	0.034	0.063
	<i>6LL</i> :	-0.135	-0.088	-0.061	-0.092	-0.062	-0.050	-0.072	-0.088	-0.039	-0.018	0.011	0.041	0.035	0.036	0.033	0.032	0.019	-0.005	0000
line	.705	-0.144	-0.093	-0.069	-0.102	-0.075	-0.066	-0.092	-0.114	-0.057	-0.041	-0.019	-0.001	0.004	0.005	0.004	0.001	-0.011	-0.032	0000
Static pressure coefficients on nozzle sidewall at centerline with values of x/l of—	.632	-0.168	-0.105	-0.078	-0.107	-0.080	-0.075	-0.10 4	-0.132	-0.068	-0.058	-0.043	-0.031	-0.031	-0.033	-0.032	-0.036	-0.051	-0.073	-0.030
efficients on nozzle side with values of x/l of—	.558	-0.214	-0.129	-0.093	-0.122	-0.096	-0.090	-0.124	-0.162	-0.083	-0.081	-0.076	-0.072	-0.064	-0.065	-0.064	-0.069	-0.082	-0.101	-0.054
coefficients o	.484	-0.334	-0.217	-0.146	-0.177	-0.147	-0.145	-0.191	-0.227	-0.118	-0.115	-0.123	-0.124	-0.115	-0.119	-0.117	-0.120	-0.133	-0.153	-0.102
itic pressure	.411	-0.535	-0.486	-0.359	-0.419	-0.364	-0.401	-0.514	-0.532	-0.256	-0.193	-0.190	-0.193	-0.178	-0.182	-0.180	-0.184	-0.197	-0.216	-0.157
St	.337	-0.641	-0.693	-0.745	-0.755	-0.747	-0.755	-0.782	-0.806	-0.781	-0.716	-0.368	-0.330	-0.297	-0.304	-0.300	-0.306	-0.320	-0.340	-0.263
	300	-0.725	-0.780	-0.842	-0.842	-0.844	-0.836	-0.844	-0.859	-0.894	-0.964	-0.974	-0.548	-0.476	-0.486	-0.477	-0.489	-0.510	-0.529	-0.411
	.226	-0.149	-0.179	-0.208	-0.212	-0.208	-0.210	-0.226	-0.256	-0.233	-0.262	-0.304	-0.318	-0.291	-0.299	-0.293	-0.299	-0.318	-0.344	-0.258
	.153	-0.085	-0.112	-0.134	-0.142	-0.136	-0.139	-0.159	-0.193	-0.152	-0.171	-0.196	-0.210	-0.195	-0.201	-0.197	-0.202	-0.221	-0.249	-0.175
	α, deg	-0.161	-0.125	-0.117	-3.120	-0.100	2.877	5.817	8.873	-0.145	-0.145	-0.14	-0.132	-0.139	-3.125	-0.141	2.842	5.868	8.847	-0.151
	M∞	0.952	0.927	0.899	0.900	0.899	0.900	0.900	0.899	0.877	0.847	0.800	0.698	0.602	0.600	0.602	0.602	0.601	0.602	0.401

Table 17. Continued

(b) Concluded

		_	_			_	_		_		_	_			\neg		_	_	\neg	_
	.926	-0.097	-0.069	-0.041	-0.072	-0.046	-0.016	-0.036	-0.047	-0.017	0.013	0.051	0.123	0.124	0.127	0.125	0.110	0.098	0.075	0.112
0.50	.705	-0.193	-0.115	-0.090	-0.136	-0.090	-0.076	-0.112	-0.147	-0.074	-0.056	-0.032	0.002	-0.003	-0.002	900.0-	-0.007	-0.026	-0.068	-0.008
all at z/Z = -	.558	-0.322	-0.152	-0.113	-0.144	-0.114	-0.116	-0.171	-0.221	-0.103	-0.101	-0.093	-0.077	-0.075	080'0-	-0.078	-0.077	-0.094	-0.130	-0.070
nozzle sidew of x/l of—	.411	1	_		1	1	1	_	_	1	1	1	-	-	ı	ı	1	ı	ı	1
efficients on nozzle side with values of x/l of—	.337	-0.637	-0.689	-0.744	-0.769	-0.747	852.0-	-0.793	-0.843	-0.788	-0.809	-0.429	-0.354	-0.314	-0.312	-0.316	-0.327	-0.351	-0.385	-0.270
Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$ with values of z/I of—	.300	-0.663	-0.714	-0.772	-0.785	-0.773	-0.775	-0.796	-0.831	-0.823	-0.888	-0.977	-0.613	-0.530	-0.520	-0.534	-0.572	-0.620	-0.673	-0.454
Stati	.226	-0.150	-0.183	-0.213	-0.234	-0.216	-0.202	-0.222	-0.265	-0.236	-0.265	-0.307	-0 322	-0.290	-0.290	-0.290	-0.305	-0.336	-0.379	-0.257
	.153	-0.089	-0.114	-0.135	-0.153	-0.136	-0.134	-0.161	-0.209	-0.152	-0.171	70 106	0129	-0.201	-0.208	-0.204	5000	-0.239	-0.284	-0.180
	α, deg	1910-	-0.125	-0.117	-3.120	-0.100	2.877	5.817	8.873	-0.145	-0.145	0 144	0.133	5 130	-3 125	-5 141	2 842	898 5	8 847	-0.151
:	M	0.952	0.927	0 899	0060	0.899	0060	0060	0 800	0.877	0.847	008.0	0090	0.020	0,600	0,50	200.0	109.0	090	0.02

Table 17. Continued

(c) Static pressure coefficients on nozzle bottom flap

	926	-0.063	-0.057	-0.023	-0.017	-0.025	-0.040	-0.051	-0.050	0.004	0.036	080.0	0.150	0.147	0.131	0.146	0.131	0.117	0.102	0.137
	.853	-0.080	-0.091	-0.055	-0.040	-0.059	-0.075	-0.090	-0.095	-0.028	0.008	0.054	0.116	0.114	0.108	0.113	0.091	0.071	0.052	0.104
= 0.75	622.	-0.114	-0.129	-0.091	-0.071	-0.095	-0.111	-0.132	-0.143	-0.065	-0.025	0.025	0.081	0.077	0.083	0.074	0.053	0.030	0.008	0.069
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.75$ with values of x/l of—	.705	-0.166	-0.173	-0.136	-0.116	-0.140	-0.147	-0.170	-0.189	-0.104	-0.065	-0.012	0.041	0.036	0.051	0.033	0.009	-0.014	-0.034	0.033
nozzle botton of x/l of—	.558	-0.322	-0.259	-0.228	-0.229	-0.234	-0.232	-0.263	-0.294	-0.200	-0.162	-0.113	-0.063	-0.061	-0.034	-0.063	-0.089	-0.109	-0.125	-0.059
fficients on nozzle bott with values of x/l of-	.411	-0.732	-0.432	-0.371	-0.374	-0.371	-0.354	-0.394	-0.481	-0.348	-0.316	-0.269	-0.228	-0.221	-0.188	-0.223	-0.250	-0.270	-0.287	-0.205
pressure coe	.337	-0.841	-0.858	-0.822	-0.798	-0.825	-0.764	-0.821	-0.899	-0.797	-0.745	-0.688	-0.485	-0.445	-0.382	-0.450	-0.496	-0.531	-0.558	-0.400
Static	300	-		ļ	_	_	***	_	-		-	_		-	_	ı	I	1	****	1
	.226	-0.152	-0.184	-0.213	-0.248	-0.216	-0.194	-0.189	-0.197	-0.239	-0.267	-0.310	-0.350	-0.324	-0.309	-0.326	-0.342	-0.356	-0.370	-0.289
	.153	-0.092	-0.118	-0.139	-0.160	-0.141	-0.131	-0.135	-0.150	-0.158	-0.178	-0.204	-0.229	-0.217	-0.215	-0.219	-0.227	-0.240	-0.256	-0.199
	α, deg	-0.161	-0.125	-0.117	-3.120	-0.100	2.877	5.817	8.873	-0.145	-0.145	-0.144	-0.132	-0.139	-3.125	-0.141	2.842	5.868	8.847	-0.151
	M_{∞}	0.952	0.927	668'0	0.900	668'0	006'0	006'0	668'0	<i>LL</i> 8.0	0.847	008'0	869'0	0.602	0.600	0.602	0.602	0.601	0.602	0.401

Table 17. Continued

(c) Continued

-0.046-0.056-0.065 -0.042 -0.022 0.025 0.162 0.165 0.153 0.163 0.148 0.134 0.155 -0.0550.121 -0.0120.077 -0.051-0.077926 -0.056-0.083 -0.096-0.102 -0.048 -0.006 0.055 0.134 0.133 0.1260.108 0.086 0.068 0.123 -0.079-0.1030.131 0.119 .853 -0.124 -0.126 0.096 -0.149-0.102-0.136-0.150-0.090-0.0460.022 0.100 0.098 0.099 0.070 0.045 0.024 0.09 -0.161-0.121*6LL*: Static pressure coefficients on nozzle bottom flap at y/Y = 0.50-0.139 -0.092 -0.181 -0.199 0.000 0.052 -0.018 0.059 0.068 -0.208-0.168-0.1590.060 0.057 0.027 -0.021-0.203-0.171-0.165705 -0.243 -0.038-0.246-0.135-0.039-0.015-0.122-0.038with values of x/l of--0.300-0.266-0.285-0.270-0.273-0.304-0.037-0.073-0.101-0.327.558 -0.362 -0.219 -0.214 -0.216-0.370-0.382-0.419 -0.454-0.372-0.256-0.289-0.425-0.201-0.802-0.357-0.311-0.397-0.381.41 -0.476-0.479-0.620-0.508-0.560-0.533-0.585-0.512-0.599-0.507-0.418-0.544-0.432-0.530-0.503-0.747-0.591-0.932-0.646.337 -0.942 -1.084 -1.202 -1.282 -0.791 -0.812-0.828 -0.935-0.826-0.859-0.858 -1.046-0.768-0.836-0.817-0.842-0.857-0.887-1.193300 .226 -0.1450.14 -0.130-0.120 -0.164 -0.186-0.260-0.255-0.259-0.267-0.239-0.218-0.267-0.096 -0.157-0.108-0.241-0.271-0.121.153 α, deg -3.120 -0.100 -0.145-0.144-0.1392.842 5.868 -0.1252.877 5.817 8.873 -0.145-0.132-3.125-0.1418.847 -0.117-0.1519.191 0.900 869.0 0.600 0.602 0.602 0.602 668.0 0.800 0.602 0.900 0.899 M_{∞} 0.952 0.899 0.877 0.847 0.601 0.401 0.927

Table 17. Continued

(c) Concluded

			Station	c pressure co	efficients on	Static pressure coefficients on nozzle bottom flap at centerline	n flap at cen	terline	
M	α, deg	.153	226	300	337	411	558	705	900
200	200	100			100:		occ.	50/-	076.
0.932	101.0	-0.104 401.04	-0.177	1	-	-0.753	1	-0.233	-0.089
0.927	-0.125	-0.127	-0.204	1	1	-0.404	ı	-0.216	-0.085
0.899	-0.117	-0.150	-0.233	1	-	-0.360	-	-0.177	-0.052
0.900	-3.120	-0.155	-0.240	l	-	-0.394	1	-0.169	-0.041
0.899	-0.100	-0.150	-0.235	-	_	-0.362	1	-0.176	-0.057
0.900	2.877	-0.139	-0.217			-0.328	ı	-0.176	-0.057
0.900	5.817	-0.128	-0.207	-	1	-0.366	1	-0.190	-0.063
0.899	8.873	-0.114	-0.194	1		-0.426		-0.212	-0.059
0.877	-0.145	-0.168	-0.255	_	_	-0.352		-0.149	-0.021
0.847	-0.145	-0.191	-0.289	1	. –	-0.351		-0.103	0.018
0.800	-0.144	-0.227	-0.343	-	-	-0.362		-0.032	0.074
0.698	-0.132	-0.282	-0.438	1	-	-0.242	1	0.065	0.169
0.602	-0.139	-0.280	-0.428	1	-	-0.238		0.062	0.175
0.600	-3.125	-0.261	-0.399	1	1	-0.204	1	0.073	0.174
0.602	-0.141	-0.283	-0.431	_	-	-0.240	. 1	0.059	0.177
0.602	2.842	-0.299	-0.460	_	ı	-0.284		0.028	0.162
0.601	5.868	-0.305	-0.473		l	-0.316		0.001	0.152
0.602	8.847	-0.301	-0.476	_	1	-0.338	1	-0.021	0.139
0.401	-0.151	-0.262	-0.388	ļ	J	-0.227	ļ	0.050	0.171

Table 17. Concluded

(d) Force data

0.2160 0.2385 0.1770 0.1564 0.1241 0.0718 0.0752 0.0718 0.0777 0.0885 0.0997 0.0857 $\begin{array}{c} C_D \\ 0.2641 \\ 0.2208 \\ 0.1946 \\ 0.2155 \\ 0.1960 \\ 0.1919 \end{array}$ α, deg -0.161 2.842 5.868 8.847 -0.151 -0.144 -3.120 -0.145-0.145 -0.139-3.125-0.125 8.873 5.817 2.877 0.927 0.899 0.900 0.900 0.900 0.900 0.899 0.847 0.602 0.602 0.601 0.800 869.0 0.401 0.952 M_{∞}

Table 18. Pressure and Force Data for Nozzle 11 With $\beta_{t,top/bot} = \beta_{t,side} = 16.4^{\circ}$, Plume On, and $\alpha = 0^{\circ}$

(a) Static pressure coefficients on nozzle top flap

Static pressure coefficients on nozzle top flap at centerline with values of x/l of—	300 337 411 484 558 632 705 779 853 926	70.487 -0.204 -0.076 0.006 0.070 0.117 - 0.196 0.224	0.502 -0.194 -0.064 0.017 0.076 0.122 - 0.191	- -0.382 -0.208 -0.124 -0.068 -0.027 0.007 - 0.070	- -0.497 -0.475 -0.430 -0.255 -0.131 -0.115 -	0.543 -0.516 -0.469 -0.191 -0.143 -0.127 0.093 -	0.452 -0.289 -0.233 -0.206 -0.183 -0.1650.116	0.358 -0.244 -0.209 -0.183 -0.162 -0.1390.082	0.326 -0.236 -0.199 -0.174 -0.148 -0.1210.057	0.318 -0.233 -0.188 -0.157 -0.125 -0.0940.026	0.317 -0.221 -0.168 -0.130 -0.096 -0.063 - 0.003	0.377 -0.204 -0.124 -0.072 -0.030 0.002 - 0.062	0.498 -0.193 -0.064 0.017 0.077 0.122 - 0.186	0.484 -0.204 -0.076 0.006 0.068 0.118 - 0.193	
Static pres	.337		-	H	-0.497	-0.543	-0.452	-0.358					-0.498		7070
	.153 .226	-0.276 -0.427	-0.278 -0.433	-0.219 -0.330	0.001 -0.006	-0.002 -0.018	-0.095 -0.162	-0.121 -0.192	-0.141 -0.219	-0.163 -0.250	-0.181 -0.277	-0.218 -0.332	-0.277 -0.432	-0.278 -0.426	0.052
	Μ∞	0.600	0.700	0.798	1.250	1.202	0.951	0.926		0.876	0.852	0.799	0.702	0.602	0 300

	Γ	L		Ţ										Γ	
	.926	0.226	0.214	0.096	-0.059	0.07	-0.083	-0.050	-0.022	0.010	0.039	0.092	0.210	0.222	0 217
	.853	0.196	0.190	0.069	-0.083	-0.094	-0.117	-0.086	-0.057	-0.026	0.003	0.063	0.187	0.193	0.187
0.25	677.	0.161	0.161	0.039	-0.100	-0.114	-0.144	-0.114	-0.091	-0.064	-0.031	0.034	0.158	0.158	0.151
flap at $y/Y =$.705	0.117	0.122	9000	-0.119	-0.131	-0.171	-0.141	-0.125	960.0-	-0.065	0.003	0.120	0.115	0.108
ifficients on nozzle top with values of x/l of—	.558	0.007	0.016	-0.070	-0.324	-0.221	-0.210	-0.189	-0.178	-0.160	-0.133	-0.071	0.018	0.008	0.001
coefficients o	114.	-0.197	-0.188	-0.214	-0.471	-0.511	-0.305	-0.260	-0.242	-0.233	-0.226	-0.208	-0.187	-0.195	-0.186
Static pressure coefficients on nozzle top flap at $y/Y = 0.25$ with values of x/l of—	.337	-0.476	-0.494	-0.389	-0.497	-0.539	-0.494	0.377	-0.342	-0.322	-0.328	-0.379	-0.493	-0.478	-0.428
Sta	300	-0.962	-1.300	-0.898	-0.379	-0.417	-0.748	-0.725	-0.704	-0.694	-0.724	-0.876	-1.272	-0.959	-0.788
	.226	-0.419	-0.427	-0.326	-0.008	-0.015	-0.160	-0.191	-0.217	-0.249	-0.273	-0.330	-0.425	-0.419	-0.372
	.153	-0.268	-0.270	-0.214	0.002	-0.001	-0.094	-0.119	-0.140	-0.160	-0.178	-0.214	-0.270	-0.269	-0.245
	M∞	0.600	0.700	0.798	1.250	1.202	0.951	0.926	0.903	0.876	0.852	0.799	0.702	0.602	0.399

Table 18. Continued

(a) Concluded

	926	37	0.224	0.215	0.103	-0.052	-0.068	-0.082	-0.049	-0.022	0.011	0.041	0.095	0.210	0.218	0.210	
	853	660.	0.194	0.189	0.072	-0.077	-0.092	-0.120	-0.086	-0.060	-0.029	0.005	0.065	0.186	0.189	0.180	
0	170	677	0.155	0.156	0.042	-0.094	0.110	-0.150	0.119	-0.094	-0.065	-0.030	0.036	0.155	0.153	0.141	
at $y/Y = 0.5$	302	./co/.	0.116	0.121	0.013	-0.111	-0.125	-0.174	-0.147	-0.125	H	H	0.007	0.120	0.114	0.105	
zzle top flap	10 10	800.	0.010	0.017	-0.065	-0.366	-0.314	-0.215	Ė		-	H	-0.067	0.019	0.010	0.011	
Static pressure coefficients on nozzle top flap at $y/Y = 0.50$	III VAILUS OI	.411	0.182	0.181			H	H	\dagger	t	T	t	╁		-	-	$\left\{ \right.$
ssure coeffi	 	.337	0.449	l	r	H	t	T	T	+	T	+	+	 	+		1
atic pre	ľ	<u>.ن</u>	9	9	٩	9	9	9	9	19		19	9	9	19	19	,
St		300	-0.924	-1.216	-0.935	777	0.418	97.0	792.0	0.757	0770	0.773	5100	1 201	0 033	-0.757	3
		.226	-0.388	-0.403	5318	0000	0.00	0.157	0.187	0.187	0.214	7960	0.20	0.320	0.402	-0.350	2000
		.153	D 250	0.257	0000	1000	1000	0.002	0110	0.119	-0.138	0176	0.170	0.257	0.262	0.22	7.77
		M	0090	000.0	0.708	1 250	2000	1.202	10.60	0.920	0.903	0.870	0.632	0.793	0.702	0.902	0.327

	1	Т	_	_	_	_		_	Г	_	_		_	1	Т	_		_	7
	.926	1,00	0.217	0.215	0.122	-0.031	-0.051	-0.074	0,00	-0:0±0	-0.013	0.021	0.057	0116	0.115	0.211	0.213	0.203	22.2
	.853	, ,	0.184	0.186	0.000	-0.062	-0.078	-0.109	7200	±0.0/4	-0.049	-0.014	0.021	2000	0.003	0.184	0.183	0.172	0.17
.75	622		0.145	0.152	0.059	-0.087	-0.100	-0.145		۰. ۱۱۱۱	-0.086	-0.053	-0.015	6500	0.033	0.151	0.145	0.136	0.1.0
ap at $y/Y = 0$	705	2	0.105	0.112	0.030	-0.133	-0.125	02.1		-0.142	-0.118	-0.088	10.051		0.024	0.112	0.104	7000	0.020
Static pressure coefficients on nozzle top flap at $y/Y = 0.75$	558	300	0.001	800.0	-0.044	-0.321	-0.353	7000	1	-0.209	-0.188	-0.163	20178		-0.048	600.0	0.001	1000	0.001
fficients on nozzle top	411	-	-0.175	-0.178	-0.192	-0.402	-0.438	0 346	2:5	-0.301	-0.279	-0.270	0.251		-0.193	-0.177	-0 174		-0.100
pressure coe	327	,cc.	-0.429	0.464	0.511	D 448	7070	2777		-0.634	-0.514	-0.473	0.467	101.0	-0.502	-0.463	0 470	, in a	-0.3/6
Static	300	onc.	-						'	1		-		'	ı				-
	200	077:	-0.339	-0.363	-0.307	8000	0.000	20.010	-0.133	-0.185	21.0	0.238	0.250	20.200	-0.310	795 0-	0.341	1	-0.300
		.153	-0.215	-0.227	0 105		200.0		-0.093	-0.114	0 134	0.157	11 \	-0.10/	-0.194		2100	I	0.194
		W 8	0.600	0 700	0 708	1 250	200	1.202	0.951	9260	2000	2000	0.070	0.832	0.799	07.0	20/.0	0.007	0.399

Table 18. Continued

(b) Static pressure coefficients on nozzle sidewall

			Static pres	sure coefficie	ints on comer	Static pressure coefficients on corner between nozzle top flap and sidewall	zle top flap a	nd sidewall		
					with value:	with values of x/l of-				
M	.153	.226	.300	.337	.411	.558	.705	6 <i>LL</i>	.853	.926
0.600	-0.218	ı	-0.744	-0.411	-0.161	900.0	0.097	0.135	0.171	0.205
0.700	-0.229	1	-0.903	-0.445	-0.166	0.011	0.104	0.142	0.177	0.207
0.798	-0.200	١	-1.013	-0.554	-0.176	-0.017	0.057	0.083	0.108	0.127
1.250	0.001	ı	-0.319	-0.446	-0.381	-0.281	-0.202	-0.114	-0.049	-0.003
1.202	-0.005	I	-0.360	-0.489	-0.413	-0.313	-0.176	101.0-	-0.058	-0.023
0.951	-0.094	1	-0.677	-0.844	-0.431	-0.206	-0.152	-0.127	-0.104	-0.088
0.926	-0.119	1	-0.732	-0.815	-0.319	-0.188	-0.119	160'0-	-0.066	-0.044
0.903	-0.139	1	-0.782	-0.704	-0.281	-0.164	-0.088	-0.058	-0.030	-0.010
0.876	-0.158	1	-0.836	-0.615	-0.264	-0.129	-0.050	-0.020	9000	0.028
0.852	-0.171	l	-0.892	-0.578	-0.239	-0.089	-0.011	0.015	0.042	0.062
0.799	-0.200	1	-1.013	-0.550	-0.177	-0.019	0.053	0.079	0.102	0.120
0.702	-0.228	ı	-0.899	-0.444	-0.163	0.013	0.105	0.140	0.175	0.204
0.602	-0.219	ı	-0.741	-0.411	-0.158	0.005	0.095	0.131	0.168	0.202
0.399	-0.197	1	-0.622	-0.361	-0.143	0.009	0.088	0.123	0.158	0.192

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		926	0.205	0.208	0.156	0.00	-0.004	-0.010	0.022	0.046	0.075	0.105	0.152	0.206	0.203	0.194
		.853	0.173	0.178	0.126	-0.049	-0.049	-0.053	-0.017	0.009	0.040	0.072	0.121	0.177	0.171	0.161
0.50		<i>6LL</i> :	0.134	0.141	0.095	-0.130	-0.107	-0.090	-0.055	-0.029	0.004	0.037	0.091	0.141	0.135	0.125
vall at z/Z = (.705	960.0	0.105	0.063	-0.205	-0.194	-0.119	-0.088	-0.066	-0.030	0.007	0.062	0.103	0.095	0.092
nozzle sidev	IO 1/X IO	.558	i		_	ŧ	1	f	ı	1	1	1	ı	1	ı	1
Static pressure coefficients on nozzle sidewall at $z/Z = 0.50$	with values of x/l of—	.411	-0.158	-0.164	-0.195	-0.409	-0.442	-0.549	-0.346	-0.309	-0.288	-0.265	-0.199	-0.160	-0.158	-0.144
ic pressure co		.337	-0.411	-0.446	-0.555	-0.447	-0.486	-0.853	-0.875	-0.770	-0.664	-0.608	-0.553	-0.442	-0.408	-0.363
Stal		.300	-0.720	698.0-	-1.004	-0.320	-0.355	-0.668	-0.722	-0.770	-0.830	-0.880	-1.004	-0.865	-0.715	-0.603
		.226	-0.332	-0.358	-0.311	-0.010	-0.024	-0.163	-0.192	-0.217	-0.244	-0.266	-0.314	-0.356	-0.334	-0.295
		.153	-0.216	-0.226	-0.200	-0.004	-0.009	-0.100	-0.122	-0.141	-0.162	-0.173	-0.204	-0.227	-0.217	-0.195
		M∞	0.600	0.700	0.798	1.250	1.202	0.951	0.926	0.903	0.876	0.852	0.799	0.702	0.602	0.399

Table 18. Continued

(b) Concluded

	.926	1		-	1	-	-	I	1	1		ı	1	ı	1
	.853	0.170	0.177	0.131	-0.049	0.044	-0.032	-0.004	0.016	0.047	0.079	0.129	0.176	0.169	0.161
	<i>6LL</i> :	0.135	0.142	0.103	-0.134	-0.109	-0.066	-0.039	-0.019	0.015	0.048	0.099	0.142	0.134	0.125
ne	.705	0.101	0.108	0.074	-0.198	-0.195	-0.090	-0.073	-0.052	-0.020	0.015	0.069	0.106	0.097	0.091
Static pressure coefficients on nozzle sidewall at centerline with values of x/l of—	.632	0.058	0.064	0.037	-0.225	-0.248	-0.117	-0.103	-0.093	-0.063	-0.023	0.034	0.065	0.057	0.055
nozzle sidew of x/l of—	.558	0.013	0.015	-0.010	-0.265	-0.289	-0.158	-0.144	-0.149	-0.118	-0.080	-0.013	0.015	0.010	0.010
oefficients on nozzle sid with values of x/l of—	.484	-0.052	-0.051	680:0-	-0.330	-0.352	-0.238	-0.216	-0.242	-0.212	-0.174	-0.093	-0.052	-0.053	-0.049
tic pressure c	.411	-0.153	-0.156	-0.251	-0.405	-0.437	-0.619	-0.381	-0.372	-0.356	-0.336	-0.248	-0.155	-0.153	-0.139
Sta	.337	-0.385	-0.409	-0.569	-0.492	-0.540	-0.920	-0.854	-0.578	-0 540	-0.534	-0.566	-0.407	-0.384	-0.339
	.300	-0.846	-1.015	-1.041	-0.384	-0.427	-0.784	-0.838	-0.864	0880	9060-	-1.016	-1.005	-0.837	-0.703
	.226	-0.344	-0.366	-0.313	-0.008	-0.024	-0.159	188	-0.214	-0.242	-0.264	-0.316	10 364	-0 345	-0.312
	153	A 218	-0.230	-0.202	0.005	9000	060 0	0.122	0.141	0.150	0.173	202.0	57.0	0.220	-0.198
	×	0090	0.000	0 798	1 250	1 202	0.051	9000	0.520	0.976	0.670	002.0	0.702	20/30	0.399

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		.926	0.206	0.210	0.167	0.005	-0.006	0.002	0.025	0.051	0.079	0.110	0.159	0.206	0.201	0.192
).50		.705	0.097	0.105	0.075	-0.219	-0.210	-0.096	-0.077	-0.058	-0.023	0.015	0.072	0.105	960.0	0.090
all at $z/Z = -4$.558	0.005	0.009	-0.009	-0.289	-0.313	-0.161	-0.152	-0.144	-0.118	-0.077	-0.013	0.010	0.005	0.003
ozzle sidewa	—jo //x jo	.411	1	-	١	1	1	1	1	1	-	_	-	1	1	1
Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$	with values of x/l of-	.337	-0.389	-0.418	-0.589	-0.463	-0.505	-0.871	-0.883	-0.782	-0.654	-0.605	-0.584	-0.417	-0.387	-0.339
pressure co		.300	-0.780	-0.948	-1.075	-0.348	-0.390	-0.721	-0.775	-0.825	-0.884	-0.939	-1.076	-0.942	-0.780	-0.653
Station		.226	-0.331	-0.354	-0.311	-0.011	-0.028	491.05	-0.193	-0.216	-0.243	-0.265	-0.314	-0.355	-0.332	-0.297
		.153	-0.216	-0.229	-0.202	9000	600.0	-0.097	-0.121	-0.139	-0.160	-0.170	-0.202	-0.225	-0.213	0 190
		M ₈	0.600	0.700	0.798	1.250	1.202	0.951	0.926	0.903	0.876	0.852	0.799	0.702	0.602	0 300
_																

Table 18. Continued

(c) Static pressure coefficients on nozzle bottom flap

	.926	0.218	0.221	0.164	-0.021	-0.036	-0.026	-0.013	0.019	0.056	0.092	0.158	0.216	0.214	0.204
	.853	0.184	0.190	0.138	-0.052	-0.063	-0.062	-0.049	-0.017	0.021	090'0	0.133	0.188	0.180	0.172
= 0.75	<i>6LL</i> :	0.146	0.153	0.108	-0.082	-0.093	-0.094	-0.086	-0.052	-0.013	0.026	0.104	0.152	0.144	0.136
n flap at y/Y	.705	0.104	0.112	0.074	-0.159	-0.134	-0.126	-0.122	-0.092	-0.051	-0.012	0.072	0.112	0.101	0.092
icients on nozzle bottor with values of x/l of—	.558	0.002	0.007	-0.018	-0.340	-0.370	-0.197	-0.196	-0.177	-0.145	-0.105	-0.022	0.007	0.000	-0.002
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.75$ with values of x/l of—	.411	-0.169	-0.174	-0.209	-0.405	-0.443	-0.461	-0.312	-0.298	-0.283	-0.265	-0.213	-0.173	-0.172	-0.157
pressure co	.337	-0.422	-0.454	-0.604	-0.453	-0.496	-0.830	-0.749	-0.664	-0.591	-0.573	-0.597	-0.450	-0.421	-0.374
Static	.300	-0.765	-0.929	-1.020	-0.321	-0.362	-0.678	-0.729	-0.777	-0.837	-0.888	-1.018	-0.928	-0.765	-0.644
	.226	-0.337	-0.363	-0.315	-0.011	-0.030	-0.166	-0.196	-0.220	-0.247	-0.269	-0.317	-0.362	-0.338	-0.300
	.153	-0.222	-0.234	-0.207	0.005	-0.013	-0.099	-0.123	-0.142	-0.163	-0.176	-0.208	-0.232	-0.223	-0.198
	M∞	0.600	0.700	0.798	1.250	1.202	0.951	0.926	0.903	0.876	0.852	0.799	0.702	0.602	0.399

	_	Т	_	1	_	т-	-	1	Т	Τ-	_	_	_	1	_
	.926	0 222	0 224	0.158	-0.036	-0.045	-0.036	-0.017	0.013	0.047	0.084	0.154	0.219	0.215	0.209
	.853	0 100	0.194	0.134	-0.060	-0.069	-0.069	-0.052	-0.021	0.016	0.052	0.129	0.191	0.186	0.177
= 0.50	977.	0.153	0.158	0.105	-0.087	-0.096	-0.102	-0.086	-0.058	-0.020	0.017	0.100	0.156	0.149	0.142
n flap at y/Y	.705	0.112	0.117	0.069	-0.117	-0.127	-0.135	-0.119	-0.096	-0.058	-0.022	0.064	0.116	0.107	0.099
nozzle botton	.558	0.003	0.00	-0.037	-0.397	-0.414	-0.211	-0.197	-0.180	-0.154	-0.128	-0.041	0.009	-0.001	-0.005
fficients on nozzle both with values of v/l of	.411	-0.184	-0.184	-0.253	-0.458	-0.497	-0.374	-0.300	-0.288	-0.284	-0.280	-0.256	-0.183	-0.185	-0.176
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.50$ with values of y/l of—	.337	-0.447	-0.475	-0.534	-0.490	-0.534	-0.750	-0.492	-0.440	-0.420	-0.424	-0.528	-0.470	-0.450	-0.400
Static	.300	-0.815	-0.999	-1.092	-0.378	-0.418	-0.759	-0.790	-0.806	-0.839	-0.868	-1.074	-0.990	-0.812	-0.685
	.226	-0.384	-0.408	-0.337	-0.008	-0.025	-0.174	-0.203	-0.230	-0.258	-0.282	-0.338	-0.408	-0.385	-0.345
	.153	-0.248	-0.256	-0.218	0.009	-0.010	-0.102	-0.126	-0.147	-0.168	-0.183	-0.219	-0.254	-0.246	-0.223
	M∞	0.600	0.700	0.798	1.250	1.202	0.951	0.926	0.903	0.876	0.852	0.799	0.702	0.602	0.399

Table 18. Concluded

(c) Concluded

		Static	pressure cox	Static pressure coefficients on nozzle bottom flap at centerline	nozzle bottom	ı flap at cente	erline	
				with values of x/l of—	—Jo <i>I/X</i> Jo			
M	.153	.226	.300	.337	.411	.558	.705	.926
0090	-0.271	-0.411	-0.849	-0.471	-0.210	-0.008	0.104	0.234
0 700	-0.280	-0.437	-1.055	-0.498	-0.209	0.002	0.116	0.235
0 798	_0.231	-0.358	-1.097	-0.531	-0.249	-0.044	0.063	0.158
1 250	0.006	-0.017	-0.383	-0.478	-0.464	-0.398	-0.124	-0.043
1 202	6000	-0.037	-0.425	-0.525	-0.508	-0.265	-0.138	-0.057
0.051	-0.113	-0.192	-0.768	-0.572	-0.323	-0.222	-0.161	-0.054
9000	-0.135	-0.218	-0.778	-0.433	-0.280	-0.189	-0.127	-0.022
0.000	-0.153	-0.241	-0.773	-0.395	-0.269	-0.180	-0.103	0.008
0.876	971.0-	-0.270	-0.808	-0.397	-0.269	-0.158	690.0-	0.043
0.852	-0.193	-0.296	-0.865	-0.422	-0.263	-0.125	-0.029	0.080
0 799	-0.233	-0.358	-1.076	-0.530	-0.252	-0.046	0.058	0.152
0.707	-0.276	-0.435	-1.052	-0.496	-0.206	0.001	0.114	0.229
0,602	-0.270	-0.411	-0.852	-0.472	-0.210	-0.011	0.104	0.227
0 399	-0.247	-0.366	-0.715	-0.417	-0.197	-0.017	0.094	0.220
11000								

(d) Force data

c_{Df}	0.0120	0.0117	0.0114	0.0106	0.0107	0.0112	0.0112	0.0113	0.0113	0.0114	0.0115	0.0118	0.0120	0.0128
$c_{D,p}$	0.0396	0.0498	0.0986	0.2192	0.2332	0.2322	0.1966	0.1759	0.1553	0.1347	0.1000	0.0496	0.0405	0.0318
c_D	0.0348	0.0381	0.0919	0.2338	0.2462	0.2336	0.1998	0.1762	0.1534	0.1341	0.0917	0.0438	0.0379	0.0315
M	0.600	0.700	0.798	1.250	1.202	0.951	0.926	0.903	0.876	0.852	0.799	0.702	0.602	0.399

Table 19. Pressure and Force Data for Nozzle 11 With $\beta_{t,top/bot} = \beta_{t,side} = 16.4^{\circ}$ and Plume Off

(a) Static pressure coefficients on nozzle top flap

	.926	-0.066	-0.083	-0.083	-0.078	-0.086	-0.102	-0.096	-0.067	-0.036	-0.063	-0.038	-0.011	0.000	0.012	-0.010	0.024	0.075	0.178	0.173	0.152	0.172	0.168	0.159	0.139	0.167
	.853	-0.084	-0.101	-0.102	-0.101	-0.116	-0.118	-0.121	-0.096	-0.069	-0.098	-0.071	-0.049	-0.043	-0.036	-0.048	-0.010	0.048	0.153	0.144	0.115	0.143	0.146	0.136	0.116	0.135
	671.		1	ļ	weeks	1	1	ı	1	1	ŀ	1	ŧ	-	1	ı	1	1	ı	t	i	ı	I	1	l	
ine	.705	-0.112	-0.129	-0.127	-0.133	-0.160	-0.148	-0.147	-0.138	-0.122	-0.149	-0.125	-0.119	-0.128	-0.129	-0.105	-0.072	-0.010	980.0	0.076	0.035	0.073	0.090	0.084	0.063	0.066
Static pressure coefficients on nozzle top flap at centerline	.632	-0.132	-0.145	-0.144	-0.151	-0.215	-0.164	-0.163	-0.155	-0.145	-0.170	-0.144	-0.151	-0.171	-0.175	-0.130	-0.101	-0.039	0.042	0.031	-0.012	0.030	0.053	0.049	0.030	9600
nozzle top f		-0.275	-0.200	-0.203	-0.230	-0.425	-0.196	-0.178	-0.172	-0.168	-0.191	-0.166	-0.182	-0.213	-0.223	-0.155	-0.137	-0.082	-0.016	-0.027	-0.073	-0.028	0.000	0.000	-0.018	6600
oefficients or	.484 .558	-0.428	-0.466	-0.464	-0.455	-0.471	-0.455	-0.203	-0.193	-0.187	-0.213	-0.187	-0.208	-0.251	-0.268	-0.185	-0.174	-0.131	-0.094	-0.104	-0.152	-0.105	-0.071	990.0-	-0.084	50103
ic pressure c	114.	-0.478	-0.527	-0.525	-0.533	-0.537	-0.578	-0.250	-0.226	-0.221	-0.254	-0.221	-0.247	-0.298	-0.323	-0.217	-0.223	-0.208	-0.225	-0.229	-0.282	-0.230	-0.190	-0.180	-0.199	-0.214
Stat	.337	-0.493	-0.551	-0.545	-0.545	-0.543	-0.601	-0.389	-0.322	-0.307	-0.359	-0.310	-0.337	-0.406	-0.445	-0.304	-0.315	-0.368	-0.543	-0.510	-0.582	-0.511	-0.456	-0.440	-0.464	-0.458
	.300	ı	_		1	_	_			-	_	_		_	1	_	-	1	-	1	_	-	_	-	_	,
	.226	-0.006	-0.019	-0.015	-0.018	-0.020	-0.040	-0.160	-0.196	-0.223	-0.207	-0.224	-0.235	-0.240	-0.236	-0.249	-0.280	-0.334	-0.442	-0.440	-0.474	-0.441	-0.405	-0.385	-0.382	-0.395
	.153	0.002	-0.003	0.000	0.003	0.002	-0.020	960.0-	-0.124	-0.144	-0.132	-0.145	-0.153	-0.161	-0.163	-0.164	-0.185	-0.218	-0.287	-0.287	-0.304	-0.288	-0.265	-0.249	-0.241	-0.263
	α, deg	-0.020	-0.021	-0.022	2.984	6.037	-0.010	-0.027	-0.033	-0.015	-3.015	0.022	2.967	5.968	8.984	-0.016	-0.023	-0.031	-0.012	-0.012	-3.020	0.002	3.010	5.979	8.990	-0.026
	M	1.251	1.198	1.200	1.200	1.200	1.150	0.952	0.924	0.900	0.000	0.900	0.901	0.901	0.000	0.877	0.850	0.800	0.701	0.601	0.602	0.600	0.601	0.602	0.601	0.402

Table 19. Continued

(a) Continued

0.136 0.135 0.116 -0.094 -0.042 -0.0450.050 0.152 0.145 0.143 0.147 -0.069-0.099 -0.050-0.102 860.0--0.120-0.121 -0.086-0.103-0.071 0.01 = 연 .853 -0.126-0.098 -0.085-0.084 0.023 0.122 0.112 0.078 0.112 0.092 -0.120-0.085 -0.0750.122 -0.138-0.114-0.135 -0.097 -0.098911.0 -0.115-0.1340.111 Static pressure coefficients on nozzle top flap at y/Y = 0.25-0.127 -0.124 -0.075 0.074 0.090 -0.154-0.133-0.133-0.108 0.084 0.034 0.072 0.083 0.062 0.067 -0.127-0.150-0.151-0.143-0.163705 -0.235 -0.138-0.015 -0.018-0.026with values of x/l of--0.183-0.213-0.223-0.159 0.00 -0.230-0.182-0.195 -0.079-0.027-0.317 -0.173-0.166-0.0250.001 -0.451-0.176-0.071-0.211.558 -0.276-0.224-0.195-0.230 -0.254 -0.229-0.229-0.218-0.183-0.210-0.239-0.236-0.308 -0.222-0.175-0.519-0.574 -0.217-0.472 -0.517-0.527-0.259-0.261 -0.328-0.5234. -0.449-0.574-0.505 -0.450-0.435-0.460-0.450 -0.323 -0.533-0.546 -0.542 -0.545 -0.594 -0.348-0.328 -0.373 -0.322-0.422 -0.335-0.503-0.493 -0.351-0.387.337 -0.916 -0.906 -0.8170.709 -0.685 -0.675 -0.704 -0.778 -0.808-0.683-0.728-0.877-1.328-0.992-1.129 -0.997 -0.468-0.879-0.418-0.422-0.422 -0.423-0.679-0.731-0.377300 -0.465-0.433-0.376-0.385 -0.373-0.221 -0.232 -0.240-0.247 -0.432 -0.015 -0.019 -0.159-0.222 -0.328-0.436-0.307 0.006 -0.016-0.038-0.193.226 -0.279 -0.258 -0.242-0.236-0.256-0.214-0.1650.006 -0.122-0.140-0.149-0.297-0.020 -0.129-0.158-0.159-0.183-0.278-0.2810.005 0.003 -0.092-0.141.153 -0.001α, deg 8.990 -0.0265.968 8.984 -0.0163.010 5.979 0.022 -0.023-3.0200.002 -0.010 -0.015 -3.015-0.0122.984 -0.033-0.031 -0.012-0.020-0.0226.037 -0.027-0.021

0.901

0.877

0.900

0.901

1.200 1.150 1.150 0.952 0.924

1.198

M

0.850

0.701

0.600

0.602

0.602

0.601

0.402

0.601

-0.036

90.00

-0.101

-0.067 -0.084 -0.084

926

-0.082

-0.077

-0.038

-0.014

0.002

-0.064

0.164

0.158

0.171

0.076

0.008

Table 19. Continued

(a) Continued

		T	T	т-	_	_	_	_		_	_	_	_	_	_		_	_	_	_	_	_		_	_	_
	.926	-0.062	0800	-0.080	-0.073	-0.074	960:0-	-0.098	-0.064	-0.037	-0.065	-0.039	-0.013	0.004	0.014	-0.009	0.024	0.075	0.176	0.169	0.150	0.169	0.164	0.155	0.139	0.160
	.853	-0.083	-0.099	-0.099	-0.091	-0.100	-0.119	-0.127	-0.098	-0.072	-0.102	-0.074	-0.052	-0.037	-0.033	-0.045	-0.011	0.051	0.149	0.142	0.115	0.140	0.145	0.134	0.118	0.132
0.50	671.	-0.097	-0.114	-0.112	-0.107	-0.124	-0.133	-0.145	-0.124	-0.103	-0.133	-0.103	-0.088	-0.079	-0.079	-0.079	-0.042	0.024	0.117	0.109	0.077	0.108	0.119	0.110	0.093	0.100
Static pressure coefficients on nozzle top flap at $y/Y = 0.50$.705	-0.113	-0.128	-0.127	-0.126	-0.160	-0.148	-0.160	-0.149	-0.130	-0.161	-0.131	-0.126	-0.127	-0.130	-0.108	-0.074	-0.003	0.084	0.074	0.037	0.072	0.090	0.084	0.067	890.0
efficients on nozzle top	.558	-0.357	-0.315	-0.320	-0.295	-0.385	-0.253	-0.190	-0.187	-0.178	-0.205	-0.174	-0.187	-0.212	-0.221	-0.164	-0.140	-0.075	-0.012	-0.019	-0.063	-0.021	0.010	0.010	-0.007	-0.015
coefficients or	.411	-0.438	-0.484	-0.481	-0.509	-0.530	-0.536	-0.278	-0.257	-0.256	-0.288	-0.248	-0.278	-0.334	-0.339	-0.248	-0.245	-0.229	-0.203	-0.204	-0.256	-0.206	-0.161	-0.151	-0.167	-0.189
tic pressure c	.337	-0.496	-0.548	-0.544	-0.564	-0.565	-0.603	-0.452	-0.381	-0.369	-0.435	-0.356	-0.390	-0.467	-0.471	-0.359	-0.372	-0.432	-0.501	-0.472	-0.544	-0.474	-0.413	-0.403	-0.425	-0.419
Sta	300	-0.375	-0.422	-0.417	-0.421	-0.420	-0.469	-0.737	-0.725	-0.730	-0.798	-0.719	-0.746	-0.832	-0.837	-0.734	-0.776	-0.916	-1.259	-0.945	-1.086	-0.948	-0.872	-0.887	-0.924	-0.781
	.226	-0.005	-0.017	-0.014	-0.017	-0.023	-0.040	-0.157	-0.190	-0.216	-0.200	-0.218	-0.231	-0.243	-0.263	-0.242	-0.272	-0.321	-0.412	-0.403	-0.433	-0.405	-0.363	-0.340	-0.353	-0.358
	.153	-0.002	-0.004	0.000	-0.002	-0.012	-0.023	-0.097	-0.121	-0.141	-0.130	-0.142	-0.155	-0.172	-0.194	-0.160	-0.180	-0.211	-0.264	-0.262	-0.276	-0.263	-0.243	-0.235	-0.247	-0.236
	α, deg	-0.020	-0.021	-0.022	2.984	6.037	-0.010	-0.027	-0.033	-0.015	-3.015	0.022	2.967	5.968	8.984	-0.016	-0.023	-0.031	-0.012	-0.012	-3.020	0.002	3.010	5.979	8.990	-0.026
	M _∞	1.251	1.198	1.200	1.200	1.200	1.150	0.952	0.924	0.900	0.900	0.900	0.901	0.901	0.900	0.877	0.850	0.800	0.701	0.601	0.602	0.600	0.601	0.602	0.601	0.402
								1	<u> </u>	<u>ୀ</u>	<u> </u>	<u> </u>	<u> </u>		0	0	9	0		0	9	o'	0	0	0	<u>.</u> 0

Table 19. Continued

(a) Concluded

	7		_	_		_	_	· · · ·	_	-1	_	_	_	_	_		_	-1	1	_	_	_				_
	926	-0.055	-0.074	-0.073	-0.065	-0.068	-0.090	-0.102	-0.061	-0.032	-0.061	-0.035	0.001	0.027	0.033	-0.006	0.031	0.082	0.170	0.165	0.150	0.164	0.160	0.147	0.137	0.153
	.853	-0.072	-0.089	-0.088	-0.080	-0.096	-0.109	-0.129	-0.095	-0.067	-0.097	-0.069	-0.033	-0.006	-0.007	-0.038	-0.001	090.0	0.145	0.136	0.114	0.134	0.140	0.125	0.116	0.128
57.	622.	-0.091	-0.107	-0.106	-0.103	-0.137	-0.124	-0.152	-0.125	-0.100	-0.132	-0.102	-0.071	-0.049	-0.056	-0.072	-0.031	0.036	0.114	0.106	0.080	0.104	0.116	0.104	0.095	0.098
ap at y/Y = 0	.705	-0.128	-0.127	-0.126	-0.132	-0.198	-0.140	-0.168	-0.150	-0.128	-0.160	-0.129	-0.109	-0.095	-0.104	-0.103	-0.062	0.010	0.079	690.0	0.040	0.068	0.086	0.077	0.067	0.062
Static pressure coefficients on nozzle top flap at $y/Y = 0.75$ with values of x/l of—	.558	-0.323	-0.356	-0.354	-0.326	-0.330	-0.370	-0.208	-0.202	-0.193	-0.227	-0.192	-0.192	-0.205	-0.207	-0.171	-0.135	-0.061	-0.019	-0.024	-0.057	-0.026	0.003	800.0	-0.003	-0.025
efficients on nozzle to with values of x/l of-	.411	-0.401	-0.446	-0.443	-0.408	-0.389	-0.497	-0.292	-0.275	-0.275	-0.322	-0.269	-0.274	-0.311	-0.315	-0.267	-0.260	-0.207	-0.200	-0.194	-0.233	-0.196	-0.155	-0.129	-0.125	-0.176
ic pressure co	.337	-0.450	-0.494	-0.491	-0.456	-0.480	-0.551	-0.654	-0.544	-0.494	-0.622	-0.481	-0.456	-0.487	-0.460	-0.465	-0.478	-0.519	-0.485	-0.445	-0.512	-0.448	-0.366	-0.322	-0.313	-0.396
Stat	300			1	1	1	-	1	1	_	ı	1	1			-		-	-	1		1	ı	1	1	1
	.226	9000-	-0.016	-0.013	-0.041	-0.052	-0.046	-0.153	-0.187	-0.212	-0.193	-0.213	-0.247	-0.266	-0.282	-0.238	-0.265	-0.311	-0.374	-0.351	-0.371	-0.353	-0.330	-0.315	-0.307	-0.312
	.153	-0.001	40.004	-0.002	-0.012	-0.026	-0.029	-0.091	-0.116	-0.135		-0.137		-0.174			-0.170			-0.223	-0.232	-0.224	-0.221	-0.221	-0.225	-0.202
	α, deg	-0.020	-0.021	-0.022	2.984	6.037	-0.010	-0.027	-0.033	-0.015	-3.015	0.022	2.967	5.968	8.984	-0.016	-0.023	-0.031	-0.012	-0.012	-3.020	0.002	3.010	5.979	8.990	70.026
	M	1.251	1 198	1.200	1.200	1.200	1.150	0.952	0.924	006.0	0060	0060	0.901	0.00	0060	0.877	0.850	0.800	0.701	0.601	0.602	0.600	0.601	0.602	0.601	0.402

Table 19. Continued

(b) Static pressure coefficients on nozzle sidewall

0.199 -0.120 -0.080	-0.181 -0.116 -0.091 -0.075	-0.122 -0.088	-0.130	-0.106	-0.145	-0.092	-0.054 -0.032	-0.091 -0.064	-0.059 -0.036	-0.013 0.007	0.005 0.027	_	22 -0.001	7 0.037	4 0.089	4 0.159	5 0.153		0.151	\vdash		┝	L
-0.199 -0.120	-0.116	-0.122		1	+	\forall	-0.054	-0.091	0.059	.013	305	8	22	7	4	4	.5	4	4	S	∞	2	
-0.199		H	-0.183	0.121	3		7	1	1	9	0.0	-0.008	-0.022	0.017	0.074	0.134	0.125	0.114	0.124	0.135	0.118	0.112	0 116
+	-0.181	175		'1	-0.169	-0.118	-0.082	-0.122	-0.086	-0.044	-0.029	-0.044	-0.048	-0.003	0.055	0.105	960'0	0.081	0.094	0.109	960.0	0.088	8800
80	-	9	-0.227	-0.160	-0.181	-0.146	-0.110	-0.153	-0.114	-0.076	-0.070	-0.088	-0.077	-0.030	0.032	0.072	0.065	0.048	0.063	0.079	0.073	0.062	0.058
-0.280	-0.314	-0.300	-0.288	-0.349	-0.213	-0.201	-0.180	-0.221	-0.181	-0.166	-0.187	-0.201	-0.150	-0.105	-0.034	-0.012	-0.017	-0.039	-0.018	0.003	0.010	-0.003	0100
-0.380	-0.417	-0.393	-0.363	-0.472	-0.347	-0.309	-0.294	-0.340	-0.290	-0.284	-0.315	-0.308	-0.277	-0.255	-0.195	-0.184	-0.175	-0.205	-0.178	-0.146	-0.118	-0.102	-0.158
0.444	-0.489	-0.492	-0.479	-0.547	-0.788	-0.738	-0.684	-0.778	-0.669	-0.681	-0.601	-0.484	-0.621	-0.612	-0.577	-0.465	-0.426	-0.478	-0.430	-0.374	-0.322	-0.267	-0.376
-0.320	-0.357	-0.376	-0.383	-0.411	-0.677	-0.734	-0.786	-0.783	-0.786	-0.804	-0.819	-0.808	-0.834	-0.896	-1.014	-0.932	-0.760	-0.863	-0.766	-0.675	-0.606	-0.502	0.643
		-	1		-	1	-	1	_	ı		_	***	_		-	1	1	1		_	_	ı
0.000	-0.004	-0.015	-0.030	-0.033	-0.096	-0.121	0.140	-0.139	-0.141	-0.159	-0.180	-0.199	-0.158	-0.177	-0.203	-0.238	-0.227	-0.237	-0.228	-0.227	-0.234	-0.237	40.70
-0.020	-0.022	2.984	6.037	0.010	-0.027	-0.033	-0.015	-3.015	0.022	2.967	5.968	8.984	-0.016	-0.023	-0.031	-0.012	-0.012	-3.020	0.002	3.010	5.979	8.990	-0.026
1.251	1.200	1.200	007		75,5	\$75d		3	ş	<u></u>	ē	8	77	20	8	اء	آ اة	12	8	5	2	<u>=</u>	0.402
0000 0000 0000	-0.02 - 0.020 - 0.020 - 0.0444	-0.021 -0.006 - -0.360 -0.492 -0.022 -0.004 - -0.357 -0.489	-0.021 -0.006 - -0.350 -0.442 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492	-0.021 -0.066 - -0.350 -0.444 -0.021 -0.006 - -0.360 -0.492 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479	-0.021 -0.0320 -0.044 -0.021 -0.006 - -0.360 -0.492 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547	-0.021 -0.0320 -0.044 -0.021 -0.006 - -0.360 -0.492 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547 -0.027 -0.096 - -0.677 -0.788	-0.021 -0.066 -0.350 -0.444 -0.021 -0.006 - -0.360 -0.492 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547 -0.027 -0.096 - -0.677 -0.788 -0.033 -0.121 - -0.734 -0.738	-0.021 -0.036 -0.320 -0.444 -0.021 -0.006 - -0.360 -0.492 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547 -0.027 -0.096 - -0.677 -0.788 -0.033 -0.121 - -0.734 -0.738 -0.015 -0.140 - -0.786 -0.684	-0.021 -0.036 - -0.360 -0.444 -0.022 -0.006 - -0.360 -0.492 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547 -0.033 -0.121 - -0.734 -0.738 -0.015 -0.140 - -0.786 -0.684 -3.015 -0.139 - -0.783 -0.778	-0.021 -0.036 - -0.360 -0.444 -0.021 -0.006 - -0.360 -0.492 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547 -0.033 -0.121 - -0.734 -0.738 -0.015 -0.140 - -0.786 -0.684 -3.015 -0.139 - -0.783 -0.778 0.022 -0.141 - -0.786 -0.669	-0.021 -0.036 - -0.360 -0.444 -0.022 -0.006 - -0.360 -0.492 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547 -0.033 -0.121 - -0.677 -0.788 -0.015 -0.140 - -0.786 -0.684 -3.015 -0.139 - -0.786 -0.669 2.967 -0.159 - -0.804 -0.681	-0.021 -0.066 - -0.350 -0.444 -0.022 -0.006 - -0.357 -0.489 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547 -0.027 -0.096 - -0.677 -0.788 -0.033 -0.121 - -0.734 -0.738 -0.015 -0.140 - -0.786 -0.684 -3.015 -0.139 - -0.786 -0.669 2.967 -0.159 - -0.786 -0.669 2.967 -0.180 - -0.804 -0.681	-0.021 -0.036 - -0.320 -0.444 -0.022 -0.006 - -0.357 -0.489 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547 -0.027 -0.096 - -0.677 -0.78 -0.033 -0.121 - -0.74 -0.78 -0.015 -0.140 - -0.78 -0.684 -3.015 -0.139 - -0.78 -0.669 2.967 -0.180 - -0.804 -0.681 8.984 -0.199 - -0.808 -0.484	-0.025 -0.0360 -0.0360 -0.0444 -0.021 -0.006 - -0.357 -0.489 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547 -0.027 -0.096 - -0.677 -0.78 -0.033 -0.121 - -0.74 -0.78 -0.015 -0.140 - 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-0.804 -0.681 -0.016 -0.158 - -0.804 -0.621 -0.023 -0.177 - -0.896 -0.465 -0.012 -0.237 - -0.932 -0.465 -0.022 -0.227 <td>-0.025 -0.026 -0.026 -0.027 -0.0492 -0.021 -0.006 - -0.350 -0.492 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547 -0.027 -0.096 - -0.677 -0.78 -0.033 -0.121 - -0.74 -0.78 -0.015 -0.140 - -0.78 -0.69 -3.015 -0.141 - -0.78 -0.69 -0.022 -0.141 - -0.78 -0.69 -0.016 -0.180 - -0.804 -0.63 -0.02 -0.180 - -0.804 -0.61 -0.03 -0.13 - -0.804 -0.621 -0.03 -0.13 - -0.804 -0.465 -0.01 -0</td> <td>-0.021 -0.036 -0.320 -0.492 -0.021 -0.006 - -0.350 -0.489 -0.022 -0.004 - -0.357 -0.489 -0.037 -0.037 -0.492 -0.492 6.037 -0.030 - -0.376 -0.492 -0.010 -0.033 - -0.411 -0.479 -0.027 -0.096 - -0.677 -0.489 -0.033 -0.121 - -0.786 -0.684 -0.015 -0.140 - -0.786 -0.684 -0.015 -0.140 - -0.786 -0.684 -0.022 -0.140 - -0.786 -0.684 -0.022 -0.141 - -0.786 -0.681 8.984 -0.180 - -0.804 -0.681 -0.023 -0.177 - -0.808 -0.484 -0.031 -0.158 - -0.804 -0.612 -0.032 -0.134 -</td>	-0.025 -0.026 -0.026 -0.027 -0.0492 -0.021 -0.006 - -0.350 -0.492 -0.022 -0.004 - -0.357 -0.489 2.984 -0.015 - -0.376 -0.492 6.037 -0.030 - -0.383 -0.479 -0.010 -0.033 - -0.411 -0.547 -0.027 -0.096 - -0.677 -0.78 -0.033 -0.121 - -0.74 -0.78 -0.015 -0.140 - -0.78 -0.69 -3.015 -0.141 - -0.78 -0.69 -0.022 -0.141 - -0.78 -0.69 -0.016 -0.180 - -0.804 -0.63 -0.02 -0.180 - -0.804 -0.61 -0.03 -0.13 - -0.804 -0.621 -0.03 -0.13 - -0.804 -0.465 -0.01 -0	-0.021 -0.036 -0.320 -0.492 -0.021 -0.006 - -0.350 -0.489 -0.022 -0.004 - -0.357 -0.489 -0.037 -0.037 -0.492 -0.492 6.037 -0.030 - -0.376 -0.492 -0.010 -0.033 - -0.411 -0.479 -0.027 -0.096 - -0.677 -0.489 -0.033 -0.121 - -0.786 -0.684 -0.015 -0.140 - -0.786 -0.684 -0.015 -0.140 - -0.786 -0.684 -0.022 -0.140 - -0.786 -0.684 -0.022 -0.141 - -0.786 -0.681 8.984 -0.180 - -0.804 -0.681 -0.023 -0.177 - -0.808 -0.484 -0.031 -0.158 - -0.804 -0.612 -0.032 -0.134 -

Table 19. Continued

(b) Continued

					_	_																				
	.926	-0.058	-0.070	-0.068	-0.057	-0.079	-0.084	-0.094	-0.032	0.004	-0.034	0.001	0.023	0.026	0.013	0.030	0.061	0.102	0.163	0.157	0.151	0.155	0.157	0.140	0.123	0.148
	.853	-0.098	-0.099	-0.098	-0.092	-0.131	-0.107	-0.128	-0.061	-0.023	-0.065	-0.026	-0.002	0.004	-0.027	0.006	0.040	0.084	0.135	0.129	0.123	0.127	0.133	0.119	0.104	0.121
.50	622.	-0.148	-0.144	-0.143	-0.145	-0.198	-0.137	-0.158	960.0-	-0.057	-0.101	-0.061	-0.034	-0.033	-0.083	-0.025	0.013	0.063	0.106	0.099	0.092	0.097	0.104	960.0	0.082	0.092
vall at $z/Z = 0$.705	-0.202	-0.201	-0.200	-0.196	-0.233	-0.185	-0.175	-0.127	-0.089	-0.133	-0.092	-0.070	-0.080	-0.132	-0.057	-0.016	0.041	0.072	0.065	950.0	0.064	0.071	690'0	0.056	0.059
nozzle sidev of x/l of—	.558	-	ŀ	_		_	_	ı	t	1	-		1		1	-	1	1	-	_	-	_	-	-	-	-
Static pressure coefficients on nozzle sidewall at $z/Z = 0.50$ with values of x/l of—	.411	-0.407	-0.446	-0.443	-0.442	-0.428	-0.504	-0.445	-0.348	-0.320	-0.349	-0.315	-0.353	-0.400	-0.372	-0.304	-0.287	-0.221	-0.181	-0.176	-0.195	-0.178	-0.160	-0.146	-0.120	-0.158
ic pressure co	.337	-0.447	-0.492	-0.488	-0.506	-0.525	-0.546	-0.837	-0.846	861.0-	-0.855	982:0-	-0.748	-0.621	-0.510	-0.715	-0.670	-0.597	-0.464	-0.426	-0.462	-0.430	-0.405	-0.388	-0.338	-0.377
Stati	300	-0.316	-0.358	-0.354	-0.368	-0.385	-0.409	-0.671	-0.729	-0.778	-0.781	-0.777	-0.790	-0.814	-0.845	-0.827	-0.889	-1.002	-0.900	-0.734	-0.801	-0.739	-0.710	969.0-	-0.646	-0.621
	.226	-0.013	-0.025	-0.023	-0.040	-0.065	-0.055	-0.161	-0.194	-0.221	-0.218	-0.221	-0.239	-0.268	-0.304	-0.244	-0.270	-0.317	-0.369	-0.341	-0.360	-0.343	-0.340	-0.353	-0.362	-0.303
	.153	-0.002	-0.010	-0.007	-0.022	-0.046	-0.037	860.0-	-0.123	-0.143	-0.149	-0.145	-0.162	-0.191	-0.220	-0.160	-0.177	-0.205	-0.236	-0.223	-0.236	-0.225	-0.228	-0.245	-0.261	-0.202
	α, deg	-0.020	-0.021	-0.022	2.984	6.037	-0.010	-0.027	-0.033	-0.015	-3.015	0.022	2.967	5.968	8.984	-0.016	-0.023	-0.031	-0.012	-0.012	-3.020	0.002	3.010	5.979	8.990	-0.026
	M	1.251	1.198	1.200	1.200	1.200	1.150	0.952	0.924	0.900	0.900	0.900	0.901	0,901	0.900	0.877	0.850	0.800	0.701	0.601	0.602	0.600	0.601	0.602	0.601	0.402

Table 19. Continued

(b) Continued

	_	_		_	_	7	, .	_	_	_	_	_	,	_		_	_		_	_	_	_	-			
	.926	1	-		,			1	1	i	ı		1	1		1	ł		1					1		
	.853	-0.123	-0.120	-0.119	-0.105	-0.151	-0.123	40.104	-0.042	-0.013	-0.041	-0.013	-0.005	-0.014	-0.026	0.015	0.047	0.087	0.134	0.127	0.128	0.126	0.124	0.106	0.088	0.118
	<i>6LL</i> :	-0.170	-0.169	-0.168	-0.176	-0.238	-0.158	-0.126	-0.070	-0.042	-0.069	-0.043	-0.035	-0.048	-0.081	-0.00	0.024	990.0	0.104	0.097	0.097	0.095	0.095	0.079	0.059	1900
line	.705	-0.198	-0.215	-0.213	-0.230	-0.273	-0.205	-0.147	-0.098	-0.073	-0.100	-0.076	-0.073	-0.091	-0.147	-0.040	-0.005	0.044	0.075	990.0	0.067	0.065	0.064	0.051	0.031	0.064
Static pressure coefficients on nozzle sidewall at centerline with values of x/l of—	.632	-0.226	-0.249	-0.247	-0.265	-0.297	-0.257	-0.166	-0.127	-0.112	-0.136	-0.113	-0.116	-0.144	-0.217	-0.084	-0.042	0.011	0.036	0.033	0.033	0.031	0.030	0.019	0.001	0.030
nozzle sidev	.558	-0.264	-0.293	-0.291	-0.314	-0.346	-0.315	-0.199	-0.164	-0.167	-0.186	-0.167	-0.182	-0.220	-0.293	-0.140	-0.101	-0.035	-0.008	-0.010	-0.011	-0.012	-0.014	-0.023	-0.037	900
oefficients on nozzle sic with values of v/l of—	.484	-0.325	-0.356	-0.353	-0.372	-0.396	-0.402	-0.271	-0.233	-0.258	-0.266	-0.254	-0.279	-0.322	-0.352	-0.237	-0.205	-0.118	-0.072	-0.071	-0.072	-0.073	-0.075	-0.084	-0.094	40.064
tic pressure c	.411	-0.406	-0.442	-0.440	-0.438	-0.437	-0.498	-0.587	-0.412	-0.393	-0.402	686.0-	-0.406	-0.431	-0.400	-0.378	-0.369	-0.288	-0.175	-0.169	-0.170	-0.170	-0.174	-0.183	-0.189	-0.155
Sta	.337	-0.489	-0.541	-0.537	-0.540	-0.548	-0.603	-0.915	-0.907	-0.672	-0.739	-0.671	-0.636	-0.632	-0.562	-0.580	-0.572	-0.594	-0.425	-0.399	-0.405	-0.401	-0.409	-0.422	-0.427	-0.357
	.300	-0.384	-0.433	-0.429	-0.430	-0.436	-0.487	-0.776	-0.841	-0.889	-0.898	-0.889	-0.882	-0.887	-0.895	-0.912	-0.943	-1.032	-1.049	-0.859	-0.875	-0.863	-0.882	-0.912	-0.913	-0.725
	.226	-0.005	-0.023	-0.021	-0.031	-0.054	-0.057	-0.159	-0.191	-0.218	-0.223	-0.219	-0.220	-0.237	-0.269	-0.243	-0.270	-0.316	-0.373	-0.353	-0.359	-0.355	-0.361	-0.381	-0.403	-0.318
	.153	0.005	-0.010	-0.008	-0.021	-0.048	-0.038	-0.098	-0.124	-0.144	-0.152	-0.145	-0.151	-0.173	-0.209	-0.160	-0.178	-0.209	-0.237	-0.226	-0.232	-0.228	-0.234	-0.253	-0.281	-0.204
	α, deg	-0.020	-0.021	-0.022	2.984	6.037	-0.010	-0.027	-0.033	-0.015	-3.015	0.022	2.967	5.968	8.984	-0.016	-0.023	-0.031	-0.012	-0.012	-3.020	0.002	3.010	5.979	8.990	-0.026
	M∞	1.251	1.198	1.200	1.200	1.200	1.150	0.952	0.924	0.900	0.900	0.900	0.901	0.901	0.900	0.877	0.850	0.800	0.701	0.601	0.602	0.000	0.601	0.602	0.601	0.402

Table 19. Continued

(b) Concluded

Static pressurr .153 .226 .300 0.010 .0.011 .0.346 -0.011 .0.032 .0.392 -0.008 .0.030 .0.388	c pressu .300 0.346 0.392	00 e co	with values of x/l of— 337 .411 -0.4560.5090.506 -	of x/l of—	Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$ with values of x/l of— 300 337 411 558 7 60 60 60 70 70 70 70 70 70 70 70 70 70 70 70 70	-0.50 -0.224 -0.248 -0.246	.926 -0.090 -0.093 -0.093
-0.063		-0.386	-0.519 -0.538 -0.564	1 1 1	-0.355 -0.407	-0.286 -0.353 -0.245	-0.067 -0.097
0.033	$\dagger \dagger$	-0.716	-0.871 -0.923		-0.214	-0.096	-0.060
0.142	ऻऻॱ	-0.830	-0.903		-0.160	-0.072 -0.084	0.011
0.142	-0.221	-0.829	10.90		-0.159	-0.071	0.009
-0.14 -0.172	-0.242	-0.824	-1.001	1 1	-0.213	-0.107	-0.001
-0.224	-0.291	-0.859	899.0-		-0.298	-0.148	0.016
9 2 2	-0.244	-0.882 -0.952	-0.741	1 1	-0.101	-0.006	0.068
-0.208	Н	-1.073	-0.645	1	-0.038	0.040	0.103
0.233	-0.365	-0.989	10.404	1 1	-0.013	0.066	0.156
-0.224	T	-0.762	-0.378	1	-0.005	0.075	0.158
-0.224	-0.343	-0.802	-0.405	ı	-0.019	0.063	0.153
-0.238	-0.362	-0.883	-0.439	_	-0.035	0.051	0.145
-0.268	-0.395	-0.959	-0.483	-	-0.067	0.026	0.133
-i	-0.314 -0.440	-1.024	-0.528	l	-0.107	-0.001	0.125
0.20	-0.306	-0.672	-0.357	1	-0.017	0.000	0.140

Table 19. Continued

(c) Static pressure coefficients on nozzle bottom flap

	.926	-0.068	-0.071	-0.069	-0.068	-0.088	-0.076	-0.053	-0.033	-0.003	9000	9000	100	0100	0.014	0.025	0.058	0.107	0.168	0.162	0.163	0.161	0.142	0.121	0.102	0.154
	.853	-0.182	-0.169	-0.166	-0.097	-0.127	-0.154	-0.080	-0.066	-0.036	-0.018	-0.039	-0.049	-0.049	-0.037	0.004	0.033	0.088	0.140	0.133	0.142	0.133	0.108	0.081	0.057	0.126
= 0.75	671.	-0.269	-0.286	-0.282	-0.203	-0.340	-0.276	-0.113	-0.101	-0.071	-0.050	-0.073	-0.085	0600	-0.090	-0.038	0.003	0.063	0.109	0.102	0.117	0.100	0.073	0.041	0.012	0.095
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.75$.705	-0.305	-0.332	-0.330	-0.364	-0.411	-0.351	-0.149	-0.142	-0.110	-0.089	-0.112	-0.125	-0.136	-0.151	-0.079	-0.035	0.030	0.073	990.0	0.086	0.065	0.034	0.000	-0.031	0.059
nozzle botton	.558	-0.336	-0.372	-0.371	-0.407	-0.433	-0.415	-0.245	-0.224	-0.205	-0.190	-0.205	-0.224	-0.242	-0.280	-0.174	-0.135	-0.063	-0.020	-0.025	0.004	-0.026	1900	-0.097	-0.133	-0.024
fficients on nozzle bott	114.	-0.403	-0.448	-0.446	-0.438	-0.432	-0.498	-0.756	-0.411	-0.351	-0.334	-0.350	-0.379	-0.520	-0.653	-0.330	-0.316	-0.263	-0.198	-0.190	-0.150	-0.191	-0.232	-0.272	-0.310	-0.174
pressure coe	.337	-0.451	-0.500	-0.496	-0.502	-0.509	-0.556	-0.862	-0.883	-0.856	-0.812	-0.854	-0.885	-0.972	-1.000	-0.803	-0.766	-0.707	-0.477	-0.442	-0.363	-0.442	-0.506	-0.559	-0.604	-0.392
Static	.300	-0.318	-0.364	-0.361	-0.352	-0.353	-0.413	-0.677	-0.736	-0.784	-0.800	-0.784	-0.772	-0.769	-0.775	-0.835	-0.900	-1.019	-0.981	-0.791	-0.634	-0.790	-0.904	-0.990	-1.056	-0.664
	.226	-0.010	-0.033	-0.031	-0.031	-0.047	-0.061	-0.163	-0.199	-0.223	-0.258	-0.225	-0.209	-0.209	-0.222	-0.248	-0.276	-0.322	-0.376	-0.349	-0.325	-0.350	-0.370	-0.390	-0.409	-0.310
	.153	0.008	-0.014	-0.012	-0.023	-0.042	-0.038	-0.099	-0.127	-0.145	-0.166	-0.146	-0.140	-0.151	-0.173	-0.164	-0.182	-0.211	-0.242	-0.231	-0.225	-0.232	-0.243	-0.260	-0.282	-0.206
	α, deg	-0.020	-0.021	-0.022	2.984	6.037	-0.010	-0.027	-0.033	-0.015	-3.015	0.022	2.967	5.968	8.984	-0.016	-0.023	-0.031	-0.012	-0.012	-3.020	0.002	3.010	5.979	8.990	-0.026
	M	1.251	1.198	1.200	1.200	1.200	1.150	0.952	0.924	0.900	0.900	0.900	0.901	0.901	0.900	0.877	0.850	0.800	0.701	0.601	0.602	0.600	0.601	0.602	0.601	0.402

Fable 19. Continued

(c) Continued

-0.056 -0.067 -0.066 <u>-0.079</u> -0.059 -0.014 0.008 0.124 0.153 -0.075-0.094 -0.0070.053 0.103 0.165 0.165 0. 18 -0.041 0.017 .926 -0.01 -0.015 -0.0189.18 0.058 -0.074 -0.054-0.060 -0.0420.144 0.135 0.130 -0.136 -0.132-0.125-0.128-0.086-0.045 -0.035 -0.047-0.0120.025 0.083 0.143 0.108 -0.101 0.081 -0.137.853 -0.148-0.227 -0.093 -0.099 -0.012 0.056 0.112 0.104 0.119 0.097 -0.291 -0.124-0.112 -0.083 -0.073-0.085 -0.053-0.2830.103 0.040 *6LL*: Static pressure coefficients on nozzle bottom flap at y/Y = 0.50-0.336-0.426 -0.126 -0.134-0.159 -0.054 0.076 0.066 -0.365 -0.388-0.153-0.125-0.0950.068 -0.0040.063 -0.363-0.319-0.167-0.150-0.117 -0.031705 0.021 -0.458 -0.473 -0.279 -0.242 -0.233 -0.227 -0.230 -0.255 -0.202 -0.170 -0.023 -0.030 -0.136-0.030 -0.439 -0.224 -0.0890.003 -0.108-0.397-0.437-0.477with values of x/l of -0.291 -0.031.558 -0.455 -0.348 -0.352 -0.162-0.326 -0.495 -0.558-0.772-0.385-0.350-0.387-0.353-0.365-0.449-0.326-0.209 -0.257 -0.296-0.651 -0.208-0.210-0.501<u>4</u>. -0.600 -0.536-0.659 -0.926-0.420 -0.491 -0.540 -0.5000.544 -0.635-0.593-0.912-0.710-0.574-0.628-0.402-0.473-0.597-0.472-0.5410.541 -1.031 -0.531-0.537.337 -0.419 -0.887 -0.862-0.862-0.841 -0.705-0.373-0.405-0.472-0.821 -0.860-0.858 -0.900 -1.055 -1.079-0.727-1.151-0.422-0.413-0.762-0.961 -1.112-0.841300 -0.248 -0.236 -0.219 -0.210 -0.205 -0.021 -0.018 -0.076 -0.076 -0.087 -0.008 -0.056 -0.105-0.086 -0.084 -0.084 -0.205-0.083-0.027 -0.173-0.211-0.091 .226 -0.165 -0.150 -0.169 -0.258 -0.272 -0.234 -0.013-0.135-0.256-0.238 -0.274-0.012-0.012-0.033-0.103 -0.130 -0.148-0.127-0.115 -0.223-0.2650.000 -0.01 .153 α, deg -0.016 3.010 -0.0202.984 6.037 -0.010 -0.0150.022 2.967 5.968 8.984 -0.023-0.012-0.012-3.020 0.002 5.979 8.990 -0.026-0.022-0.033-3.015-0.027-0.031-0.0210.900 0.850 0.402 1.198 ...5 0.952 0.900 0.900 0.602 0.600 1.200 0.602 1.200 0.877 × 1.251 0.901 0.901 0.701 0.601 0.601 0.601

Table 19. Continued

(c) Concluded

-0.063 -0.083 -0.047 -0.100-0.080-0.060 -0.042 -0.014 -0.025 -0.039 0.016 926 -0.006 0.104 -0.0170.167 0.169 0.146 -0.011 0.051 0.167 0.108 0.158-0.408 -0.429 -0.169 -0.427 -0.242-0.132 -0.125 -0.133-0.146 -0.175-0.160-0.175 -0.064 .705 -0.1020.012 0.061 0.059 -0.009 0.034 0.071 Static pressure coefficients on nozzle bottom flap at centerline -0.492 -0.490 -0.491 -0.489 -0.536 -0.277 -0.240 -0.453-0.224-0.234 -0.224 -0.229 -0.262 -0.293 -0.201 90.100 .558 -0.173-0.032 -0.041 -0.009 -0.043 -0.118-0.1430.04 with values of x/l of--0.462-0.510-0.507 -0.336 -0.386 -0.568 -0.513 -0.566-0.365-0.336-0.368-0.339 -0.333 -0.335 -0.328 -0.752-0.234-0.235 -0.236 -0.282 -0.318 <u>4</u>. -0.217-0.529-0.527 -0.586 -0.515 -0.478-0.626-0.535-0.600 -0.531-0.901-0.522-0.661 -0.627 -0.494-0.440 -0.554-0.628 -0.436 .337 -0.501 -0.521 -0.951 -0.850 -0.878 -0.379-0.429 -0.428-0.425 -0.779 -0.826-0.846 -0.866 -0.884 -0.956 -0.853-1.129-1.128 -0.879-0.421 -0.481 -1.054-0.799-0.881 -0.971 -0.737-0.016 -0.038-0.036 -0.219 -0.245 -0.252 -0.064 -0.246 -0.235 -0.224 -0.210 -0.272 -0.305 -0.033-0.036.226 -0.191 -0.363-0.427 -0.457 -0.451-0.480-0.427-0.379-0.010 -0.036 0.00 -0.013-0.013 -0.112 -0.159 -0.167-0.160-0.149 -0.139-0.124 -0.200 -0.281 -0.257 -0.282 -0.299 -0.305 .153 -0.303-0.258-0.011 -0.137-0.287α, deg -0.0202.984 0.010 -0.015 -3.015 -0.022 6.037 -0.027-0.0332.967 5.968 8.984 -0.016 -0.023 -0.031 8.990 -0.021 -0.0123.010 -0.012-3.020 0.002 5.979 1.198 1.200 1.200 0.952 \mathbf{z}_{8} 0.900 0.900 0.900 1.251 0.901 0.850 0.800 0.600 0.901 0.601 0.602 0.602 0.402 0.701 0.601 0.601

Table 19. Concluded

(d) Force data

 M_{∞} α , deg
 CD

 1.251
 -0.020 0.2654

 1.198
 -0.021 0.2885

 1.200
 -0.022 0.2868

 1.200
 2.984 0.2805

 1.200
 2.984 0.2805

 1.200
 2.984 0.2805

 1.200
 2.984 0.2805

 1.200
 -0.010 0.3115

 0.952 -0.010 0.2105

 0.952 -0.015 0.2040

 0.900 -3.015 0.2040

 0.900 -3.015 0.2040

 0.900 -3.015 0.2040

 0.900 -3.015 0.2040

 0.901 2.967 0.2040

 0.901 2.967 0.2040

 0.807 -0.016 0.1616

 0.800 -0.023 0.1616

 0.800 -0.023 0.1616

 0.601 -0.012 0.0593

 0.602 -0.012

Table 20. Pressure and Force Data for Nozzle 12 With $\beta_{l,top/bot} = 15.0^{\circ}/\beta_{l,side} = 22.4^{\circ}$, Plume On, and $\alpha = 0^{\circ}$

(a) Static pressure coefficients on nozzle top flap

			_	_			~		\ <u>\</u>	_	<u> </u>		_			
	.926	0.221	0.223	0.137	-0.022	9.0	990.0	-0.058	-0.045	-0.013	0.022	0.050	0.128	0.217	0.218	0.211
	.853	0.189	0.191	0.114	-0.052	-0.066	-0.095	-0.086	-0.072	-0.041	9000	0.024	0.104	0.186	0.185	0.177
	<i>6LL</i> :	0.153	0.155	0.087	-0.073	-0.088	-0.117	-0.102	-0.096	-0.068	-0.036	-0.007	0.075	0.153	0.150	0.142
line	.705	0.107	0.111	0.050	-0.095	-0.107	-0.136	-0.126	-0.123	-0.098	-0.066	-0.041	0.043	0.111	0.108	0.098
Static pressure coefficients on nozzle top slap at centerline with values of x/l of—	.632	0.061	0.063	0.009	-0.177	-0.145	-0.163	-0.151	-0.150	-0.129	-0.100	820.0-	0.001	0.063	090.0	0.056
efficients on nozzle top with values of x/l of—	.558	0.000	0.002	-0.048	-0.402	-0.426	-0.335	-0.186	-0.182	-0.164	-0.142	-0.122	-0.058	0.003	0.000	-0.001
coefficients o	.484	-0.079	-0.079	-0.132	-0.405	-0.446	-0.501	-0.255	-0.224	-0.208	-0.193	-0.178	-0.136	-0.077	-0.078	-0.078
itic pressure	.411	-0.201	-0.205	-0.264	-0.459	-0.500	-0.559	-0.456	-0.300	-0.277	-0.264	-0.261	-0.265	-0.202	-0.201	-0.187
Stz	.337	-0.456	-0.485	-0.564	-0.466	-0.517	-0.572	-0.863	-0.573	-0.462	-0.427	-0.431	-0.537	-0.481	-0.454	-0.403
	.300	-0.859	-1.117	-1.126	-0.377	-0.426	-0.474	-0.772	-0.823	-0.843	-0.854	-0.886	-1.079	-1.122	-0.849	-0.707
	.226	1	1	1	l	1	1	l	ı	1	1	ŀ	1	1	ı	1
	.153	-0.270	-0.280	-0.222	0.002	-0.007	-0.026	-0.096	-0.128	-0.147	-0.166	-0.183	-0.223	-0.278	-0.270	-0.245
	M∞	0.597	0.698	0.799	1.252	1.198	1.151	0.953	0.923	0.899	0.874	0.853	0.802	0.703	0.599	0.402

	7	Т	T	Γ	Γ	Г	Γ	Γ	Π	Γ	Γ	Ι			J	Γ
	.926	0.222	0.222	0.138	-0.029	0.0 4	-0.070	-0.057	-0.043	-0.013	0.020	0.051	0.129	0.218	0.218	0.212
	.853	0.188	0.193	0.116	-0.055	-0.069	-0.095	-0.081	-0.071	0.040	-0.007	0.024	0.106	0.188	0.186	0.181
0.25	<i>6LL</i> :	0.152	0.157	0.087	-0.076	-0.090	-0.119	-0.101	-0.094	-0.067	-0.035	-0.006	0.077	0.153	0.151	0.146
lap at $y/Y = 0$	705	0.109	0.113	0.050	-0.100	-0.111	-0.143	-0.127	-0.121	-0.096	-0.068	-0.042	0.043	0.112	0.107	0.101
nozzle top f	.558	0.000	0.002	-0.050	-0.404	-0.434	-0.429	-0.183	-0.181	-0.164	-0.142	-0.121	-0.057	0.004	0.001	-0.001
Defficients on nozzle to	.411	-0.195	-0.196	-0.262	-0.457	-0.500	-0.557	-0.492	-0.304	-0.279	-0.266	-0.261	-0.262	-0.195	-0.194	-0.182
Static pressure coefficients on nozzle top flap at $y/Y = 0.25$.337	-0.447	-0.475	-0.561	-0.467	-0.516	-0.572	-0.871	-0.604	-0.476	-0.437	-0.441	-0.541	-0.474	-0.446	-0.398
Stat	.300	-0.865	-1.127	-1.126	-0.371	-0.418	-0.470	-0.764	-0.822	-0.850	-0.868	-0.906	-1.086	-1.126	-0.858	-0.712
	.226	-0.406	-0.429	-0.337	-0.008	-0.023	-0.048	-0.163	-0.200	-0.226	-0.254	-0.278	-0.334	-0.427	-0.405	-0.359
	.153	-0.263	-0.271	-0.216	900.0	-0.002	-0.023	0.093	-0.124	-0.145	-0.165	-0.181	-0.216	-0.270	-0.261	-0.238
	M∞	0.597	0.698	0.799	1.252	1.198	1.151	0.953	0.923	0.899	0.874	0.853	0.802	0.703	0.599	0.402

Table 20. Continued

(a) Concluded

	.926	0.220	0.221	0.141	-0.027	-0.043	-0.066	-0.058	-0.042	-0.013	0.022	0.052	0.129	0.216	0.215	0.207
	.853	0.187	0.189	0.115	-0.056	-0.069	-0.095	-0.085	-0.072	-0.041	-0.006	0.024	0.106	0.185	0.183	0.177
.50	6 <i>LL</i> :	0.149	0.153	0.087	-0.077	-0.092	-0.118	-0.105	660'0-	-0.069	-0.036	-0.006	0.078	0.151	0.149	0.143
Static pressure coefficients on nozzle top flap at $y/Y = 0.50$ with values of v/I of—	.705	0.113	0.113	0.051	-0.108	-0.116	-0.143	-0.127	-0.125	-0.100	-0.067	-0.040	0.045	0.112	0.111	0.108
nozzle top fi	.558	0.010	0.008	-0.044	-0.380	-0.417	-0.463	-0.190	-0.179	-0.166	-0.141	-0.119	-0.051	0.008	0.011	0.013
efficients on nozzle top with values of 1/1 of—	.411	-0.179	-0.182	-0.248	-0.438	-0.481	-0.536	-0.446	-0.305	-0.282	-0.270	-0.264	-0.249	-0.181	-0.176	-0.162
c pressure co	.337	-0.429	-0.453	-0.557	-0.472	-0.522	-0.578	-0.878	-0.643	-0.500	-0.463	-0.464	-0.541	-0.451	-0.424	-0.377
Stati	300	-0.843	-1.078	-1.129	-0.372	-0.417	-0.469	-0.764	-0.826	698 0	-0.900	-0.937	-1.092	-1.079	-0.839	-0.701
	.226	-0 384	-0.405	-0.326	6000	-0.022	-0.048	-0.157	-0.195	20.02	-0.251	-0.275	-0.324	0.406	-0.385	-0.342
	.153	-0.248	-0.253	-0.210	0.003	-0002	7,000	1600	-0.123	-0.143	-0.162	-0.177	-0.208	-0.254	-0.246	-0.225
	N	0.507	0.698	0 799	1 252	1 198	1 151	0.053	0.003	0080	0.874	0.853	0.802	0.703	0 509	0.402

		_	_		_	_			_	_		_	-	_	_		_
	.926	800.0	0.500	0.215	0.143	-0.017	-0.034	-0.051	-0.058	-0.042	-0.011	0.024	0.054	0.132	0.211	0.203	0.197
	.853	0 100	0.102	0.186	0.118	-0.040	-0.059	-0.083	-0.084	-0.068	-0.037	-0.002	0.028	0.108	0.182	0.178	0.174
.75	179 l	0 150	0.130	0.151	0.087	-0.066	-0.083	-0.107	-0.117	860:0-	-0.068	-0.035	-0.005	0.079	0.149	0.148	0.144
$ap\ at\ y/Y=0$	705	31.0	0.113	0.110	0.050	-0.144	-0.120	-0.138	-0.156	-0.127	-0.100	-0.067	-0.038	0.041	0.108	0.112	0.109
nozzle top fl	.558	,,,,,	0.010	9000	-0.058	-0.347	-0.388	-0.441	-0.256	-0.200	-0.175	-0.147	-0.121	-0.067	0.005	0.017	0.015
efficients on nozzle top	411		-0.138	-0.163	-0.230	-0.404	-0.444	-0.500	-0.380	-0.324	-0.299	-0.280	-0.273	-0.232	-0.163	-0.155	-0.147
Static pressure coefficients on nozzle top flap at $y/Y = 0.75$	337	, ,	-0.406	-0.422	-0.479	-0.480	-0.533	-0.591	-0.638	-0.498	-0.456	-0.437	-0.445	-0.470	-0.418	-0.401	-0.360
Stati	300	SOC:	-0.867	-1.050	-1.013	-0.353	-0.398	-0.453	-0.731	-0.785	-0.811	-0.830	-0.863	-0.973	-1.040	-0.855	-0.719
	126	0777	-0.352	-0.364	-0.303	-0.005	-0.018	-0.051	-0.151	-0.187	-0.214	-0.238	-0.259	-0.303	-0.363	-0.348	-0.315
	153	66:	-0.225	-0.230	-0.198	0.002	-0.002	-0.034	1000	1210	-0.141	-0 159		-0.195	-0.230		
	*	8/4/	0.597	0.698	0.799	1 252	1 198	1511	0.053	0.073	0800	0.874	0.853	0.802	0.703	0 500	0.402

Table 20. Continued

(b) Static pressure coefficients on nozzle sidewall

			Static pres	sure coefficie	ents on corne	r between noz	Static pressure coefficients on corner between nozzle top flap and sidewall	ind sidewall		
					with value	with values of x/l of-				
M_{∞}	.153	.226	.300	.337	114.	.558	.705	<i>6LL</i> :	.853	.926
0.597	-0.223	-	-0.906	-0.422	-0.139	0.036	0.117	0.150	0.174	0.195
0.698	-0.228	ı	-1.060	-0.413	-0.147	9000	0.108	0.146	0.178	0.203
0.799	-0.196	ı	-0.935	-0.409	-0.237	-0.085	0.033	0.078	0.114	0.142
1.252	0.004	1	-0.335	-0.512	-0.406	-0.332	-0.163	-0.055	-0.025	-0.003
1.198	-0.003	1	-0.377	-0.568	-0.447	-0.374	-0.126	-0.067	-0.048	-0.030
1.151	-0.034	1	-0.434	-0.630	0.500	-0.427	-0.128	-0.091	-0.067	-0.060
0.953	-0.091	1	-0.693	-0.500	-0.359	-0.276	-0.190	-0.145	-0.103	-0.067
0.923	-0.121	1	-0.732	-0.423	-0.322	-0.227	-0.143	-0.106	-0.075	-0.043
0.899	-0.142	1	-0.745	-0.392	-0.306	-0.197	-0.108	-0.071	-0.040	-0.013
0.874	-0.156	1	-0.758	-0.376	-0.290	-0.169	-0.070	-0.032	-0.001	0.026
0.853	-0.170	1	-0.796	-0.387	-0.287	-0.142	-0.040	-0.001	0.032	0.056
0.802	-0.196	1	-0.899	-0.400	-0.235	-0.092	0.025	0.069	0.106	0.133
0.703	-0.227	ı	-1.051	-0.410	-0.144	0.003	0.104	0.141	0.173	0.199
0.599	-0.225	ı	-0.888	-0.415	-0.134	0.037	0.116	0.143	0.169	0.192
0.402	-0.208	1	-0.752	-0.379	-0.127	0.040	0.114	0.143	0.167	0.187

	.926	0.198	0.205	0.148	0.033	0.013	0.013	-0.055	-0.023	0.013	0.048	0.077	0.141	0.202	0.195	0 102
		H	-		\vdash				H	\vdash		H	-	_		H
	.853	0.174	0.180	0.115	-0.014	-0.035	-0.049	-0.099	-0.066	-0.027	0.012	0.042	0.109	0.175	0.172	0.170
0.50	622.	0.148	0.146	0.071	-0.059	-0.063	-0.083	-0.147	-0.111	-0.072	-0.031	0.001	0.065	0.140	0.144	0.150
wall at $z/Z =$.705	0.119	0.104	0.018	-0.138	-0.120	-0.128	-0.193	-0.153	-0.117	-0.080	-0.049	200'0	960'0	0.115	0.122
nozzle side	.558	1	1	**	-	-	1	1	ı	1	-	_	-	1	1	1
Static pressure coefficients on nozzle sidewall at $z/Z = 0.50$ with values of x/I of—	.411	-0.125	-0.171	-0.233	-0.460	-0.502	-0.558	-0.345	-0.302	-0.289	-0.280	-0.280	-0.237	-0.168	-0.120	-0.122
tic pressure o	.337	-0.442	-0.369	-0.360	-0.549	-0.604	-0.670	-0.455	-0.387	-0.363	-0.355	-0.372	-0.349	-0.360	-0.436	-0.413
Sta	.300	-0.970	-1.038	-0.865	-0.359	-0.407	-0.463	-0.711	-0.705	-0.698	-0.715	-0.752	-0.828	-1.018	-0.949	-0.814
	.226	-0.349	-0.346	-0.294	-0.001	-0.017	-0.053	-0.149	-0.183	-0.209	-0.233	-0.252	-0.291	-0.344	-0.347	-0.316
	.153	1	1	1	1	ı	-			1		!	1		1	ı
	M∞	0.597	0.698	0.799	1.252	1.198	1.151	0.953	0.923	0.899	0.874	0.853	0.802	0.703	0.599	0.402

Table 20. Continued

(b) Concluded

	200	.920	1	ı	ı			1	ı			1	i		1	ı			j	t		1	
	250	.833	0.173	0.181	0.115	COCO	70.07	-0.018	-0.026	001	0.100	-0.066	0600	7.07	0.012	0.045	00	0.100	0.177	1710		0.170	
		.779	0.147	0.149	0.073	6.0.0	00.0-	-0.053	-0.067	0710	70.140	-0.116	9200	20.070	-0.036	-0.003	3000	0.005	0.141	0 142	71.0	0.148	
ine		.705	0.119	0 104	7100	710.0	-0.115	901.0	-0.116	20.00	-0.1%	-0.161	2010	-0.120	-0.088	0.057	1000	0.000	0.097	2110	0.113	0.124	
Static pressure coefficients on nozzle sidewall at centerline		.632	0.083	0.042	210.0	-0.057	-0.185	-0.186	9810	-0.100	-0.237	-0.199	01.0	-0.172	-0.145	0 110	-0.110	-0.065	0.038	0200	0.0/9	0.096	
nozzle sidev	of x/l of—	.558	0.044	0.037	/ co.o_	-0.131	-0.275	-0.295	0 308	-0.200	-0.269	70 736	0.00	-0.218	-0 100	107	70.107	-0.137	0.47	2,000	0.030	0.058	
oefficients on	with values of x/l of—	.484	0.017	0.10	-0.130	-0.194	-0.409	-0 446	203.0	7000-	-0.284	0.255	0.433	-0.246	20 336	0000	-0.228	-0.196	0 133	001.0	-0.019	-0.006	
ic pressure c		.411	1110	0.10	-0.199	-0.223	-0.518	895 0	0.200	-0.630	-0.300	0.061	-0.201	-0.257	0.250	2020	-0.250	-0.215	201.0	-0.17/	-0.107	-0.113	
Stat		337	0.400	-0.463	-0.256	-0.229	-0.565	0.623	-0.023	-0.689	-0.372	7000	-0.230	-0.284	1.00	1/7.0-	-0.267	-0.225	27.0	-0.243	-0.468	-0.479	
		300	2000	-0.886	-0.776	-0.690	-0.356	2000	-0.40 4	-0.460	-0 691	1000	-0.0/8	-0 684	9000	-0.000	-0.694	C89 U	200.0	-0.722	0.870	-0.767	: 3
		226	077	-0.380	-0.366	-0.307	0.003	0.00	-0.024	-0.061	0 156	001.0	-0.192	0.210	27.02	-0.245	-0.263	0.305	COC.O	-0.360	-0.374	-0.352	10:00
		152	CCI.	-0.232	-0.225	-0.192	6100	0.012	-0.000	-0.038	0000	-0.072	-0.120	0 130	-0.137	-0.155	-0.168	2010	-0.192	-0.225	-0.231	-0.216	10.410
		`	Μ∞	0.597	869.0	0 799	0301	1.222	1.198	1.151	0.00	0.933	0.923	000	0.699	0.874	0.853	2000	0.802	0.703	0 500	040	704.0

		Static	c pressure co	Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$	nozzle sidew	all at $z/Z = -$	0.50	
				with values of x/l of—	—jo <i>1/x</i> jo			
Ž	153	226	300	.337	.411	.558	.705	.926
80.7	0220	-0.343	-1 026	-0.437		0.040	0.116	0.197
0.509	027.0	-0.339	-1.145	-0.381	1	-0.012	0.105	0.204
0.070	7177	-0.285	-0.802	-0.332		-0.122	0.014	0.149
1 252	0016	0.000	-0.336	-0.562		-0.346	-0.145	0.023
7071	0.010	-0.019	-0.386	-0.619		-0.376	-0.112	0.002
1.170	0.002	0.052	-0.438	-0.685	1	-0.405	-0.123	0.001
1.131	0.007	0.02	8290-	-0.356		-0.268	-0.208	-0.062
0.933	-0.002	0810	0.578	-0.271	1	-0.240	-0.177	-0.030
0.923	0.11.0	0.203	0.575	9500		-0.229	-0.143	0.008
0.899	-0.131	-0.203	0050	0.752		-0.208	-0.103	0.045
0.8/4	-0.151	-0.227	00,00	0.057		-0 188	690 0-	0.076
0.853	-0.163	-0.240	-0.02U	-0.407		201.0	100	0 130
0.802	-0.187	-0.284	-0.772	-0.323	1	-0.128	0.00/	0.139
0.703	-0.214	-0 338	-1.121	-0.376	ı	-0.017	0.101	0.199
0.70	712.0	0 342	-1 011	-0.430	1	0.038	0.114	0.192
0.399	0.200	0.212	0.863	-0.406	1	0.043	0.122	0.186
0.407	707.0-	15.7	Coo.o.	0.400				

Table 20. Continued

(c) Static pressure coefficients on nozzle bottom flap

	т-	$\overline{}$	_	т —	_	_	_	_	_	-	_	_	_	_	_	_
	.926	0.207	0.214	0.160	-0.001	-0.015	-0.032	-0.029	0.002	0.032	7900	0.093	0.155	0.210	0 203	0.197
	.853	0.179	0.183	0.129	-0.027	-0.040	-0.063	-0.092	-0.052	1100	0.027	0.056	0.120	0.179	0.174	0.169
= 0.75	671.	0.146	0.147	0.000	-0.061	-0.067	-0.090	-0.155	-0.113	-0.062	-0.018	0.014	0.082	0.145	0.145	0.141
n flap at y/Y	705	0.109	0.106	0.045	-0.199	-0.119	-0.129	-0.215	-0.175	-0.123	-0.076	-0.039	0.034	0.102	0.106	0.101
icients on nozzle botton with values of x/l of—	.558	0.013	0.002	-0.073	-0.368	-0.410	-0.457	-0.280	-0.261	-0.235	-0.196	-0.162	-0.083	-0.001	0.011	0.007
Static pressure coefficients on nozzle bottom flap at $y/Y = 0.75$ with values of x/I of—	.411	-0.159	-0.166	-0.243	-0.407	-0.449	-0.501	-0.337	-0.293	-0.294	-0.293	-0.288	-0.249	-0.166	-0.159	-0.150
pressure coe	.337	-0.397	-0.413	-0.455	-0.472	-0.523	-0.583	-0.471	-0.373	-0.366	-0.370	-0.391	-0.445	-0.410	-0.394	-0.357
Static	.300	-0.900	-1.090	-0.929	-0.394	-0.445	-0.503	-0.748	-0.688	289 .0–	-0.710	-0.754	-0.897	-1.086	-0.894	-0.755
	.226	-0.340	-0.351	-0.292	-0.001	-0.020	-0.053	-0.148	-0.184	-0.209	-0.231	-0.250	-0.291	-0.352	-0.341	-0.310
	.153	-0.218	-0.223	-0.189	0.015	-0.006	-0.035	-0.085	-0.115	-0.134	-0.149	-0.162	-0.188	-0.221	-0.217	-0.198
	M_{∞}	0.597	0.698	0.799	1.252	1.198	1.151	0.953	0.923	0.899	0.874	0.853	0.802	0.703	0.599	0.402

M _∞ .153 .226 .300 .337 0.597 -0.022 -0.373 -0.786 -0.416 0.698 -0.021 -0.396 -0.957 -0.445 0.799 -0.020 -0.326 -1.136 -0.562 1.252 0.034 -0.003 -0.384 -0.459 1.198 0.021 -0.024 -0.431 -0.567 1.151 -0.004 -0.024 -0.486 -0.567 0.953 -0.010 -0.163 -0.486 -0.567 0.923 -0.010 -0.163 -0.843 -0.670 0.899 -0.020 -0.197 -0.843 -0.670 0.874 -0.020 -0.228 -0.843 -0.542 0.873 -0.020 -0.223 -0.942 -0.542 0.883 -0.020 -0.275 -0.986 -0.542 0.703 -0.020 -0.275 -0.986 -0.553 0.703 -0.023 -0.958 -0.444	0.000				2.5		
.153 .226 .300 -0.022 -0.373 -0.786 -0.021 -0.396 -0.957 -0.020 -0.326 -1.136 -0.034 -0.003 -0.384 -0.041 -0.024 -0.431 -0.004 -0.058 -0.486 -0.010 -0.163 -0.777 -0.017 -0.163 -0.843 -0.020 -0.228 -0.843 -0.020 -0.228 -0.895 -0.020 -0.228 -0.986 -0.020 -0.253 -0.942 -0.020 -0.253 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986		with value	with values of x/l of-)		
-0.022 -0.373 -0.786 -0.021 -0.396 -0.957 -0.020 -0.326 -1.136 0.034 -0.003 -0.384 0.021 -0.024 -0.431 -0.004 -0.058 -0.486 -0.010 -0.163 -0.777 -0.017 -0.197 -0.843 -0.020 -0.228 -0.895 -0.020 -0.253 -0.942 -0.020 -0.253 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986	.300	.411	.558	.705	677.	.853	.926
-0.021 -0.396 -0.957 -0.020 -0.326 -1.136 0.034 -0.003 -0.384 0.021 -0.024 -0.431 -0.004 -0.058 -0.486 -0.010 -0.163 -0.777 -0.017 -0.197 -0.843 -0.020 -0.228 -0.895 -0.020 -0.253 -0.942 -0.020 -0.253 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986		-0.181	-0.001	0.105	0.145	0.179	0.213
-0.020 -0.326 -1.136 0.034 -0.003 -0.384 0.021 -0.024 -0.431 -0.004 -0.058 -0.486 -0.010 -0.163 -0.777 -0.017 -0.197 -0.843 -0.020 -0.228 -0.895 -0.020 -0.253 -0.942 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986		-0.189	-0.002	0.105	0.148	0.185	0.221
0.034 -0.003 -0.384 0.021 -0.024 -0.431 -0.004 -0.058 -0.486 -0.010 -0.163 -0.777 -0.017 -0.197 -0.843 -0.020 -0.228 -0.895 -0.020 -0.253 -0.942 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986		-0.242	-0.051	0.057	0.099	0.136	0.168
0.021 -0.024 -0.431 -0.004 -0.058 -0.486 -0.010 -0.163 -0.777 -0.017 -0.197 -0.843 -0.020 -0.228 -0.895 -0.020 -0.253 -0.942 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986		-0.449	-0.394	-0.146	-0.067	-0.032	-0.00¢
-0.004 -0.058 -0.486 -0.010 -0.163 -0.777 -0.017 -0.197 -0.843 -0.020 -0.228 -0.895 -0.020 -0.253 -0.942 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986 -0.020 -0.275 -0.986		-0.494	-0.431	-0.112	-0.071	-0.043	-0.017
-0.010 -0.163 -0.777 -0.017 -0.197 -0.843 -0.020 -0.228 -0.895 -0.020 -0.253 -0.942 -0.020 -0.275 -0.986 -0.020 -0.275 -1.109 -0.023 -0.038 -0.958		-0.550	-0.478	-0.132	-0.096	-0.065	-0.038
-0.017 -0.197 -0.843 -0.020 -0.228 -0.895 -0.020 -0.253 -0.942 -0.020 -0.275 -0.986 -0.020 -0.322 -1.109 -0.023 -0.398 -0.958		-0.408	-0.250	-0.157	-0.103	-0.049	10.00
-0.020 -0.228 -0.895 -0.020 -0.253 -0.942 -0.020 -0.275 -0.986 -0.020 -0.322 -1.109 -0.023 -0.398 -0.958		-0.342	-0.224	-0.119	-0.069	-0.021	0.015
-0.020 -0.253 -0.942 -0.020 -0.275 -0.986 -0.020 -0.322 -1.109 -0.023 -0.398 -0.958		-0.319	-0.187	-0.082	-0.038	0.000	0.032
-0.020 -0.275 -0.986 -0.020 -0.322 -1.109 -0.023 -0.398 -0.958		-0.305	-0.156	-0.046	-0.003	0.033	0.066
-0.020 -0.322 -1.109 -0.023 -0.398 -0.958		-0.292	-0.127	-0.017	0.024	0.061	0.094
-0.023 -0.398 -0.958		-0.246	-0.058	0.048	0.091	0.128	0.162
	-0.958	-0.189	-0.005	0.102	0.145	0.182	0.217
0.599 -0.021 -0.373 -0.782 -0.415		-0.182	-0.003	0.103	0.144	0.178	0.210
0.402 -0.019 -0.333 -0.667 -0.371	199.0-	-0.172	-0.006	0.097	0.137	0.172	0.203

Table 20. Concluded

(c) Concluded

	.926	0.225	0.229	0.178	-0.010	-0.022	-0.046	0.006	0.013	0.028	0.067	0.096	0.167	0.225	0.219	0.213
rline	.705	0.094	0.097	0.062	-0.126	-0.125	-0.143	-0.101	-0.087	-0.076	-0.045	-0.015	0.056	0.099	0.094	0.084
flap at cente	.558	-0.015	-0.012	-0.046	-0.424	-0.459	-0.463	-0.196	-0.171	-0.173	-0.154	-0.127	-0.055	-0.013	-0.015	-0.020
ozzle botton	.411	-0.203	-0.213	-0.277	-0.433	-0.480	-0.537	-0.723	-0.400	-0.356	-0.343	-0.336	-0.291	-0.211	-0.204	-0.192
Static pressure coefficients on nozzle bottom flap at centerline with values of x/l of—	.337	-0.432	-0.467	-0.647	-0.447	-0.500	-0.558	-0.877	-0.909	-0.694	-0.592	-0.587	-0.631	-0.465	-0.431	-0.381
pressure coe	.300	-0.811	-1.003	-1.182	-0.388	-0.440	-0.494	-0.795	-0.866	-0.920	-0.962	-1.007	-1.156	-1.029	-0.818	-0.694
Static	.226	-0.389	-0.417	-0.348	-0.012	-0.035	-0.066	-0.182	-0.213	-0.239	-0.263	-0.288	-0,343	-0.417	-0.390	-0.346
	.153	-0.265	-0.276	-0.230	9000	-0.012	-0.040	-0.109	-0.135	-0.158	-0.176	-0.190	-0.228	-0.271	-0.263	-0.240
	M	0.597	0.698	0.799	1.252	1.198	1.151	0.953	0.923	0.899	0.874	0.853	0.802	0.703	0.599	0.402

(d) Force data

c_{Df}	0.0115	0.0112	0.0110	0.0102	0.0103	0.0104	0.0107	0.0108	0.0108	0.0109	0.0109	0.0110	0.0113	0.0115	0.0123
$c_{D,p}$	0.0567	0.0732	0.1222	0.2295	0.2510	0.2808	0.2444	0.2099	0.1891	0.1696	0.1570	0.1235	0.0736	0.0560	0.0444
c_D	0.0439	0.0543	0.1081	0.2511	0.2683	0.2894	0.2495	0.2056	0.1813	0.1607	0.1441	0.1081	0.0517	0.0391	0.0311
M	0.597	869.0	0.799	1.252	1.198	1.151	0.953	0.923	0.899	0.874	0.853	0.802	0.703	0.599	0.402

Table 21. Pressure and Force Data for Nozzle 12 With $\beta_{t,top/bot} = 15.0^{\circ}/\beta_{t,side} = 22.4^{\circ}$ and Plume Off

(a) Static pressure coefficients on nozzle top flap

		_	_				_																
	.926	-0.036	-0.053	-0.070	-0.071	-0.052	-0.023	-0.020	-0.025	-0.006	0.031	0.065	0.012	0.046	0.115	0.171	0.165	0.145	0.164	0.162	0.149	0.132	0.155
	.853	-0.055	-0.069	-0.087	-0.102	-0.084	-0.057	-0.057	-0.061	-0.045	-0.014	0.025	-0.023	0.017	0.090	0.144	0.137	0.110	0.136	0.140	0.130	0.113	0.128
	<i>6LL</i> :	-0.074	-0.088	-0.103	-0.122	-0.111	-0.085	-0.088	-0.087	-0.078	-0.054	-0.015	-0.053	-0.015	0.058	0.113	0.107	0.074	0.107	0.116	0.109	0.093	0.098
line	.705	-0.109	-0.116	-0.127	-0.143	-0.135	-0.114	-0.122	-0.117	-0.110	-0.100	-0.064	-0.085	-0.048	0.022	0.077	0.071	0.033	0.070	0.085	0.081	990.0	0.061
nap at center	.632	-0.325	-0.210	-0.168	-0.163	-0.159	-0.142	-0.157	-0.148	-0.142	-0.149	-0.125	-0.119	-0.087	-0.023	0.033	0.028	-0.013	0.028	0.049	0.048	0.034	0.024
Static pressure coefficients on nozzle top flap at centerline with values of x/l of—	.558	-0.399	-0.445	-0.443	-0.194	-0.186	-0.178	-0.203	-0.182	-0.182	-0.209	-0.205	-0.158	-0.134	-0.086	-0.024	-0.029	-0.074	-0.030	-0.003	0.000	-0.014	-0.029
coefficients on nozzle to with values of x/l of—	.484	-0.400	-0.441	-0.491	-0.246	-0.222	-0.215	-0.260	-0.222	-0.221	-0.270	-0.303	-0.205	-0.192	-0.170	-0.100	-0.103	-0.151	-0.104	-0.073	-0.064	-0.079	-0.100
tic pressure o	.411	-0.453	-0.505	-0.550	-0.394	-0.294	-0.280	-0.377	-0.287	-0.284	-0.363	-0.498	-0.270	-0.275	-0.306	-0.224	-0.221	-0.274	-0.222	-0.185	-0.172	-0.187	-0.207
Sta	.337	-0.461	-0.514	-0.565	-0.765	-0.544	-0.471	-0.781	-0.482	-0.460	-0.675	-1.033	-0.441	-0.455	-0.587	-0.506	-0.478	-0.548	-0.480	-0.429	-0.407	-0.427	-0.424
	300	-0.375	-0.420	-0.470	-0.772	-0.814	-0.835	-0.875	-0.835	-0.830	-0.897	-0.903	-0.849	-0.904	-1.115	-1.194	-0.885	-1.007	-0.891	-0.804	-0.766	-0.805	-0.733
	.226	_	1	1			1	-	-	_	-	1	1	1	-	-	1	-	-	_	_	1	_
	.153	0.000	-0.002	-0.020	-0.096	-0.128	-0.148	-0.134	-0.148	-0.157	-0.162	-0.165	-0.167	-0.189	-0.227	-0.287	-0.282	-0.300	-0.283	-0.262	-0.242	-0.234	-0.254
	α, deg	0.008	0.015	0.012	-0.015	0.029	-0.014	-2.979	-0.006	2.987	5.992	9.005	0.016	0.016	0.005	-0.010	-0.012	-2.995	-0.012	2.995	5.993	8.995	0.030
	M_{∞}	1.251	1.198	1.150	0.952	0.922	0.899	0.899	0.900	0.899	0.899	0.899	0.875	0.849	0.802	0.701	0.601	0.602	0.602	0.603	0.600	0.600	0.400

Table 21. Continued

(a) Continued

		_		_	_	_	_			\neg	\neg		_	\neg	_					_		Т	T	٦
	.926	-0.037	-0.051	-0.068	-0.071	-0.051	-0.022	-0.020	-0.024	-0.003	0.032	0.065	0.014	0.047	0.117	0.171	0.165	0.145	0.164	0.163	0.150	0.134	0.158	0.1.0
	.853	-0.054	-0.071	-0.087	-0.101	-0.082	-0.055	-0.056	-0.057	-0.043	-0.010	0.025	-0.020	0.016	0.092	0.147	0.139	0.113	0.139	0.142	0.132	0 116	133	0.132
25	622.	-0.075	880.0-	-0.104	-0.123	-0.110	-0.085	-0.091	680'0-	-0.080	-0.054	6100-	-0.050	-0.015	090'0	0.116	0.112	0.079	0.112	0.121	0 114	0000	0.00	0.104
ip at y/Y = 0.	.705	-0.117	-0.121	-0.129	-0.145	-0.136	-0.112	-0.123	-0.117	-0.111	-0.099	-0.065	-0.087	-0.050	0.023	0.079	0.072	0.034	0.072	0.087	0.087	200.0	2000	0.005
nozzle top fla	.558	-0.405	-0.445	-0.467	-0.193	-0.189	-0.179	-0.202	-0.183	-0.182	-0.204	-0.198	-0.158	-0.134	-0.084	-0.022	-0.024	0700	-0.025	1000	200	2500	710.0	-0.030
fficients on nozzle to	.411	-0.451	-0.499	-0.553	-0.413	-0.304	-0.284	-0.374	-0.291	-0.285	-0.361	-0.481	-0.278	-0.276	-0.302	-0.217	-0.217	0200	5120	0.170	7710	001.00	10.104	-0.202
Static pressure coefficients on nozzle top flap at $y/Y = 0.25$ with values of x/l of—	.337	-0.463	-0.513	-0.565	-0.793	-0.582	-0.491	-0.806	-0.509	-0.469	669.0-	1.041	-0.455	-0.462	-0.587	0.500	0.472	0.541	0.773	0.477	0.400	20.400	-0.422	-0.418
Static	300	-0.370	-0.414	0.464	-0.762	-0.815	-0.840	-0.867	-0.843	-0.834	6880	-0.895	C98 0-	8160	-1115	194	0800	0101	0.805	2100	0.010	10.7	-0.80/	-0.733
	.226	9009	9100	040	1910	661 0	-0.226	0 2 10	7000	0.230	0.237	0.244	0.250	0.285	0.337	0.736	8170	0.450	0.470	0.700	0.200	-0.360	-0.355	-0.368
	.153	0 003	0.00	910.0	5003	124	141	121	181.0	0.153	160	0.167	0.161	0.101	0 220	0.22.0	0.371	0.20	0.220	-0.273	-0.232	-0.232	-0.225	-0.247
	g deg	8000	0.000	610.0	210.0	0000	7700	2 070	-6.717	2000	5 000	2,772	5100	0.010	0.010	500.0	0.010	210.0-	2,995	710.0	2.995	5.993	8.995	0.00
	\$	8 7 7	1071	1.150	0000	0.000	0.900	0.099	0.099	0.900	0.899	0.099	0.099	0.070	0.049	0.802	0.701	0.601	0.602	0.602	0.603	0.000	0.600	0.400

Table 21. Continued (a) Continued

		1	_	_	_	_		_	_	_	_	_	_	_	_	_	_	_		_	_		
	.926	0000	0.020	900	0.000	0.073	1000	0.021	0.010	0.005	0031	0.055	0.014	9700	0.040	0 169	0 164	0010	0.072	20.02	-0.003	0.031	0.00
	.853	-0.053	890 9	0.000	0.000	0.00	0.054	0.057	0.056	00.0	1100	1100	-0.00	0.017	1000	0.145	0 141	0.057	0.05	0.030	10.0	10.01	0.132
0.50	677.	70 076	10.092	20105	201.0	0.12	0.087	000	880.0	0.003	-0.053	-0.030	-0.054	5100	0.050	0.116	0.111	-0.093	880 0	0.000	0.063	0.033	101.0
flap at $y/Y =$	705.	-0.137	128	0130	-0.145	5 130	0.116	2131	120	-0110	6600	-0.077	-0.085	-0.048	0.023	0.080	0.077	-0131	0 120	0 110	0000	5000	0.071
Static pressure coefficients on nozzle top flap at $y/Y = 0.50$ with values of y/l of—	.558	-0.378	-0.417	-0.456	20107	161.0	121	-0.207	-0.180	-0.182	-0.194	-0.191	-0.160	-0.131	-0.078	-0.014	-0.014	-0.207	0810	281 9	197	191	-0.011
coefficients c	.411	-0.432	-0.476	-0.529	-0.423	-0.311	-0.298	-0.369	-0.301	-0.305	-0.372	-0.448	-0.285	-0.281	-0.289	-0.201	-0.199	-0.369	-0.301	-0.305	77.0	-0.448	-0.181
atic pressure	.337	-0.468	-0.518	-0.572	-0.833	-0.650	-0.534	-0.795	-0.554	-0.492	-0.699	-1.030	-0.490	-0.491	-0.590	-0.473	-0.448	-0.795	-0.554	-0.492	009 0-	-1.030	-0.394
Si	300	-0.370	-0.413	-0.463	-0.764	-0.820	-0.867	-0.875	-0.869	-0.869	-0.910	-0.917	-0.897	-0.954	-1.120	-1.146	-0.875	-0.875	-0.869	-0.869	0.910	-0.917	-0.716
	.226	-0.009	-0.019	-0.044	-0.159	-0.196	-0.223	-0.206	-0.225	-0.241	-0.253	-0.272	-0.246	-0.277	-0.329	-0.416	-0.397	-0.206	-0.225	-0.241	-0.253	-0.272	-0.352
	.153	0.005	-0.002	-0.021	-0.091	-0.123	-0.144	-0.131	-0.144	-0.159	-0.176	-0.198	-0.160	-0.181	-0.215	-0.261	-0.256	-0.131	-0.144	-0.159	-0.176	-0.198	-0.232
	α, deg	0.008	0.015	0.012	-0.015	0.029	-0.014	-2.979	-0.006	2.987	5.992	9.005	0.016	0.016	0.005	-0.010	-0.012	-2.979	-0.006	2.987	5.992	9.005	0.030
	M	1.251	1.198	1.150	0.952	0.922	0.899	0.899	0.900	0.899	0.899	0.899	0.875	0.849	0.802	0.701	0.601	0.899	0.900	0.899	0.899	0.899	0.400

Table 21. Continued

(a) Concluded

-0.062 -0.026 0.0390.014 0.169 0.1490.162 0.1520.044 -0.050-0.023-0.022 0.029 0.047 0.118 0.149 0.161 0.157-0.027926 0.000 0.019 0.146 0.132 -0.082 -0.105 -0.056 -0.041 0.143 0.143 0.142 0.138 0.134 -0.083 -0.0080.093 -0.063 -0.059 0.127 -0.047 .853 -0.074 -0.104 -0.114-0.08890.100 -0.091 -0.049-0.042 -0.0130.114 0.114 0.115 0.112 0.110 -0.0870.119 0.093 0.117 0.061 *9LL*: Static pressure coefficients on nozzle top flap at y/Y = 0.75-0.120-0.146 -0.089 0.076 -0.220-0.135-0.160 -0.144-0.123-0.092-0.048 0.023 0.082 0.055 0.092 0.085 -0.163-0.1170.087 705 with values of x/l of--0.085 -0.013 -0.052 -0.009 -0.256 -0.166-0.136 0.015 -0.003 -0.008-0.389-0.432 -0.194-0.197-0.192-0.202 -0.009 0.013 -0.347-0.211-0.211.558 -0.493 -0.303 -0.295 -0.274-0.396 -0.373-0.319-0.360-0.139-0.339-0.297 -0.321 -0.178 -0.163-0.437-0.316-0.182-0.1789.18 -0.131<u>4</u>. -0.231-0.470 -0.457 -0.494 -0.536-0.446 -0.503 -0.296-0.270 -0.374-0.504 -0.515-0.348-0.483-0.585 -0.560 -0.509 -0.585 -0.480.337 -0.355 -0.448 -0.733 -0.792 -0.809 -0.809 0.909 -1.106 -0.893 -1.067 -0.896 -0.828 -1.019 -0.699 -0.583 -0.738-0.831-0.881300 -0.249 -0.236 -0.320 -0.007 -0.046 -0.152-0.214-0.196-0.214 -0.285-0.377-0.364-0.386-0.325-0.189 -0.343-0.311-0.365.226 -0.135-0.160 -0.156 -0.174 -0.238 -0.246-0.236-0.234 -0.229 0.003 -0.003 -0.028 -0.092 -0.120 -0.139-0.140 -0.179-0.198 -0.202-0.213.153 α, deg 0.029 -0.014-2.9799000 9.005 0.016 0.016 2.995 8.995 0.015 0.012 2.987 5.992 0.005 -2.995 5.993 0.030 0.008 0.010 -0.012-0.0121.251 1.198 1.150 0.952 0.899 0.899 0.8990.899 0.875 0.802 0.602 0.603 0.600 0.600 0.701 0.601 M

Table 21. Continued

(b) Static pressure coefficients on nozzle sidewall

				Static pres	sure coefficion	Static pressure coefficients on corner between nozzle top flap and sidewall	s on corner between no	zzle top flap a	and sidewall		
M_{∞}	α, deg	.153	.226	.300	.337	.411	.558	.705	<i>611</i> .	.853	.926
1.251	0.008	0.003	1	-0.337	-0.515	-0.406	-0.333	-0.212	-0.088	-0.040	-0.023
1.198	0.015	-0.004		-0.381	-0.565	-0.443	-0.374	-0.187	-0.083	-0.058	-0.039
1.150	0.012	-0.029	1	-0.427	-0.625	-0.493	-0.418	-0.139	-0.093	-0.074	-0.059
0.952	-0.015	-0.092	ı	-0.701	-0.622	-0.409	-0.274	-0.185	-0.153	-0.122	-0.088
0.922	0.029	-0.122	ı	-0.755	-0.484	-0.353	-0.238	-0.158	-0.124	-0.093	-0.060
0.899	-0.014	-0.142	1	-0.776	-0.445	-0.335	-0.213	-0.128	-0.091	-0.059	-0.027
0.899	-2.979	-0.140	ı	-0.751	-0.406	-0.343	-0.279	-0.170	-0.119	-0.071	-0.033
0.900	-0.006	-0.142	1	-0.781	-0.451	-0.337	-0.215	-0.131	-0.095	-0.062	-0.031
0.899	2.987	-0.161	1	-0.779	-0.455	-0.345	-0.215	-0.124	-0.085	-0.046	-0.010
0.899	5.992	-0.182	1	-0.699	-0.386	-0.333	-0.251	-0.148	-0.110	-0.071	-0.028
0.899	9.005	-0.199	1	-0.655	-0.373	-0.339	-0.290	-0.200	-0.168	-0.141	-0.058
0.875	0.016	-0.156	ı	-0.801	-0.429	-0.320	-0.188	-0.090	-0.051	-0.019	0.010
0.849	0.016	-0.174	į.	-0.844	-0.443	-0.319	-0.156	-0.049	-0.012	0.021	0.046
0.802	0.005	-0.205	1	-0.954	-0.472	-0.282	-0.106	0.012	0.057	0.090	0.113
0.701	-0.010	-0.239	ļ	-1.143	-0.449	-0.163	-0.002	0.088	0.119	0.143	0.164
0.601	-0.012	-0.235	1	-0.932	-0.443	-0.160	0.013	0.090	0.117	0.139	0.159
0.602	-2.995	-0.247	1	-1.077	0.512	-0.206	-0.018	0.074	0.105	0.125	0.145
0.602	-0.012	-0.236	1	-0.939	-0.445	-0.160	0.013	0.091	0.118	0.139	0.160
0.603	2.995	-0.235	t	-0.814	-0.375	-0.125	0.027	0.094	0.119	0.139	0.158
0.600	5.993	-0.236	1	-0.690	-0.292	-0.093	0.017	0.087	0.116	0.137	0.152
0.600	8.995	-0.232	-	-0.462	-0.188	-0.159	0.003	0.092	0.117	0.132	0.134
0.400	0.030	-0.215	-	-0.769	-0.396	-0.144	0.018	0.084	0.113	0.133	0.151

Table 21. Continued

(b) Continued

| $\neg \tau$ | | | | П | Т | | | | |

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 | Т | \neg | П | | | | |
 | Т | 7 |
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| .926 | -0.019 | -0.034 | -0.055 | -0.077 | -0.044 | -0.010 | -0.017 | -0.013 | 0.005 | -0.002

 | -0.007 | 0.025
 | 170.0

 | 0.001
 | 0.119 | 0.170 | 0.163 | 0.145 | 0.164 | 0.159 | 0.138 | 0.005
 | 0.000 | 0.130 |
| .853 | -0.042 | -0.051 | -0.068 | -0.115 | -0.085 | -0.049 | -0.067 | -0.053 | -0.043 | -0.075

 | -0.113 | 1109
 |

 | 0.029
 | 0.091 | 0.148 | 0.142 | 0.125 | 0.142 | 0.139 | 0.122 | 0000
 | 0.030 | 0.141 |
| 622. | -0.099 | -0.092 | -0.090 | -0.154 | -0.127 | -0.091 | -0.119 | -0.095 | -0.094 | -0.157

 | -0.215 | 0.052
 | 20.02

 | -0.011
 | 0.052 | 0.122 | 0.121 | 0.105 | 0.122 | 0.119 | 0 103 | 0.002
 | 0.003 | 0.122 |
| .705 | -0.169 | -0.170 | -0.142 | -0.194 | -0.167 | -0.136 | -0.173 | -0.139 | -0.150 | -0.230

 | -0.286 | 0000
 | -0.07/

 | -0.060
 | -0.004 | 0.088 | 0.097 | 0.082 | 0.097 | 960.0 | 0.078 | 0.00
 | 0.002 | 0.099 |
| .558 | | | | | ı | 1 | , | | 1 | 1

 | 1 |
 | 1

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 | _ | 1 | 1 | 1 | ı | | |
 | 1 | - |
| .411 | -0.456 | -0.496 | -0.551 | -0.405 | -0.347 | -0.321 | -0.306 | -0.323 | -0.347 | -0.350

 | -0.355 | 21.00
 | C15.0

 | -0.314
 | -0.284 | -0.171 | -0.151 | -0.179 | -0.153 | 0130 | 20100 | 501.0
 | 121.0- | -0.143 |
| .337 | -0.549 | -0.606 | -0.666 | -0.561 | -0.445 | -0.408 | -0 337 | -0.414 | -0.453 | 0.419

 | 0410 | 0.110
 | -0.398

 | -0.423
 | -0.438 | -0.435 | -0.475 | -0.521 | -0.478 | 0770 | 0.776 | 0.570
 | -0.254 | -0.431 |
| 300 | -0.362 | -0.407 | -0.459 | -0.734 | -0.747 | -0.739 | 5990- | 0.202 | 0.783 | 0.742

 | 0.712 | -0.712
 | -0.753

 | -0.799
 | -0.895 | -1.172 | -1.001 | -1 108 | -1 008 | 0,062 | -0.302 | -0.899
 | -0.733 | -0.837 |
| .226 | 5000 | 610.0 | 0.049 | 0.150 | -0.186 | 0100 | 0.205 | 0.21 | 0.230 | 0.250

 | 0.207 | -0.297
 | -0.231

 | -0.258
 | -0.299 | 795 0- | 292.0- | 0 381 | 595.0 | 0350 | -0.300 | -0.363
 | -0.356 | -0.324 |
| .153 | | | | | | | | | - | _

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 | | 1 |
| α. deg | 8000 | 0.000 | 0.012 | 2100 | 0000 | 0.020 | 10.014 | -2.979 | 2 000 | 2.987

 | 3.992 | 5.00.6
 | 0.016

 | 0.016
 | 0.005 | 0100 | 0.010 | 2,005 | 22.77 | 2000 | 2.995 | 5.993
 | 8.995 | 0.030 |
| × | 85. | 1001 | 1.190 | 0.052 | 0.932 | 0.922 | 0.099 | 0.899 | 0.500 | 0.899

 | 0.899 | 0.899
 | 0.875

 | 0.849
 | 0.802 | 0.00 | 0.701 | 00.00 | 0.002 | 0.002 | 0.603 | 0.600
 | 0.600 | 0.400 |
| | g. deg 153 226 300 337 411 .558 705 705 853 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 0.008 - -0.005 -0.362 -0.549 -0.456 - -0.169 -0.092 -0.042 0.015 - -0.019 -0.407 -0.606 -0.496 - -0.170 -0.092 -0.051 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 0.008 - -0.005 -0.362 -0.549 -0.456 - - -0.169 -0.099 -0.042 0.015 - -0.019 -0.477 -0.606 -0.496 - -0.0170 -0.092 -0.051 0.012 - -0.049 -0.459 -0.666 -0.551 - -0.142 -0.090 -0.068 | α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 0.008 - -0.005 -0.362 -0.549 -0.456 - - -0.169 -0.042 0.015 - -0.019 -0.407 -0.666 -0.496 - -0.170 -0.092 -0.051 0.012 - -0.049 -0.459 -0.666 -0.551 - -0.142 -0.090 -0.068 0.015 - -0.150 -0.734 -0.561 -0.405 - -0.194 -0.154 -0.115 | α , deg.153.226.300.337.411.558.705.779.8530.0080.005-0.362-0.549-0.4560.169-0.092-0.0420.0150.019-0.407-0.606-0.4960.170-0.092-0.0510.0120.049-0.459-0.666-0.5510.142-0.090-0.0680.0150.150-0.734-0.561-0.4050.154-0.154-0.154-0.157-0.085 | α , deg .153 .226 .300 .337 .411 .558 .705 .779 .853 0.008 - -0.005 -0.362 -0.549 -0.456 - -0.169 -0.099 -0.042 0.015 - -0.019 -0.407 -0.666 -0.496 - -0.170 -0.092 -0.051 0.012 - -0.049 -0.459 -0.666 -0.551 - -0.142 -0.090 -0.068 -0.015 - -0.150 -0.734 -0.561 -0.405 - -0.194 -0.154 -0.115 0.029 - -0.186 -0.747 -0.445 -0.347 - -0.167 -0.127 -0.085 0.012 - -0.186 -0.747 -0.408 -0.321 - -0.136 -0.091 -0.049 | α , deg .153 .226 .300 .337 .411 .558 .705 .779 .853 0.008 - -0.005 -0.362 -0.549 -0.456 - -0.169 -0.099 -0.042 0.015 - -0.019 -0.407 -0.666 -0.496 - -0.142 -0.090 -0.048 0.012 - -0.049 -0.459 -0.666 -0.551 - -0.142 -0.090 -0.068 -0.015 - -0.150 -0.734 -0.561 -0.405 - -0.194 -0.154 -0.115 0.029 - -0.186 -0.747 -0.561 -0.347 - -0.167 -0.127 -0.085 0.014 - -0.210 -0.739 -0.408 -0.321 - -0.136 -0.091 -0.091 -0.049 0.020 - -0.016 -0.739 -0.408 -0.337 -0.136 -0.119 -0.119 -0.019 | α , deg .153 .226 .300 .337 .411 .558 .705 .779 .853 0.008 - -0.005 -0.362 -0.549 -0.456 - -0.169 -0.099 -0.042 0.015 - -0.019 -0.407 -0.666 -0.496 - -0.170 -0.090 -0.042 0.012 - -0.049 -0.459 -0.666 -0.551 - -0.142 -0.090 -0.068 -0.015 - -0.150 -0.734 -0.561 -0.405 - -0.194 -0.154 -0.115 0.029 - -0.186 -0.747 -0.561 -0.347 - -0.167 -0.127 -0.085 -0.014 - -0.210 -0.739 -0.408 -0.321 - -0.139 -0.091 -0.049 -0.026 -0.205 -0.665 -0.337 -0.336 - -0.139 -0.095 -0.091 | α , deg .153 .226 .300 .337 .411 .558 .705 .779 .853 0.008 - -0.005 -0.362 -0.549 -0.456 - -0.169 -0.099 -0.042 0.015 - -0.019 -0.407 -0.666 -0.496 - -0.170 -0.092 -0.042 0.012 - -0.049 -0.459 -0.666 -0.551 - -0.142 -0.090 -0.068 0.029 - -0.150 -0.734 -0.561 -0.405 - -0.194 -0.154 -0.115 0.029 - -0.186 -0.747 -0.561 -0.347 - -0.167 -0.157 -0.085 -0.014 - -0.210 -0.739 -0.445 -0.347 - -0.167 -0.091 -0.049 -2.979 - -0.205 -0.665 -0.337 -0.306 - -0.139 -0.095 -0.095 -0.006 - <t< td=""><td>α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 0.008 - -0.005 -0.362 -0.549 -0.456 - -0.169 -0.099 -0.042 0.015 - -0.019 -0.479 -0.666 -0.496 - -0.170 -0.092 -0.051 0.012 - -0.049 -0.459 -0.666 -0.551 - -0.142 -0.090 -0.068 0.015 - -0.150 -0.734 -0.561 -0.405 - -0.194 -0.154 -0.115 0.029 - -0.186 -0.747 -0.445 -0.347 - -0.194 -0.157 -0.085 -0.014 - -0.014 -0.739 -0.445 -0.347 - -0.167 -0.091 -0.049 -0.006 - -0.017 -0.130 -0.13 -0.091 -0.049 -0.049 -0.016 - -0.216 -0.747</td><td>α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 0.008 - -0.005 -0.362 -0.549 -0.456 - -0.169 -0.099 -0.042 0.015 - -0.019 -0.479 -0.666 -0.496 - -0.170 -0.092 -0.051 0.012 - -0.049 -0.459 -0.666 -0.551 - -0.142 -0.090 -0.068 0.012 - -0.150 -0.734 -0.561 -0.405 - -0.194 -0.154 -0.115 0.029 - -0.150 -0.747 -0.347 - -0.194 -0.154 -0.045 -0.014 - -0.014 -0.747 -0.445 -0.347 - -0.136 -0.091 -0.049 -2.979 - -0.205 -0.665 -0.337 -0.306 - -0.139 -0.095 -0.095 -0.987 - -0.230 <t< td=""><td>α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 0.008 - -0.005 -0.362 -0.549 -0.456 - -0.169 -0.099 -0.042 0.015 - -0.019 -0.407 -0.666 -0.496 - -0.170 -0.092 -0.045 0.012 - -0.049 -0.459 -0.666 -0.551 - -0.142 -0.090 -0.068 0.012 - -0.049 -0.459 -0.666 -0.551 - -0.142 -0.154 -0.115 0.029 - -0.150 -0.747 -0.561 -0.347 - -0.167 -0.154 -0.154 -0.014 - -0.014 -0.745 -0.408 -0.347 - -0.167 -0.154 -0.014 - -0.016 -0.205 -0.665 -0.337 -0.366 - -0.167 -0.194 -0.194 -0.006 - <t< td=""><td>α, deg .153 .226 .300 .337 .411 .558 .705 .779 .853 0.008 - -0.005 -0.362 -0.549
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Table 21. Continued

(b) Continued

926 -0.059-0.064 -0.067 -0.085-0.050-0.067 -0.053-0.045 -0.068-0.095-0.0090.030 0.094 0.149 0.144 0.135 0.144 0.133 0.116 0.047 0.141 .853 0.101 -0.103-0.105 -0.099 -0.158-0.130-0.094-0.118-0.098-0.150-0.1960.114 -0.0530.115 0.123 -0.1010.124 0.036 0.121 -0.0110.051 0.087 -0.149-0.147-0.198-0.172-0.142-0.169-0.163-0.274-0.105-0.0030.089 -0.147-0.227-0.0630.095 0.099 0.093 705 -0.161 0.101 0.101 0.031 0.071 Static pressure coefficients on nozzle sidewall at centerline -0.190-0.216-0.243-0.214-0.189-0.216-0.125 -0.2740.068 0.068 0.015 0.074 -0.211 -0.191 -0.221-0.311-0.161 0.063 .632 0.041 0.061 0.041 with values of x/l of— -0.235 -0.256 -0.239 -0.272 -0.306 -0.313-0.254-0.280-0.2860.036 -0.215-0.1490.024 0.028 0.008 .558 -0.191-0.0260.027 0.023 -0.021-0.440-0.405-0.490 -0.323-0.289-0.269-0.275-0.272-0.309-0.319-0.033-0.317-0.249-0.034-0.045-0.036-0.074-0.024-0.116 .484 -0.261-0.221-0.037-0.516 -0.626-0.565-0.370-0.294-0.330-0.299-0.304 -0.286-0.289-0.262-0.198-0.139-0.156-0.140-0.143-0.143-0.144-0.132-0.291-0.277-0.31114. -0.532 -0.539 -0.566 -0.686 -0.382-0.340 -0.308-0.343-0.315-0.308-0.326-0.298 -0.518-0.623-0.492-0.372-0.528-0.535-0.497-0.502-0.331.337 -0.406-0.453-0.717-0.737-0.704-0.743-0.675-0.748-0.784 -0.803 -0.940 -0.928-0.946-0.936 -0.957 -0.954-0.935-0.789-0.357-0.741-0.721 300 -0.771 -0.026-0.056-0.160-0.194-0.219-0.224-0.219-0.266-0.272 -0.313 -0.007 -0.221 -0.237 -0.392-0.399-0.394-0.402-0.412226 -0.363-0.241-0.387-0.006 -0.146-0.146-0.2000.008 -0.138-0.139-0.167 -0.154-0.173-0.242-0.248-0.250-0.264-0.288-0.223-0.093-0.121-0.244.153 -0.0310.199 -0.237α, deg 0.008 0.015 -0.015-0.0142.987 0.016 0.016 0.012 0.029 -2.9799.005 0.005 -0.010-0.012-2.995-0.0125.992 2.995 5.993 8.995 0.030 1.150 1.198 0.952 0.8990.900 0.899 0.875 0.849 0.802 M 0.922 0.899 0.899 0.899 0.602 0.602 0.603 0.600 0.600 0.400 0.701 0.601 1.251

Table 21. Continued

(b) Concluded

			Stati	c pressure co	Static pressure coefficients on nozzle sidewall at $z/Z = -0.50$ with values of x/l of—	nozzle sidew of x/I of—	z/Z = -	-0.50	
M	α, deg	.153	.226	.300	.337	.411	.558	.705	.926
1.251	0.008	0.013	0.003	-0.334	-0.559	ı	-0.344	-0.193	-0.038
1.198	0.015	-0.005	-0.022	-0.383	-0.618		-0.369	-0.205	-0.045
1.150	0.012	-0.032	-0.046	-0.434	-0.682	1	-0.402	-0.195	-0.054
0.952	-0.015	-0.087	-0.147	-0.675	-0.447	1	-0.289	-0.213	-0.078
0.922	0.029	-0.116	-0.180	-0.646	-0.345	1	-0.262	-0.190	-0.047
0.899	-0.014	-0.136	-0.203	-0.623	-0.306	_	-0.246	-0.156	-0.011
0.899	-2.979	-0.153	-0.223	-0.629	-0.321	1	-0.257	-0.171	-0.026
0.900	9000	-0.135	-0.204	-0.622	-0.307	1	-0.248	-0.161	-0.016
0.899	2.987	0.140	-0.203	-0.652	-0.328	i.	-0.280	-0.178	-0.002
0.899	5.992	-0.167	-0.226	-0.629	-0.300	-	-0.310	-0.235	-0.001
0.899	9.005	-0.217	-0.273	-0.617	-0.309	1	-0.339	-0.293	-0.005
0.875	0.016	-0.148	-0.224	-0.637	-0.302	1	-0.231	-0.119	0.028
0.849	0.016	-0.168	-0.251	1/9'0-	-0.314	1	-0.206	-0.074	0.065
0.802	0.005	-0.192	-0.291	-0.814	-0.378	-	-0.145	-0.006	0.120
0.701	-0.010	-0.228	-0.355	-1.253	-0.449	_	-0.011	0.089	0.167
0.601	-0.012	-0.227	-0.355	-1.060	-0.465	1	0.020	0.094	0.160
0.602	-2.995	-0.230	-0.350	-1.009	-0.426	1	0.027	0.095	0.157
0.602	-0.012	-0.229	-0.357	-1.069	-0.469	ı	0.019	0.093	0.160
0.603	2.995	-0.243	-0.377	-1.180	-0.514	1	0.001	0.077	0.143
0.600	5.993	-0.270	-0.406	-1.253	-0.550	1	-0.022	0.055	0.122
0.600	8.995	-0.316	-0.451	-1.330	-0.599	I	-0.058	0.025	0.118
0.400	0.030	-0.209	-0.323	-0.879	-0.424		0.018	0.094	0.153

Table 21. Continued

(c) Static pressure coefficients on nozzle bottom flap

- 1		-	Т	┰		_	_	7	_	_	7	_	_	_	_	_	_	_	_	_	_	_					
		926	0200	-0.039	-0.047	-0.056	-0.057	-0.026	0.007	0.018	0.004	0.012	0.024	20.0	0.020	0.040	0.069	0.121	0.167	0.161	0 157	0.137	0.101	0.147	0.127	0.106	0.152
		853	301.0	20.103	-0.101	-0.104	-0.108	-0.072	-0.036	-0.024	-0.040	-0.038	-0.046	0.050	600	0.004	0.038	0.094	0.144	0.137	0 138	0.130	0.137	0.120	0.092	0.061	0.132
	= 0.75	977.	0.720	0.230	-0.221	-0.189	-0.161	-0.126	-0.086	-0.071	-0.089	-0.094	-0.126	0 150	2000	7.000	0.000	0.060	0.115	0.110	0 117	0110	0.110	0.088	0.057	0.016	0.104
	Static pressure coefficients on nozzle bottom flap at $y/Y = 0.75$ with values of x/I of—	705	0.325	0.247	-0.347	-0.342	-0.215	-0.183	-0.147	-0.134	-0.151	-0.169	-0.220	-0.275	2000	10:00	-0.049	0.015	0.077	0.076	080	0.075	2000	0.045	0.000	-0.041	0.068
	nozzle botton s of x// of—	.558	0360	1170	0.411	-0.450	-0.291	-0.274	-0.249	-0.246	-0.254	-0.290	-0.348	-0.399	-0.216	0.170	0/1/0	-0.104	-0.014	-0.011	0.016	-0013	6,000	/cn.n-	-0.103	-0.162	-0.014
	efficients on nozzle both with values of x/l of-	.411	-0.403	0.446	0.402	-0.493	-0.383	-0.334	-0.319	-0.309	-0.320	-0.356	-0.373	-0.387	-0.323	302.0	0.220	-0.293	-0.185	-0.181	-0.137	-0.182	0.735	0.233	-0.286	-0.345	-0.170
	: pressure co	.337	-0.468	70 506	0.570	0.5.0	-0.586	-0.432	-0.406	-0.387	-0.402	-0.446	-0.448	-0.453	-0.412	0770	2.00	-0.501	-0.437	-0.418	-0.342	-0.420	0870	0.707	-0.548	-0.607	-0.377
Consti	Static	300	-0.392	-0.443	7070	76.50	-0.781	-0.759	-0.730	-0.710	-0.729	-0.792	-0.804	-0.817	-0.749	-0.805	2000	-0.74	-1.148	-0.930	-0.729	-0.936	-1 080	1.07	-1.19/	-1.303	-0.780
		.226	0.000	-0.024	-0.047	170	-0.148	-0.184	-0.206	-0.240	-0.207	-0.194	-0.195	-0.209	-0.227	-0.256	0000	0.270	-0.303	-0.334	-0.333	-0.355	-0.376	0 304	0.1.2	-0.417	-0.318
		.153	0.013	-0.005	-0.028	7000	-0.000	-0.116	-0.133	-0.153	-0.134	-0.131	-0.144	-0.170	-0.147	-0.168	901.0	0.150	-0.231	-0.223	-0.222	-0.226	-0.238	2500	0.00	-0.283	-0.206
		α, deg	0.008	0.015	0.012	2100	0.01	0.029	-0.014	-2.979	-0.006	2.987	5.992	9.005	0.016	0.016	0.005	0100	0.010	710.0-	-2.995	-0.012	2.995	\$ 003	9000	0.993	0.030
		M_{∞}	1.251	1.198	1.150	0.052	2000	0.927	0.899	0.899	0.900	0.899	0.899	0.899	0.875	0.849	0.802	0.701	0.70	0.001	0.602	0.602	0.603	0 600	0600	0.000	0.400
																											_

Table 21. Concluded

(c) Continued

			Static	pressure coe	Static pressure coefficients on nozzle bottom flap at $y/Y = 0.50$ with values of x/I of—	ozzle botton of x/l of—	flap at y/Y	= 0.50	853	926
.153	3	.226	.300	.337	.411	.558	co/.	611.	.633	0.035
0.036	-	50005	-0.384	-0.461	-0.448	-0.390	-0.360	-0.300	-0.103	0.033
2000	-	-0.003	-0.430	-0.510	-0.491	-0.433	-0.391	-0.257	-0.097	-0.045
270.0	_	0.052	-0.480	-0.559	-0.545	-0.473	-0.423	-0.194	-0.096	-0.038
500	┰	0.032	77.0	-0.865	-0.502	-0.257	-0.165	-0.122	-0.077	-0.043
0.00	Т	0000	-0.846	-0.805	-0.380	-0.238	-0.140	-0.092	-0.050	-0.016
0.015	Т	0020	0.804	-0.686	-0.355	-0.211	-0.106	-0.059	-0.022	0.010
0.010	Т	0.244	0.016	-0.768	-0.367	-0.200	-0.092	-0.046	-0.009	0.023
410.0	Т	0.225	0.510	789.0	-0.355	-0.216	-0.109	-0.062	-0.024	0.010
0.010	T	0.205	0.000	0.824	-0411	-0.245	-0.122	-0.068	-0.022	0.021
-0.019	П	-0.203	-0.092	0.020	0.457	0.305	-0.159	-0.086	-0.022	0.032
-0.019	· I	-0.189	-0.883	0/8/0	-0.437	0.351	0 105	1119	-0.033	0.036
-0.021		-0.175	-0.876	-0.922	-0.480	10.331	0.071	7,000	0.011	0.036
-0.014		-0.248	-0.944	-0.628	-0.33/	20.1/3	70.0	2000	0.041	0.065
-0.018		-0.280	-1.014	-0.615	-0.327	-0.145	0000	2000	0.004	0110
6100	1	-0.330	-1.137	-0.616	-0.289	-0.084	0.023	0.00	10:00	2710
100	ı	-0.407	-1.008	-0.463	-0.206	-0.025	0.075	0.111	0.141	0.103
200	ı	0 380	-0.815	-0.437	-0.199	-0.028	0.071	0.104	0.133	0.138
270.0	ı	0.351	0.708	-0.374	-0.155	0.004	0.089	0.116	0.139	0.158
170.0	1	0.331	0.90	0.440	-0.201	-0.029	0.070	0.104	0.132	0.158
-0.023	J	195.0	-0.019	2020	0770	0.071	0.036	0.074	0.109	0.141
-0.025	ı	-0.418	-0.952	-0.505	0.242	8010	1000	0.042	0.080	0.117
-0.026	- 1	-0.431	-1.050	-0.550	-0.209	0.100	-0.033	0.011	0.054	0.097
-0.027	- 1	-0.436	-1.136	-0.398	-0.324	0.030	0.062	0.096	0.125	0.145
-0.016	- 1	-0.346	-0.689	-0.391	1 -0.192	0.00	700:0			

Table 21. Concluded

(c) Concluded

		\			Ţ				Ţ		I	Γ		T			Π			Τ	Ι	Τ	T
	.926	-0 038	0.048	0.058	900	0.010	000	0.023	0.007	0.00	0.039	0.04	0.02	0.072	0.122	0.165	0.158	0.160	0.158	0 130	0.115	0.095	
terline	705	-0 380	-0.419	-0.458	-0.131	-0.110	-0.093	-0.080	-0.094	-0.094	-0.110	-0.133	-0.068	-0.036	0.023	0.065	0.058	0.078	0.056	0.022	-0.011	-0.038	2000
m flap at cen	.558	-0.423	-0.464	-0.500	-0.225	-0.192	-0.189	-0.182	-0.189	-0.196	-0.225	-0.253	-0.174	-0.149	-0.084	-0.037	-0.043	-0.012	-0.044	-0.084	-0.117	-0.146	0.045
Static pressure coefficients on nozzle bottom flap at centerline	114.	-0.432	-0.481	-0.535	-0.790	-0.481	-0.396	-0.412	-0.396	-0.484	-0.740	-0.902	-0.378	-0.370	-0.330	-0.232	-0.225	-0.186	-0.227	-0.271	-0.304	-0.331	-0.713
Defficients on	.337	-0.447	-0.501	-0.554	-0.880	-0.948	-0.848	-0.904	-0.863	-0.990	-1.013	-1.010	-0.714	-0.661	-0.683	-0.488	-0.455	-0.403	-0.458	-0.510	-0.549	-0.576	0.400
ic pressure co	.300	-0.388	-0.439	-0.487	-0.800	-0.868	-0.921	-0.928	-0.922	-0.919	-0.913	-0.907	-0.975	-1.040	-1.174	-1.073	-0.848	-0.761	-0.855	-0.938	-1.002	-1.043	-0.717
Stat	.226	-0.013	-0.037	-0.059	-0.183	-0.213	-0.237	-0.244	-0.238	-0.229	-0.218	-0.203	-0.260	-0.293	-0.350	-0.430	-0.405	-0.372	-0.408	-0.437	-0.452	-0.461	-0.360
	.153	0.007	-0.014	-0.035	-0.108	-0.134	-0.155	-0.162	-0.156	-0.146	-0.135	-0.120	-0.174	-0.197	-0.233	-0.284	-0.274	-0.251	-0.275	-0.293	-0.299	-0.299	-0.250
	α, deg	0.008	0.015	0.012	-0.015	0.029	-0.014	-2.979	-0.006	2.987	5.992	9.005	0.016	0.016	0.005	-0.010	-0.012	-2.995	-0.012	2.995	5.993	8.995	0.030
	M∞	1.251	1.198	1.150	0.952	0.922	0.899	0.899	0.900	0.899	0.899	0.899	0.875	0.849	0.802	0.701	0.601	0.602	0.602	0.603	0.600	0.600	0.400

Table 21. Concluded

(d) Force data

0.008 0.015 -2.995 -0.014 2.995 -0.012 0.012 0.029 -0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.017 2.997 0.016 0.016 0.017 0.016 0.017 0.018 0.018 0.019 0.010	M	α, deg	$a_{\mathcal{D}}$
0.015 -2.995 -0.014 2.995 6.000 8.988 8.988 0.012 -0.015 -0.015 -0.015 -0.016 0.005 0.005 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.017 -0.010 0.017 -0.010 0	1.251	0.008	0.2786
2.995 -0.014 2.995 6.000 8.988 0.012 -0.015 -0.015 -0.014 -2.979 -0.016 0.005 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.017 -0.010 -0.017 -0.010	1.198	0.015	0.2999
2.995 6.000 8.988 0.012 0.015 0.015 0.029 0.005 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.017 0.017 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.019 0.018	1.200	-2.995	0.3114
2.995 6.000 8.988 0.012 -0.015 0.029 -0.014 -2.979 -0.016 0.016 0.016 0.016 0.016 -0.010 -0.012 -2.995 2.995 2.995 0.013 0.013		-0.014	0.2992
6.000 8.988 0.012 0.012 0.029 0.029 0.014 -2.979 -2.979 -2.979 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.017 -2.995 2.995 2.995 0.013 0.013 0.013 0.013 0.013 0.014	1.198	2.995	0.3020
8.988 0.012 0.012 0.029 0.029 0.029 0.016 0.017 0.017 0.018 0.018 0.019 0.010 0.	1.199	000'9	0.3237
0.012 -0.015 0.029 -0.014 -2.979 -0.006 -0.006 0.016 0.005 -0.010 -0.012 -2.995 -2.995 -2.995 -2.995 -2.995 -2.995 -2.995 -2.995		886.8	0.3384
0.015 0.029 0.029 0.029 0.014 0.014 0.016 0.005 0.016 0.005 0.016 0.005 0.016 0.005 0.016 0.005 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.017 0.017 0.017 0.018 0.018 0.019 0.010 0.	1.150	0.012	0.3222
0.029 -0.014 -2.979 -0.006 2.987 2.987 5.992 9.005 0.016 0.016 0.016 0.016 -0.010 -0.012 -2.995 2.995 5.993 8.995	0.952	-0.015	0.2718
0.014 -2.979 -0.006 2.987 5.992 9.005 0.016 0.016 0.016 0.005 -0.010 -0.012 -2.995 2.995 5.993 8.995	0.922	0.029	0.2336
2.979 -0.006 2.987 5.992 9.005 0.016 0.016 0.005 -0.012 -2.995 2.995 8.995	0.899	-0.014	0.2097
2.987 2.987 5.992 9.005 0.016 0.016 0.005 -0.012 -2.995 2.995 8.995	0.899	-2.979	0.2220
2.987 5.992 9.005 0.016 0.016 0.005 -0.012 -2.995 2.995 5.993 8.995	0.900	-0.006	0.2100
5.992 9.005 0.016 0.016 0.005 -0.012 -2.995 2.995 5.993 8.995	0.899	2.987	0.2199
9.005 0.016 0.016 0.005 -0.010 -2.995 -2.995 2.995 5.993 8.995	0.899	5.992	0.2414
0.016 0.005 0.005 0.005 0.010 0.012 0.012 0.012 2.995 5.993 8.995	0.899	9.005	0.2709
0.016 0.005 -0.010 -0.012 -2.995 -2.995 5.993 8.995	0.875	0.016	0.1912
0.005 -0.010 -0.012 -2.995 -2.995 5.993 8.995	0.849	0.016	0.1709
-0.010 -0.012 -2.995 -0.012 2.995 5.993 8.995	0.802	0.005	0.1368
2.995 -2.995 -0.012 2.995 5.993 8.995	0.701	-0.010	0.0801
2.995 -0.012 2.995 5.993 8.995	0.601	-0.012	0.0718
2.995 2.995 5.993 8.995 0.030	0.602	-2.995	0.0697
2.995 5.993 8.995 0.030	0.602	-0.012	0.0701
8.995 0.030	0.603	2.995	0.0715
8.995	0.600	5.993	0.0777
0.030	0.600	8.995	0.0869
20010	0.400	0:030	0.0646

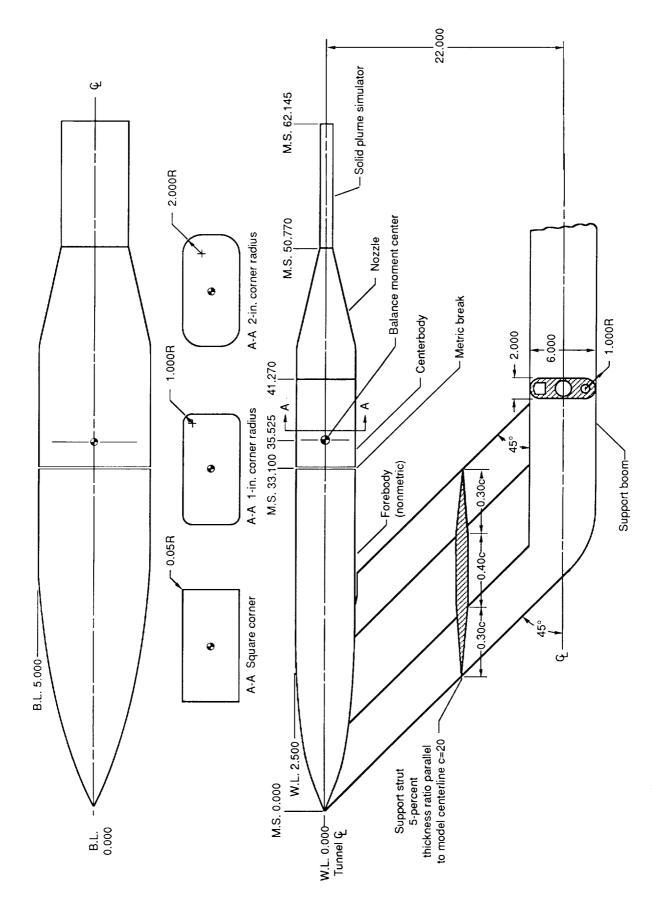
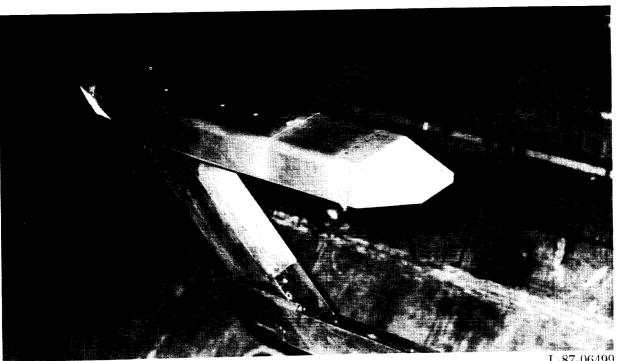


Figure 1. General arrangement of model and support system showing three fuselage cross sections with different corner radii. All linear dimensions are given in inches.

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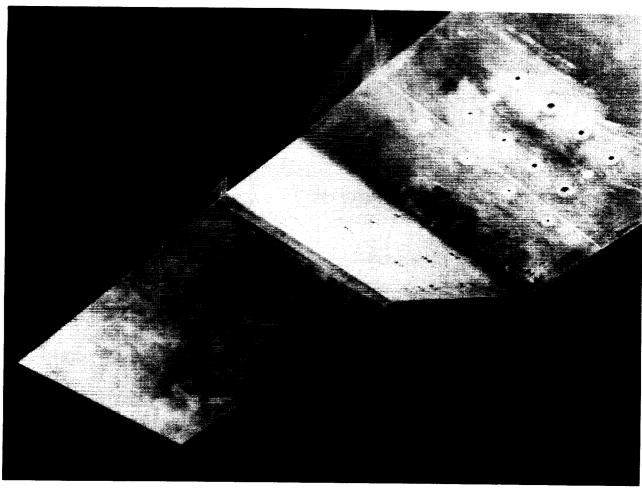
(a) Nozzle 7 without solid plume simulator.



(b) Nozzle 7 with solid plume simulator.

Figure 2. Model installed in the Langley 16-Foot Transonic Tunnel.

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L-87-06210

(c) Nozzle 2 with solid plume simulator.

Figure 2. Concluded.

Nozzie	AR	h _e , in.	w _e , in.	β _{t,top/bot} , deg	$\beta_{t,side}$, deg	R, in.
1	14.49	0.69	10.00	17.9	0	0
2	9.23	.83	7.66	17.3	9.7	0
3	5.76	1.05	6.05	16.4	16.4	0
4	3.28	1.39	4.56	15.0	22.4	0
5	14.49	.69	10.00	17.9	0	1
6	9.23	.83	7.66	17.3	9.7	1
7	5.76	1.05	6.05	16.4	16.4	1
8	3.28	1.39	4.56	15.0	22.4	1
l 9	14.49	.69	10.00	17.9	0	2
10	9.23	.83	7.66	17.3	9.7	2
11	5.76	1.05	6.05	16.4	16.4	2
12	3.28	1.39	4.56	15.0	22.4	2

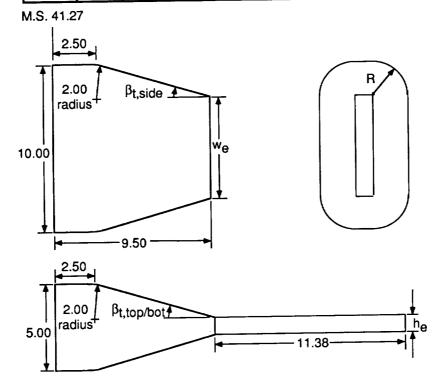


Figure 3. Geometry of nozzle with solid plume simulator. Linear dimensions are given in inches.

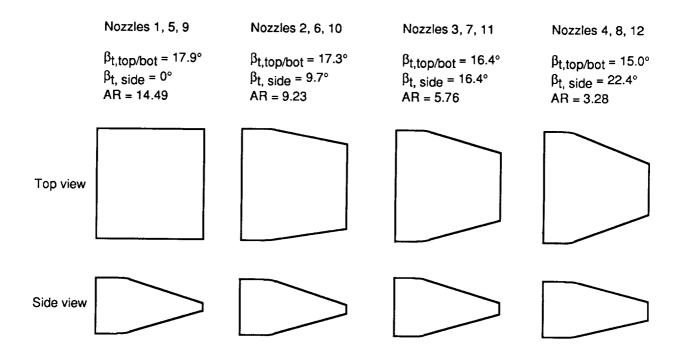


Figure 4. Closure distributions of nozzles.

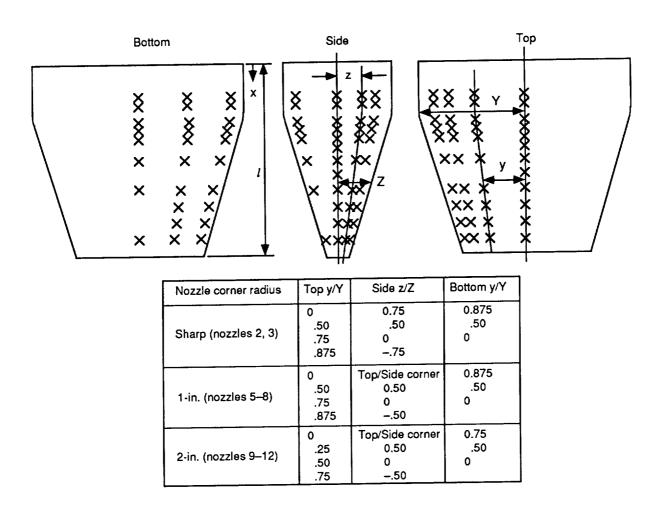


Figure 5. Locations of nozzle pressure orifices.

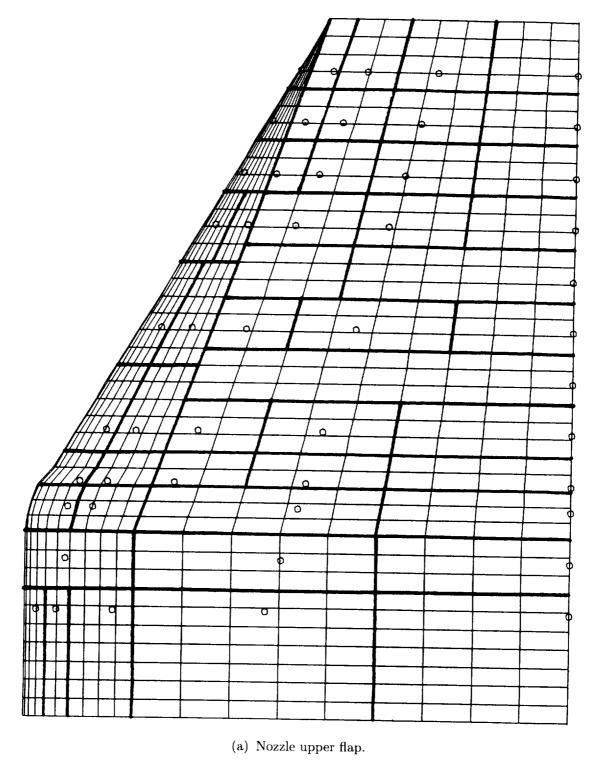
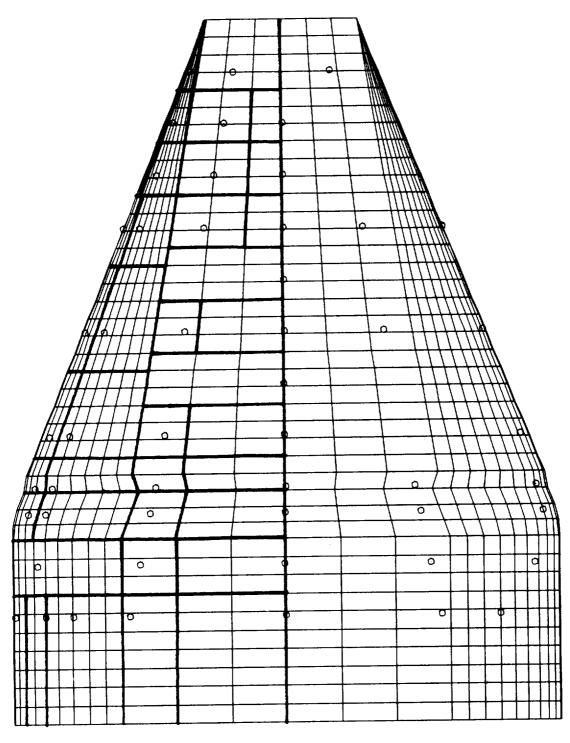
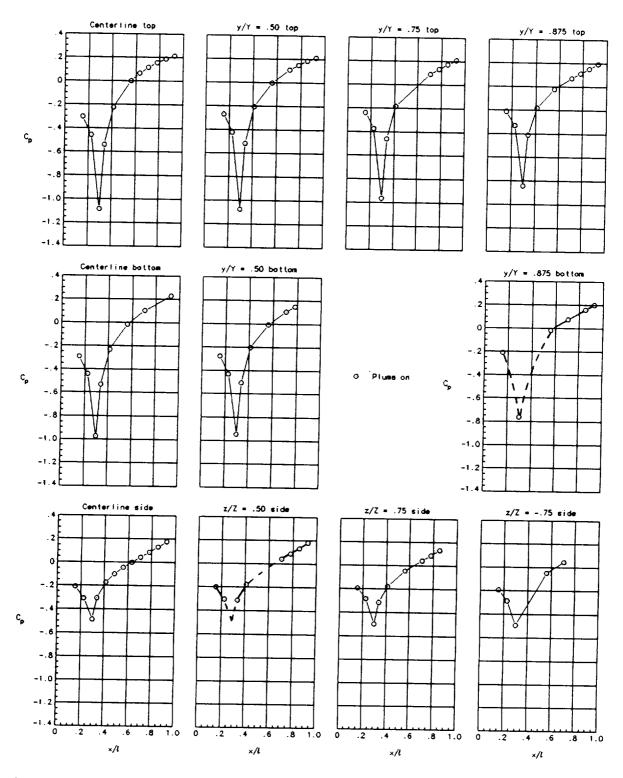


Figure 6. Grid used for determining areas for pressure integration.

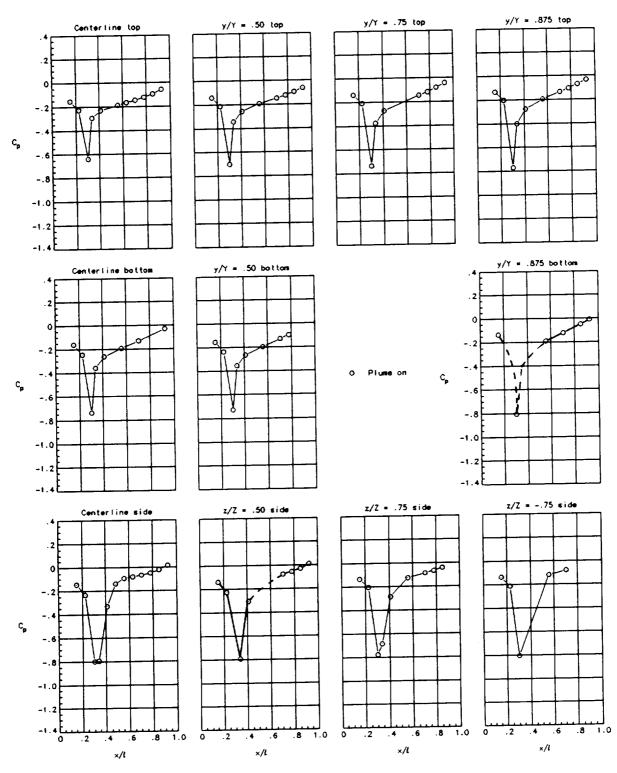


(b) Nozzle sidewall.

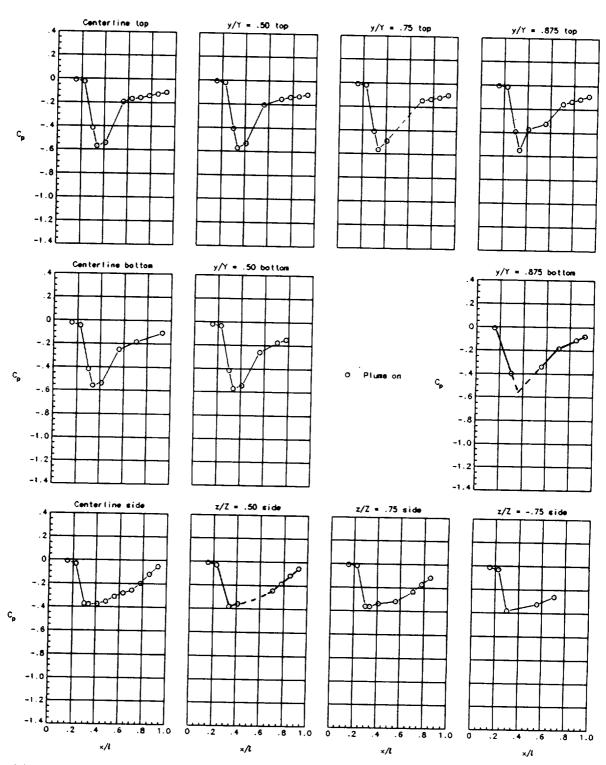
Figure 6. Concluded.



(a) Nozzle 2 with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ and sharp corner at $M_{\infty} = 0.6$. $C_{p,\text{crit}} = -1.290$. Figure 7. Static pressure coefficient distributions on nozzles at $\alpha = 0^{\circ}$.

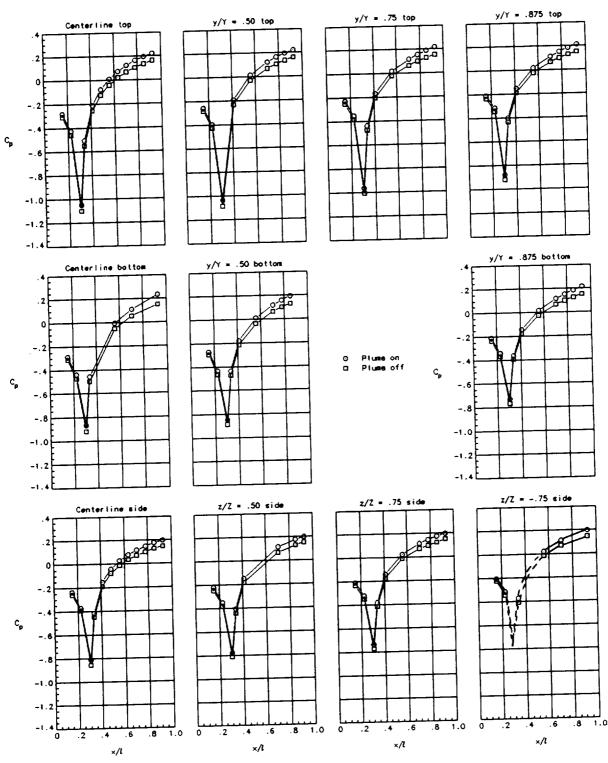


(b) Nozzle 2 with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ and sharp corner at $M_{\infty} = 0.9$. $C_{p,\text{crit}} = -0.188$. Figure 7. Continued.

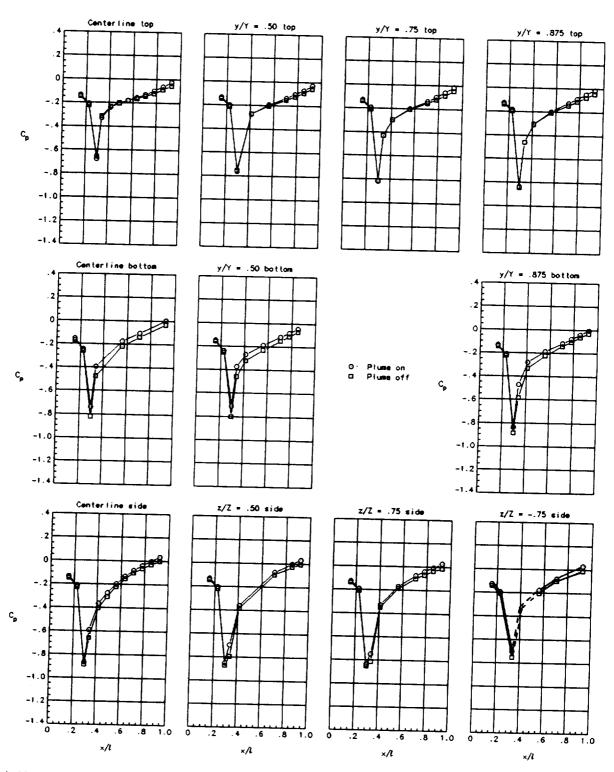


(c) Nozzle 2 with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ and sharp corner at $M_{\infty} = 1.2$. $C_{p,\text{crit}} = 0.279$.

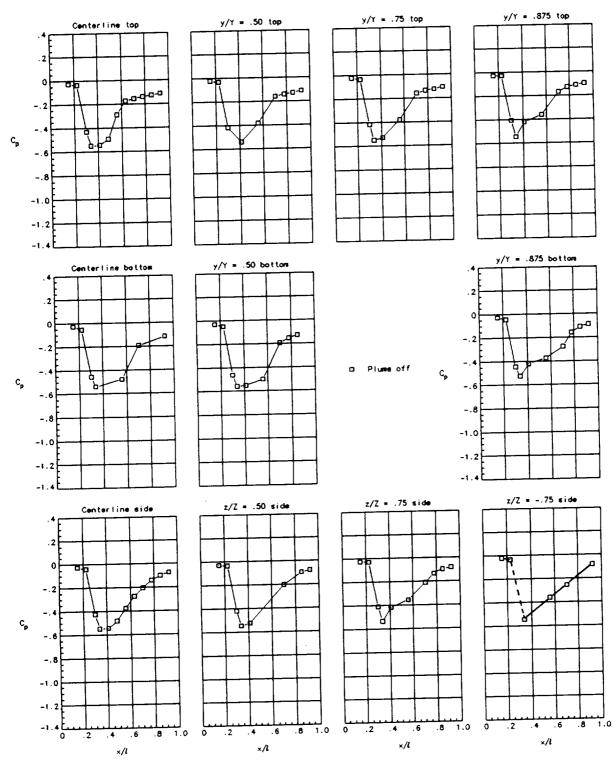
Figure 7. Continued.



(d) Nozzle 3 with $\beta_{t,\text{top/bot}} = 16.4^{\circ}/\beta_{t,\text{side}} = 16.4^{\circ}$ and sharp corner at $M_{\infty} = 0.6$. $C_{p,\text{crit}} = -1.290$. Figure 7. Continued.

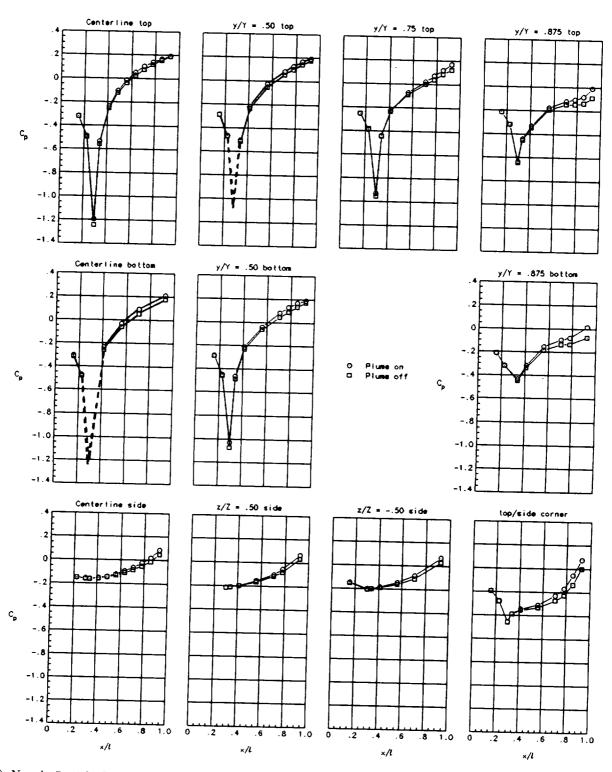


(e) Nozzle 3 with $\beta_{t,\text{top/bot}} = 16.4^{\circ}/\beta_{t,\text{side}} = 16.4^{\circ}$ and sharp corner at $M_{\infty} = 0.9$. $C_{p,\text{crit}} = -0.188$. Figure 7. Continued.

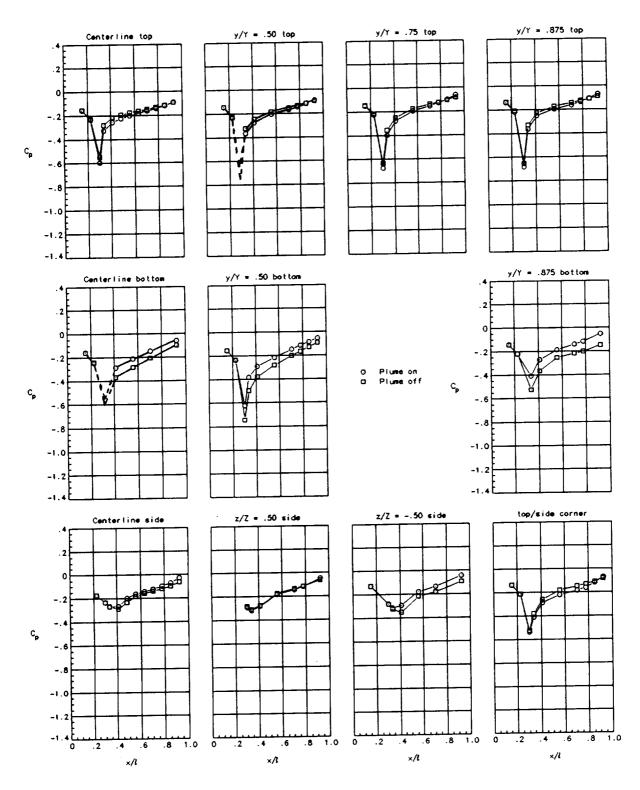


(f) Nozzle 3 with $\beta_{t,\text{top/bot}} = 16.4^{\circ}/\beta_{t,\text{side}} = 16.4^{\circ}$ and sharp corner at $M_{\infty} = 1.2$. $C_{p,\text{crit}} = 0.279$.

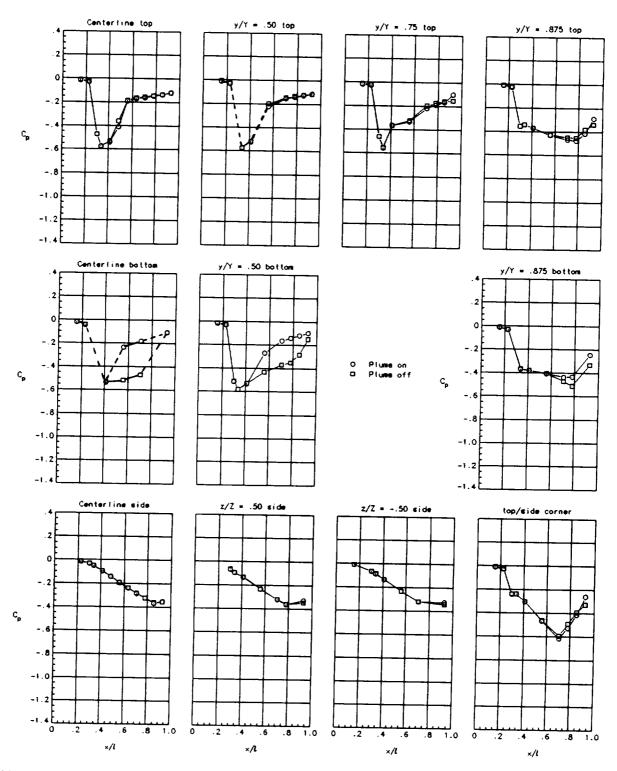
Figure 7. Continued.



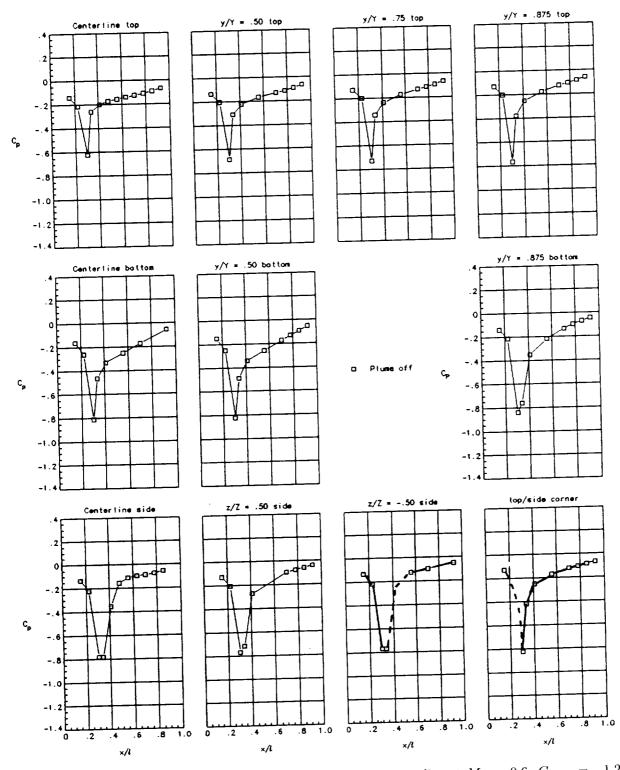
(g) Nozzle 5 with $\beta_{t,\mathrm{top/bot}} = 17.9^{\circ}/\beta_{t,\mathrm{side}} = 0^{\circ}$ and 1-in. corner radius at $M_{\infty} = 0.6$. $C_{p,\mathrm{crit}} = -1.290$. Figure 7. Continued.



(h) Nozzle 5 with $\beta_{t,\text{top/bot}} = 17.9^{\circ}/\beta_{t,\text{side}} = 0^{\circ}$ and 1-in. corner radius at $M_{\infty} = 0.9$. $C_{p,\text{crit}} = -0.188$. Figure 7. Continued.

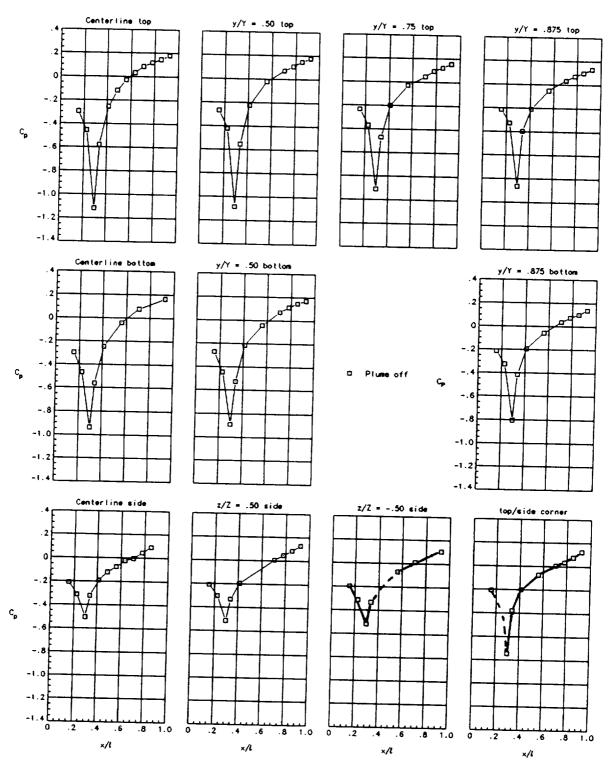


(i) Nozzle 5 with $\beta_{t,\text{top/bot}} = 17.9^{\circ}/\beta_{t,\text{side}} = 0^{\circ}$ and 1-in. corner radius at $M_{\infty} = 1.2$. $C_{p,\text{crit}} = 0.279$. Figure 7. Continued.

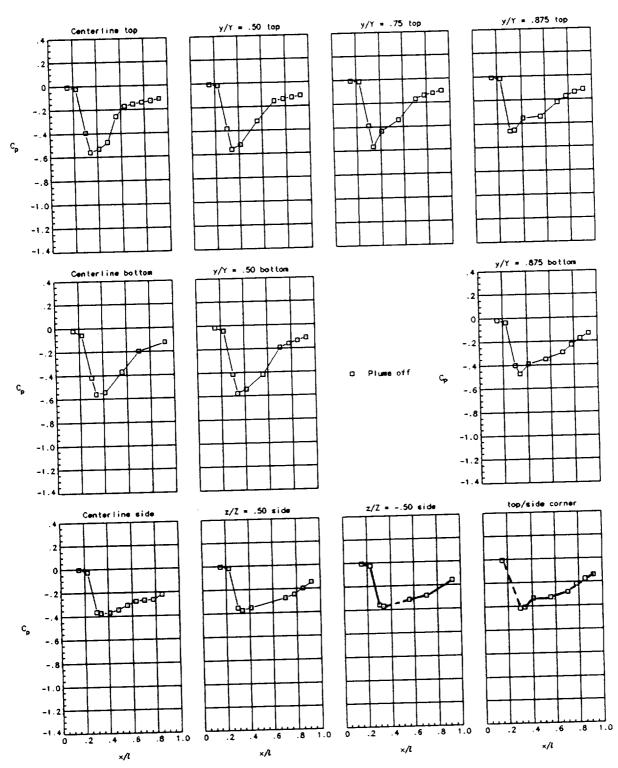


(j) Nozzle 6 with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ and 1-in. corner radius at $M_{\infty} = 0.6$. $C_{p,\text{crit}} = -1.290$.

Figure 7. Continued.

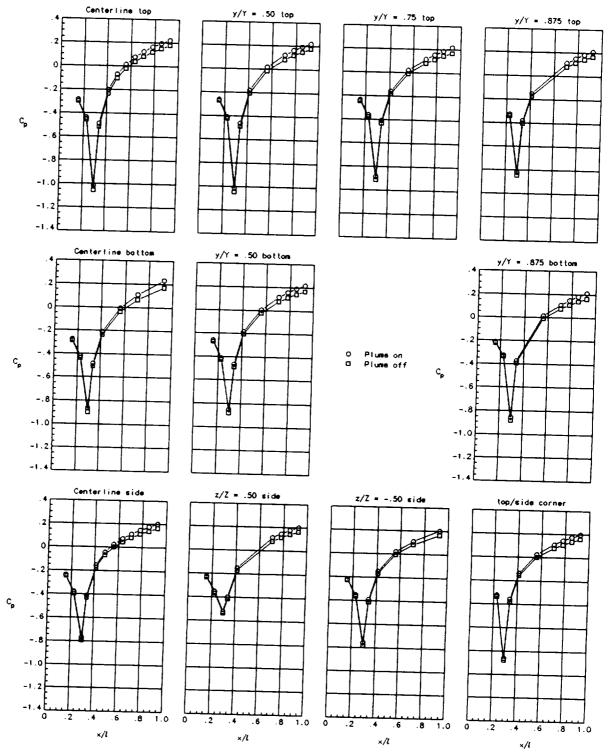


(k) Nozzle 6 with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ and 1-in. corner radius at $M_{\infty} = 0.9$. $C_{p,\text{crit}} = -0.188$. Figure 7. Continued.

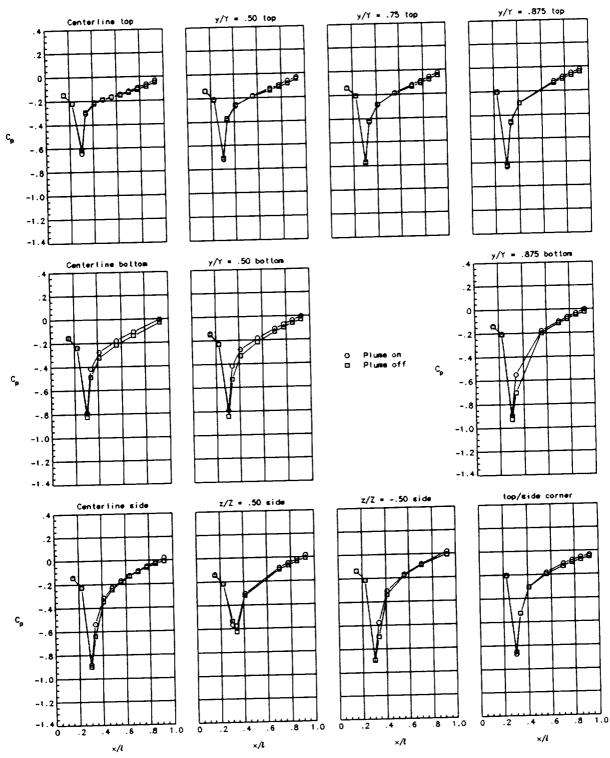


(l) Nozzle 6 with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ and 1-in. corner radius at $M_{\infty} = 1.2$. $C_{p,\text{crit}} = 0.279$.

Figure 7. Continued.

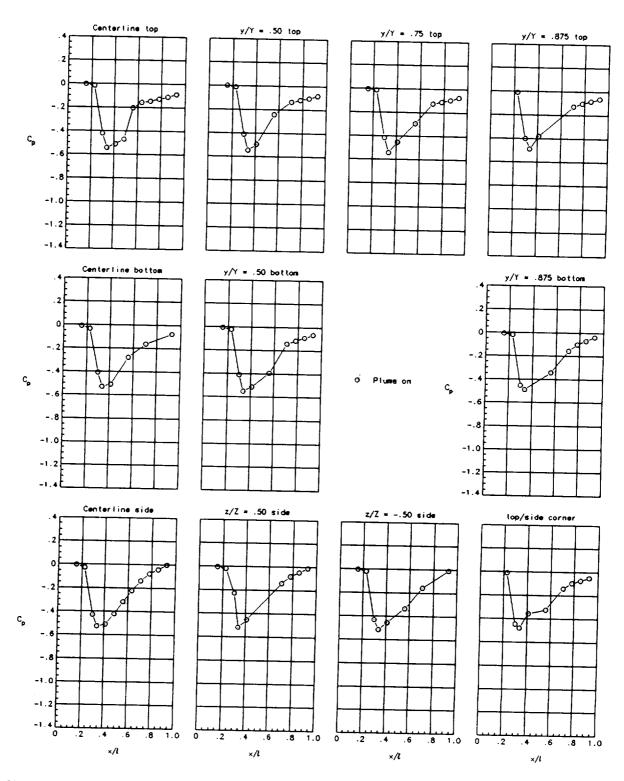


(m) Nozzle 7 with $\beta_{t,\text{top/bot}} = 16.4^{\circ}/\beta_{t,\text{side}} = 16.4^{\circ}$ and 1-in. corner radius at $M_{\infty} = 0.6$. $C_{p,\text{crit}} = -1.290$. Figure 7. Continued.

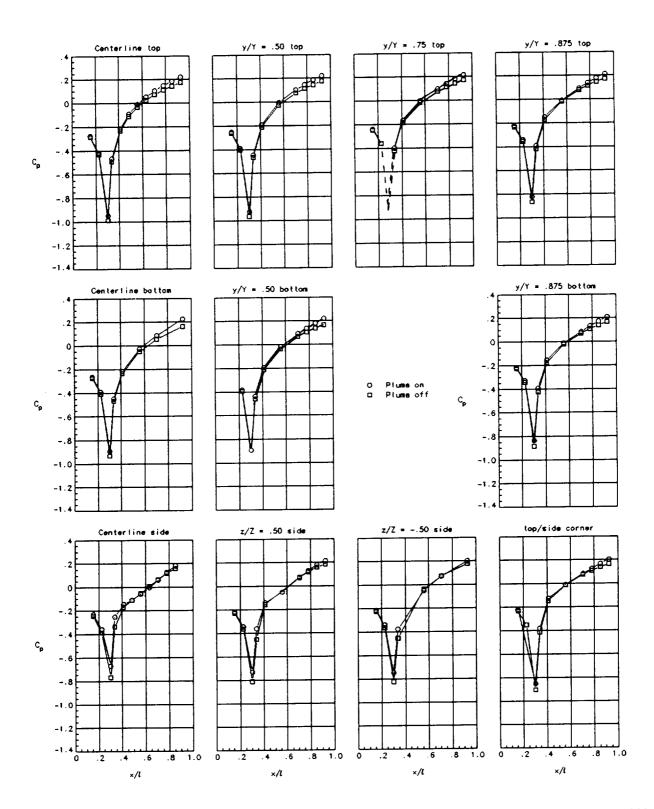


(n) Nozzle 7 with $\beta_{t,\text{top/bot}} = 16.4^{\circ}/\beta_{t,\text{side}} = 16.4^{\circ}$ and 1-in. corner radius at $M_{\infty} = 0.9$. $C_{p,\text{crit}} = -0.188$.

Figure 7. Continued.

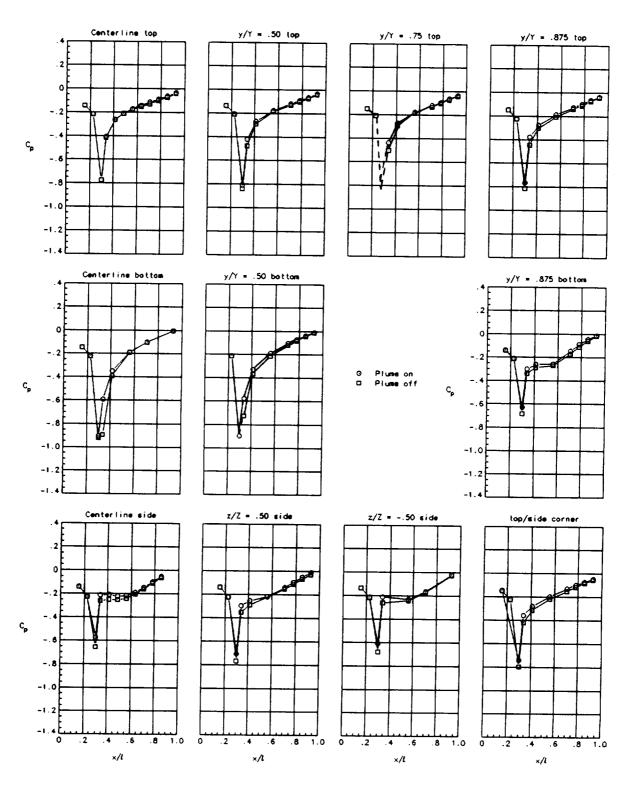


(o) Nozzle 7 with $\beta_{t,\mathrm{top/bot}}=16.4^\circ/\beta_{t,\mathrm{side}}=16.4^\circ$ and 1-in. corner radius at $M_\infty=1.2$. $C_{p,\mathrm{crit}}=0.279$. Figure 7. Continued.

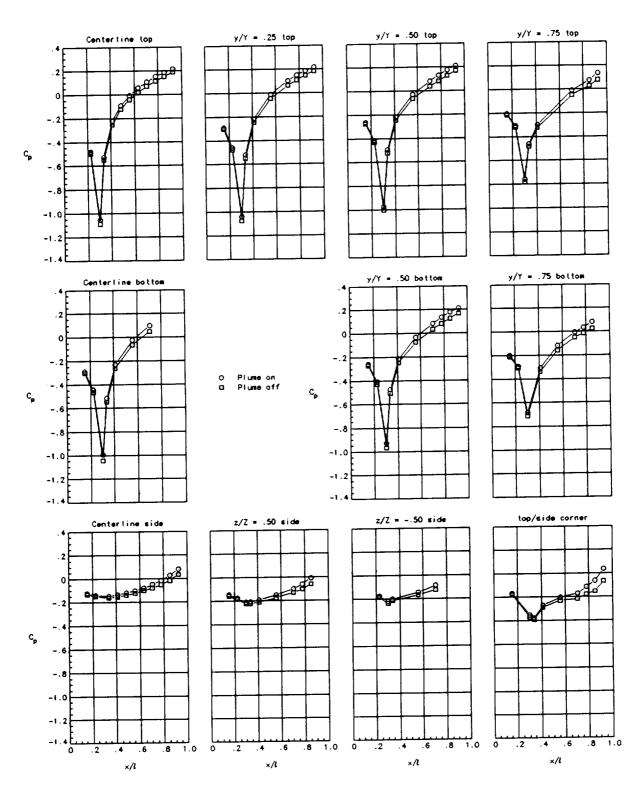


(p) Nozzle 8 with $\beta_{t,\text{top/bot}} = 15.0^{\circ}/\beta_{t,\text{side}} = 22.4^{\circ}$ and 1-in. corner radius at $M_{\infty} = 0.6$. $C_{p,\text{crit}} = -1.290$.

Figure 7. Continued.

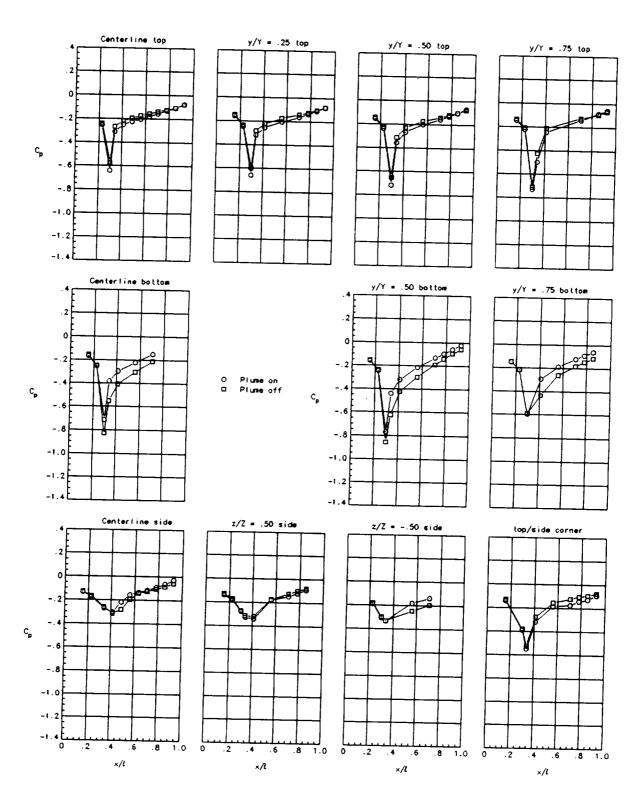


(q) Nozzle 8 with $\beta_{t,\text{top/bot}} = 15.0^{\circ}/\beta_{t,\text{side}} = 22.4^{\circ}$ and 1-in. corner radius at $M_{\infty} = 0.9$. $C_{p,\text{crit}} = -0.188$. Figure 7. Continued.

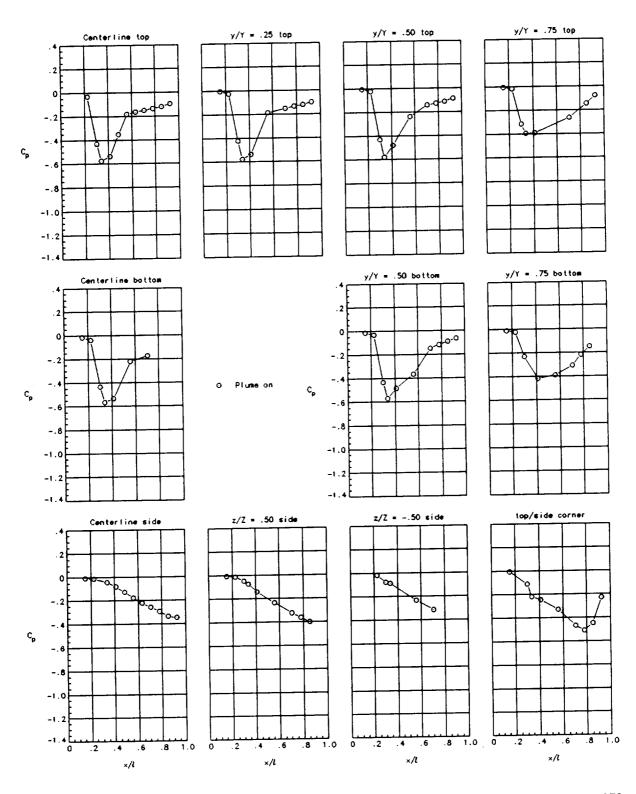


(r) Nozzle 9 with $\beta_{t,\text{top/bot}} = 17.9^{\circ}/\beta_{t,\text{side}} = 0^{\circ}$ and 2-in. corner radius at $M_{\infty} = 0.6$. $C_{p,\text{crit}} = -1.290$.

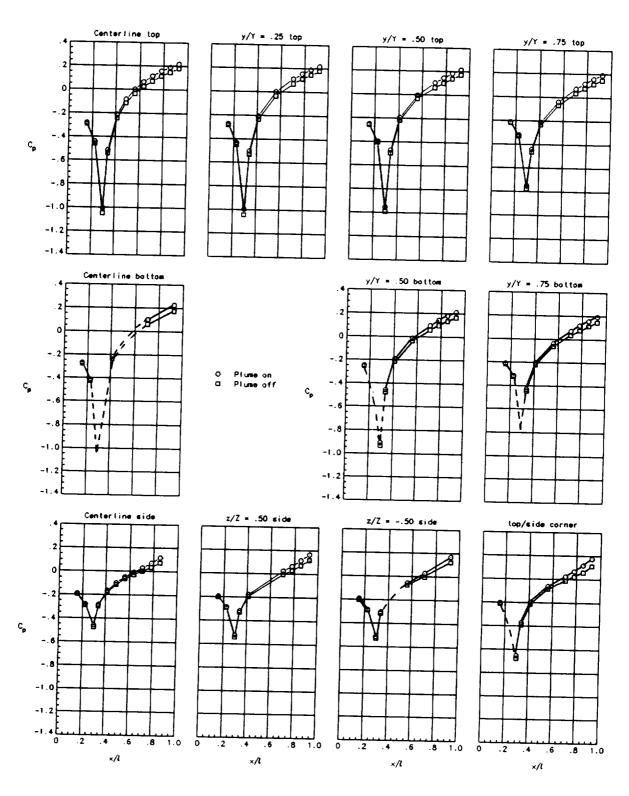
Figure 7. Continued.



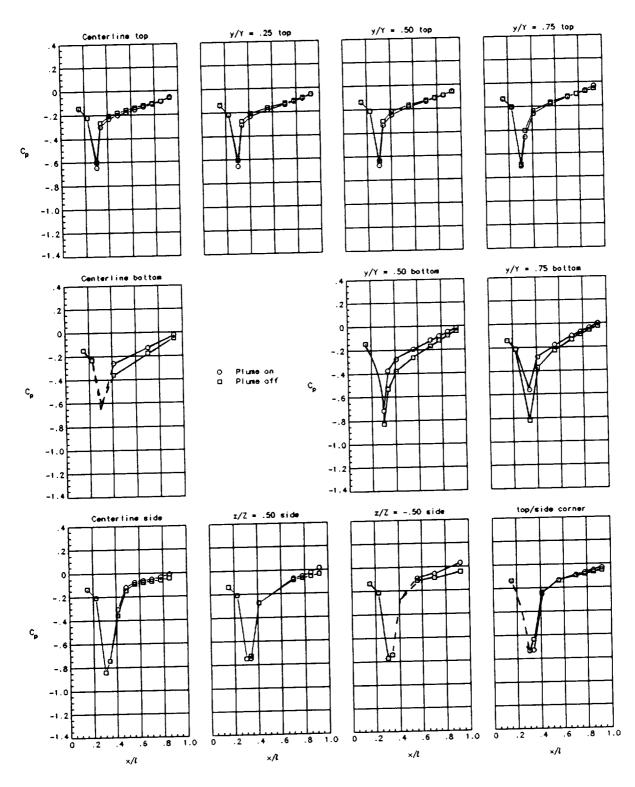
(s) Nozzle 9 with $\beta_{t,\text{top/bot}} = 17.9^{\circ}/\beta_{t,\text{side}} = 0^{\circ}$ and 2-in. corner radius at $M_{\infty} = 0.9$. $C_{p,\text{crit}} = -0.188$. Figure 7. Continued.



(t) Nozzle 9 with $\beta_{t,\text{top/bot}} = 17.9^{\circ}/\beta_{t,\text{side}} = 0^{\circ}$ and 2-in. corner radius at $M_{\infty} = 1.2$. $C_{p,\text{crit}} = 0.279$. Figure 7. Continued.

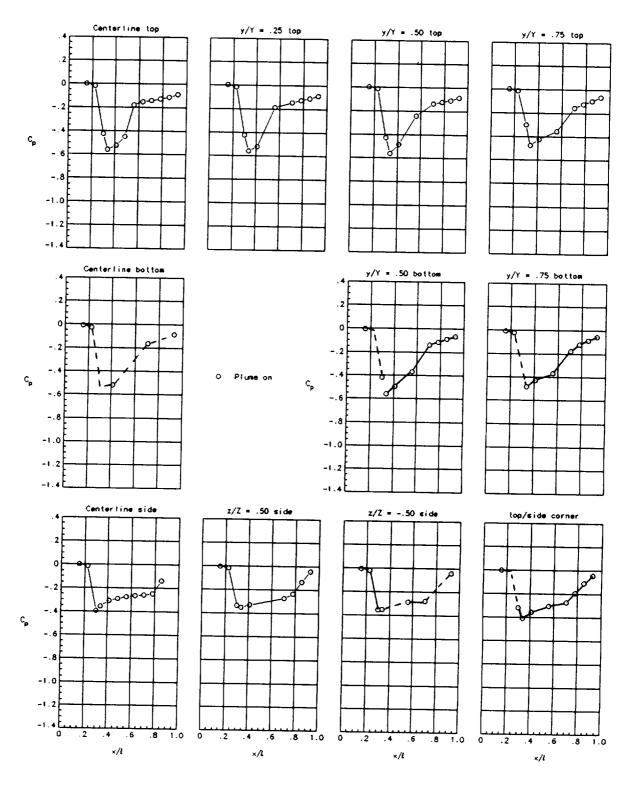


(u) Nozzle 10 with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ and 2-in. corner radius at $M_{\infty} = 0.6$. $C_{p,\text{crit}} = -1.290$. Figure 7. Continued.

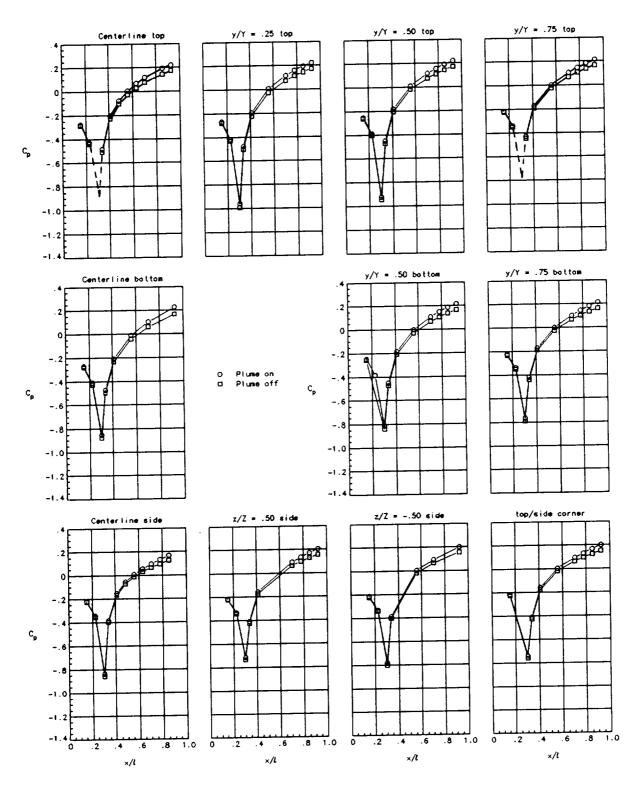


(v) Nozzle 10 with $\beta_{t,\mathrm{top/bot}} = 17.3^{\circ}/\beta_{t,\mathrm{side}} = 9.7^{\circ}$ and 2-in. corner radius at $M_{\infty} = 0.9$. $C_{p,\mathrm{crit}} = -0.188$.

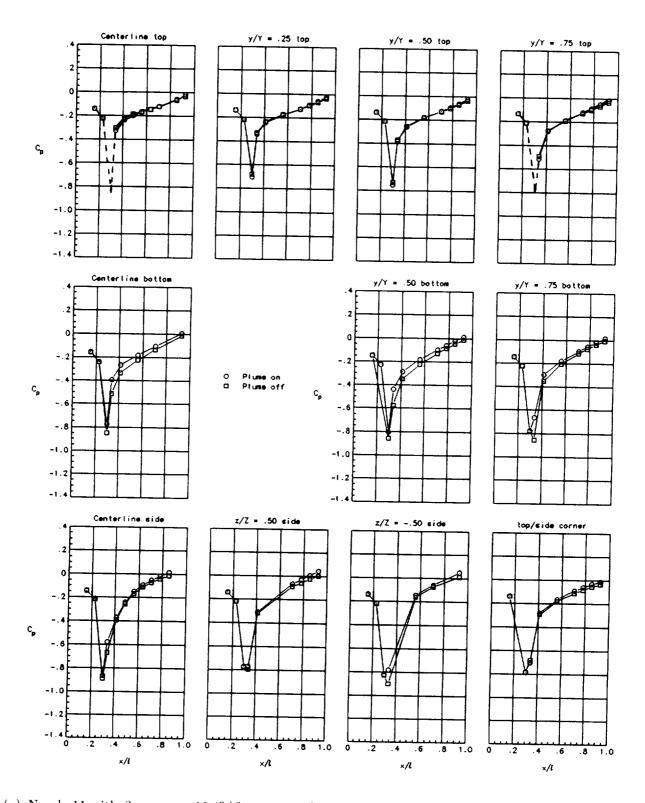
Figure 7. Continued.



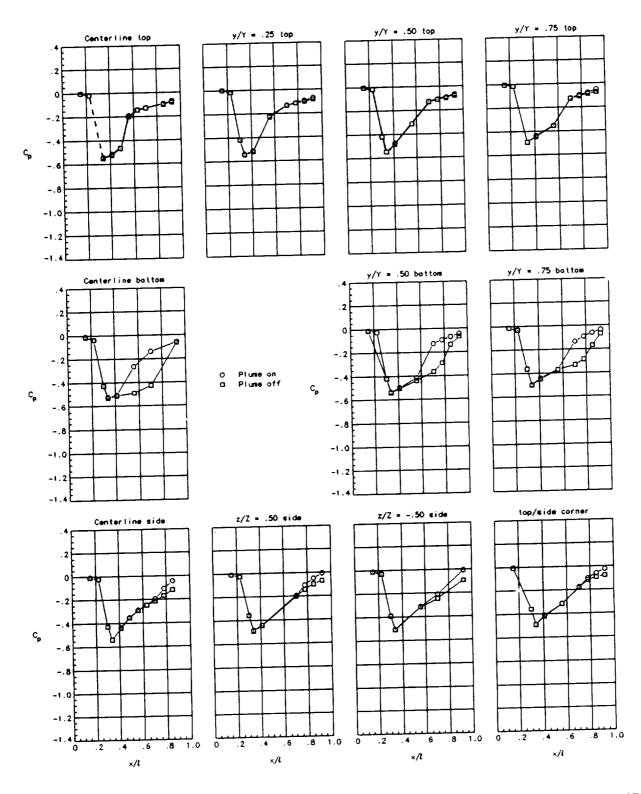
(w) Nozzle 10 with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ and 2-in. corner radius at $M_{\infty} = 1.2$. $C_{p,\text{crit}} = 0.279$. Figure 7. Continued.



(x) Nozzle 11 with $\beta_{t,\text{top/bot}} = 16.4^{\circ}/\beta_{t,\text{side}} = 16.4^{\circ}$ and 2-in. corner radius at $M_{\infty} = 0.6$. $C_{p,\text{crit}} = -1.290$. Figure 7. Continued.

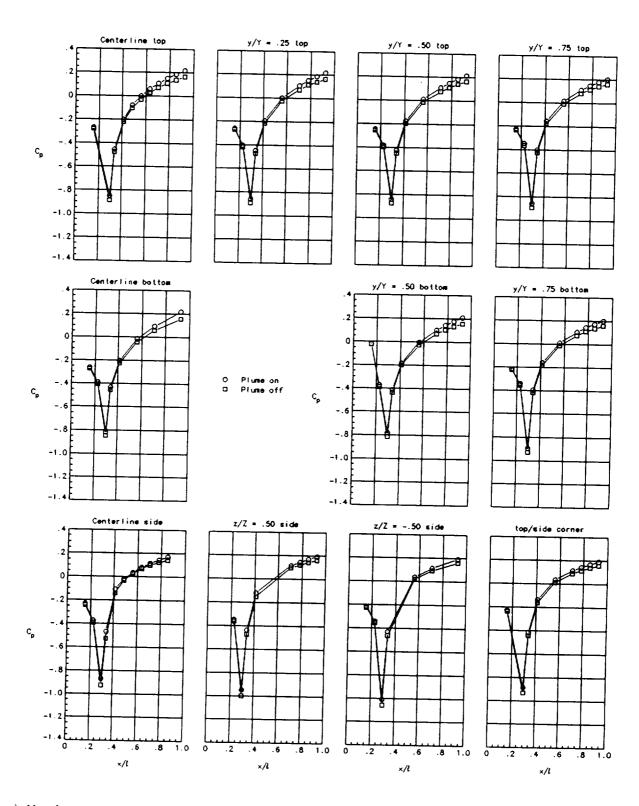


(y) Nozzle 11 with $\beta_{t,\text{top/bot}} = 16.4^{\circ}/\beta_{t,\text{side}} = 16.4^{\circ}$ and 2-in. corner radius at $M_{\infty} = 0.9$. $C_{p,\text{crit}} = -0.188$. Figure 7. Continued.

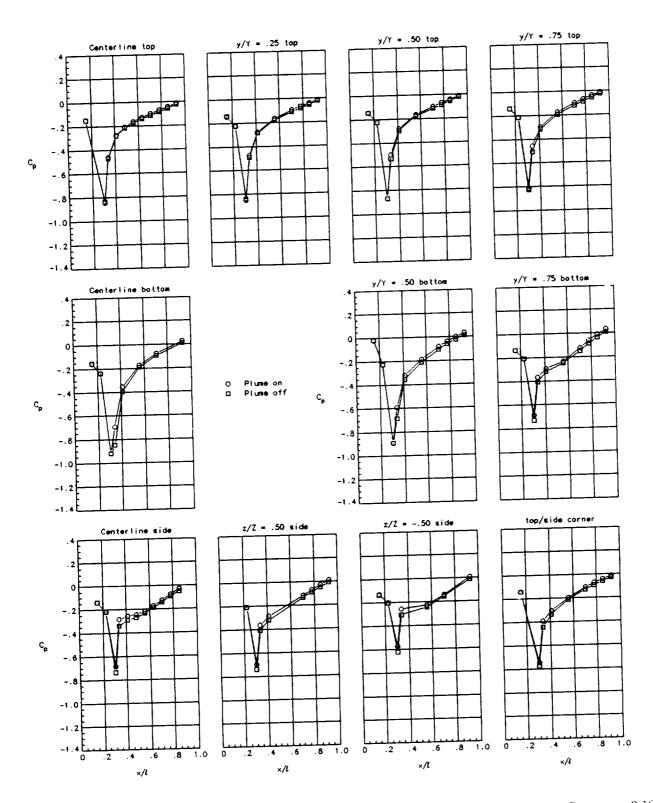


(z) Nozzle 11 with $\beta_{t,\text{top/bot}} = 16.4^{\circ}/\beta_{t,\text{side}} = 16.4^{\circ}$ and 2-in. corner radius at $M_{\infty} = 1.2$. $C_{p,\text{crit}} = 0.279$.

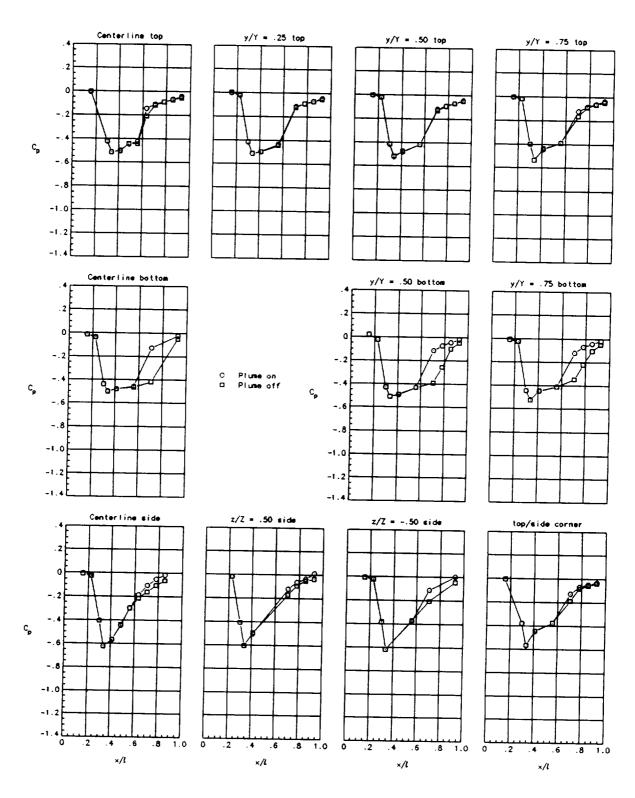
Figure 7. Continued.



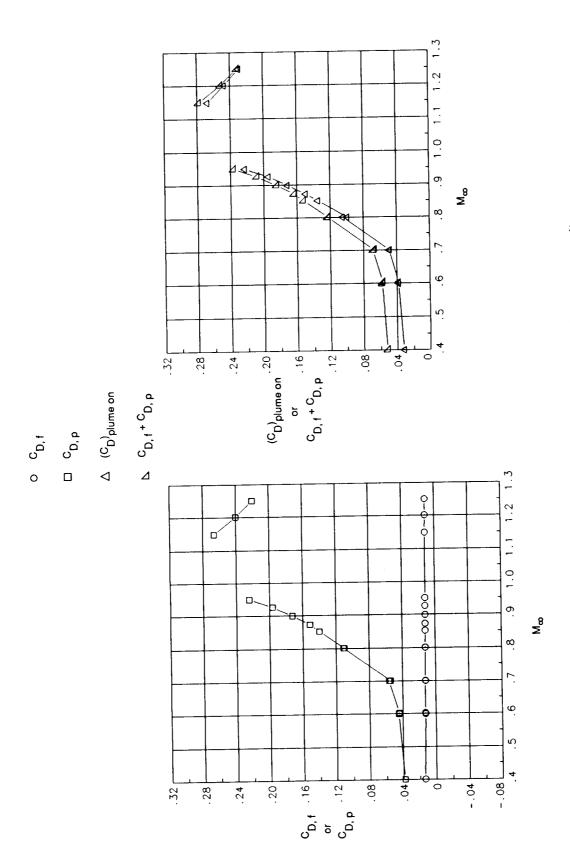
(aa) Nozzle 12 with $\beta_{t,\text{top/bot}} = 15.0^{\circ}/\beta_{t,\text{side}} = 22.4^{\circ}$ and 2-in. corner radius at $M_{\infty} = 0.6$. $C_{p,\text{crit}} = -1.290$. Figure 7. Continued.



(bb) Nozzle 12 with $\beta_{t,\text{top/bot}} = 15.0^{\circ}/\beta_{t,\text{side}} = 22.4^{\circ}$ and 2-in. corner radius at $M_{\infty} = 0.9$. $C_{p,\text{crit}} = -0.188$. Figure 7. Continued.

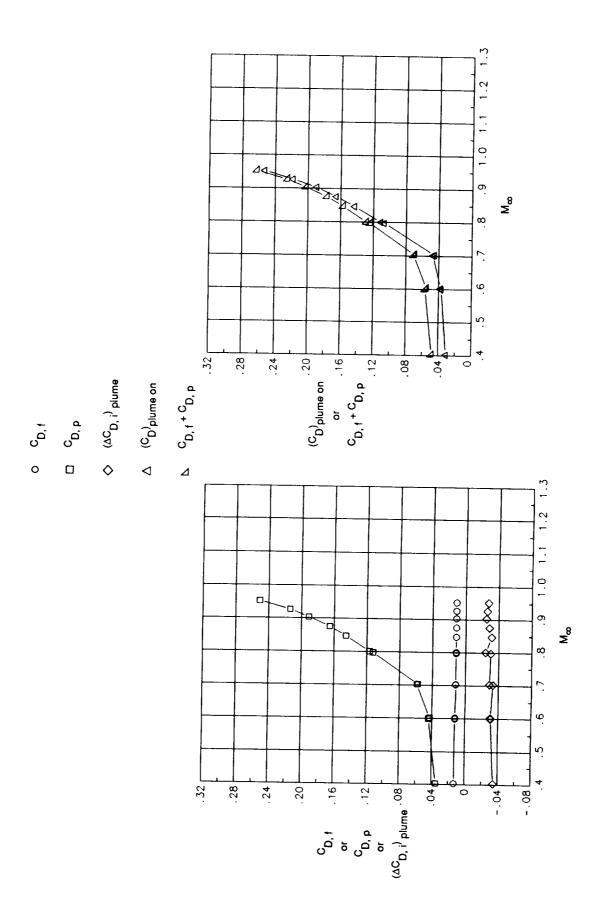


(cc) Nozzle 12 with $\beta_{t,\text{top/bot}} = 15.0^{\circ}/\beta_{t,\text{side}} = 22.4^{\circ}$ and 2-in. corner radius at $M_{\infty} = 1.2$. $C_{p,\text{crit}} = 0.279$. Figure 7. Concluded.



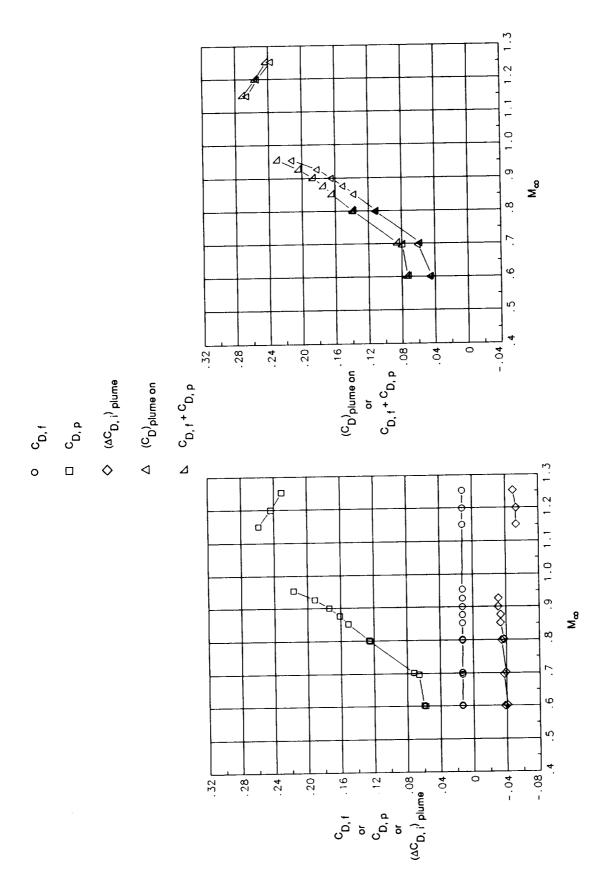
(a) Nozzle 2 with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ and sharp-corner radius.

Figure 8. Various component drag coefficients as a function of Mach number at $\alpha=0^\circ.$



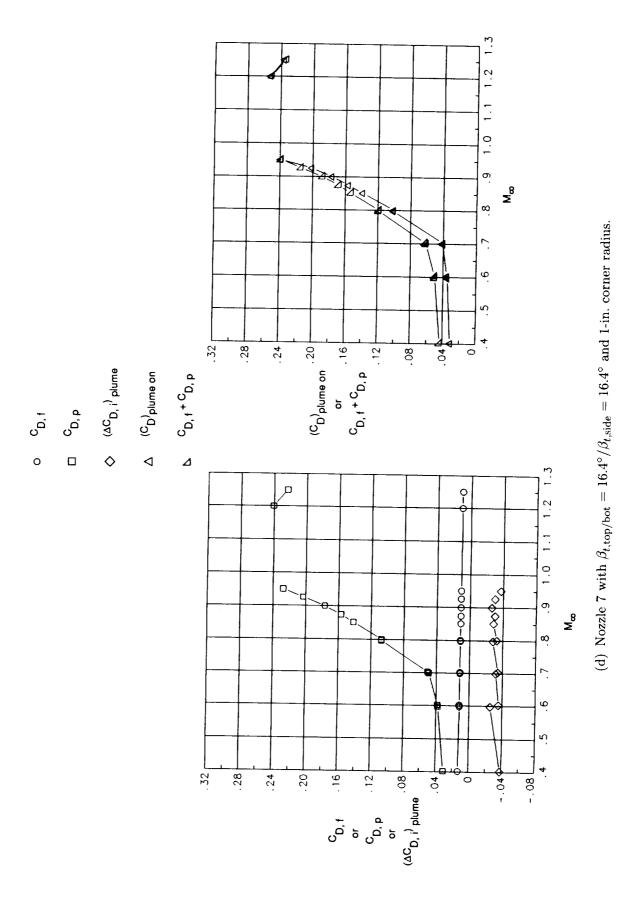
(b) Nozzle 3 with $\beta_{t,\text{top/bot}} = 16.4^{\circ}/\beta_{t,\text{side}} = 16.4^{\circ}$ and sharp-corner radius.

224

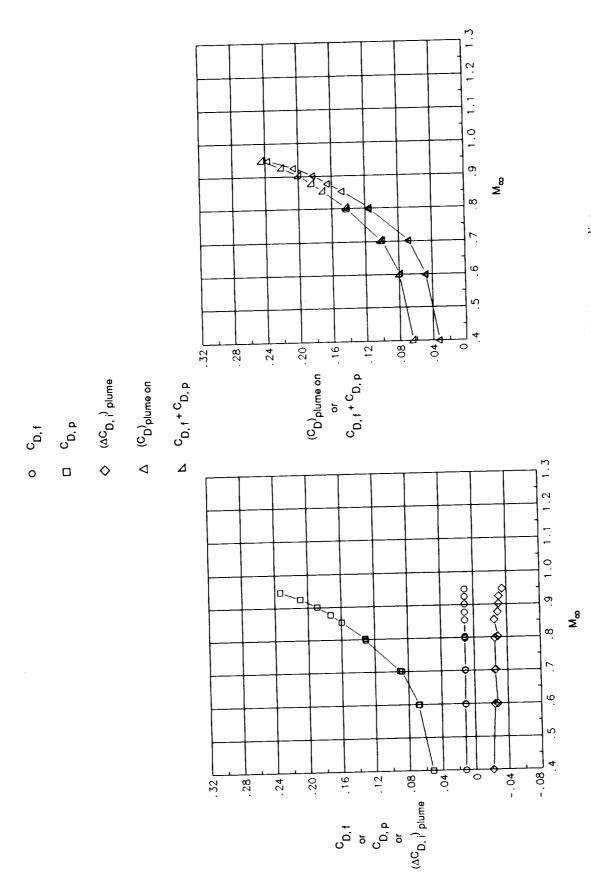


(c) Nozzle 5 with $\beta_{t,\text{top/bot}} = 17.9^{\circ}/\beta_{t,\text{side}} = 0^{\circ}$ and 1-in. corner radius.

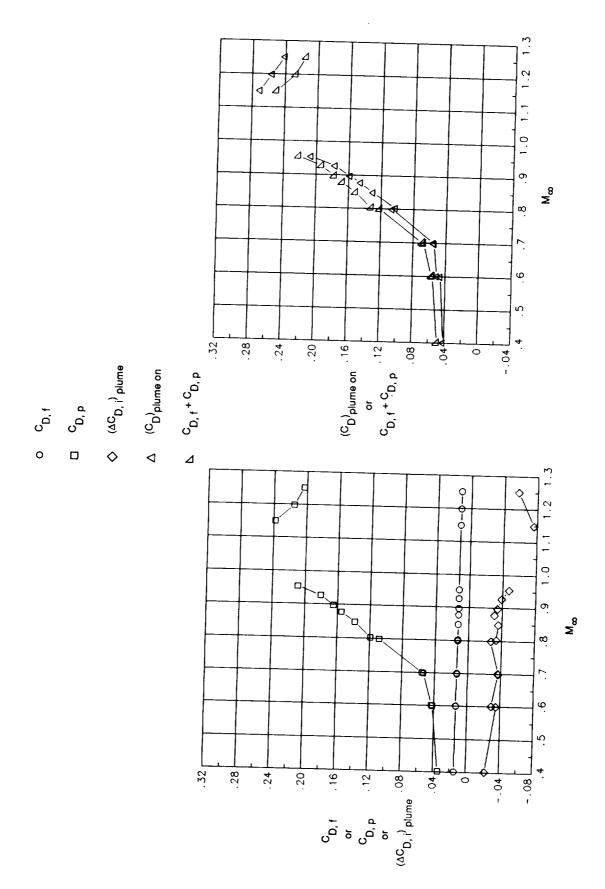
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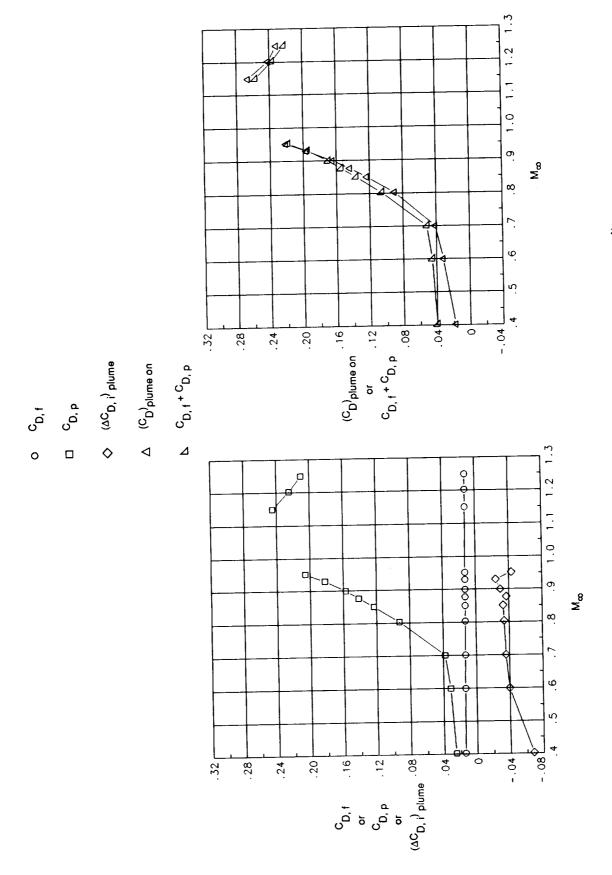
226



(e) Nozzle 8 with $\beta_{t,\text{top/bot}}=15.0^{\circ}/\beta_{t,\text{side}}=22.4^{\circ}$ and 1-in. corner radius. Figure 8. Continued.

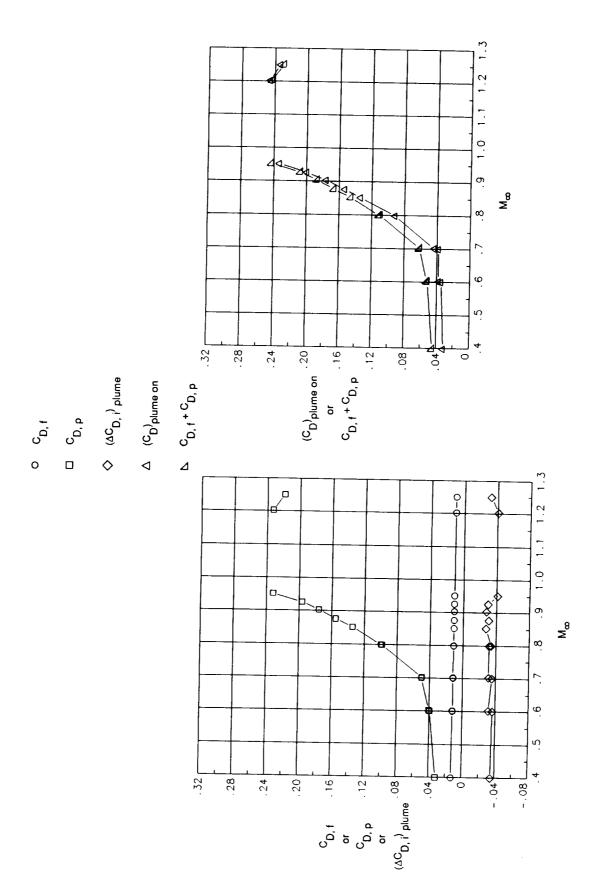


(f) Nozzle 9 with $\beta_{t,\text{top/bot}} = 17.9^{\circ}/\beta_{t,\text{side}} = 0^{\circ}$ and 2-in. corner radius.

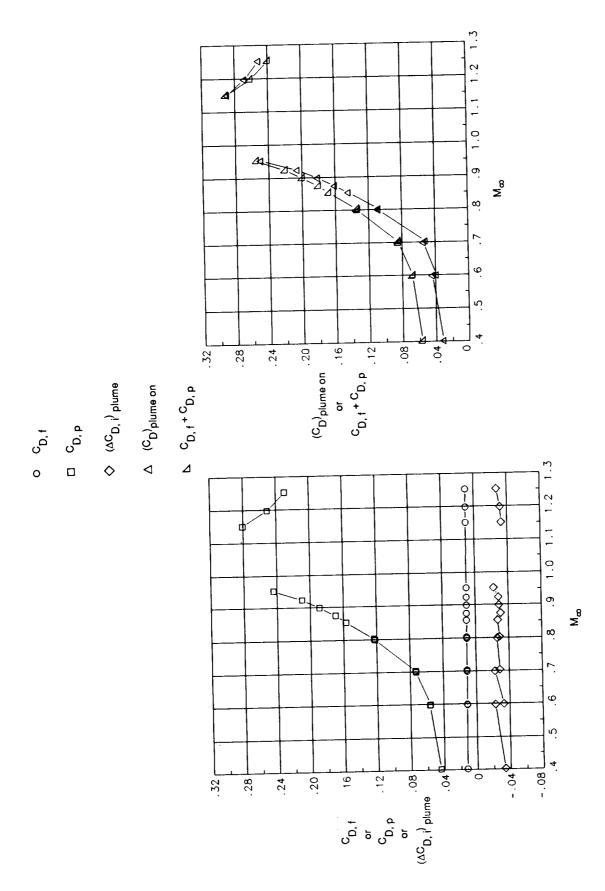


(g) Nozzle 10 with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ and 2-in. corner radius.

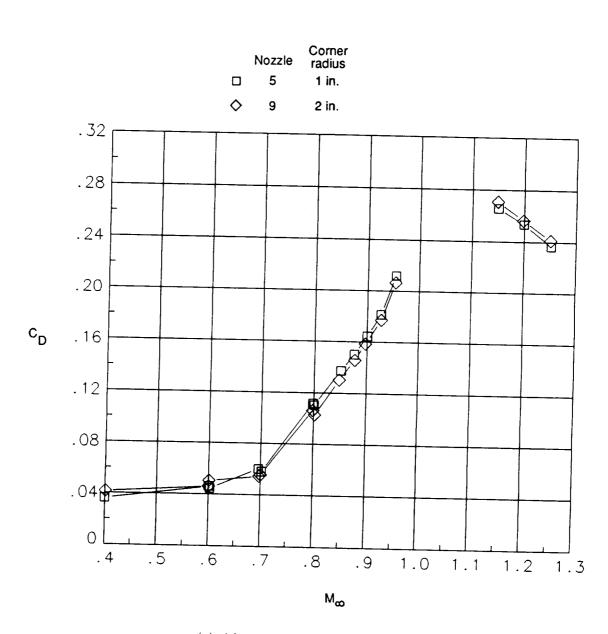
229



(h) Nozzle 11 with $\beta_{t,\text{top/bot}}=16.4^\circ/\beta_{t,\text{side}}=16.4^\circ$ and 2-in. corner radius. Figure 8. Continued.

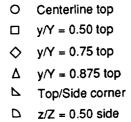


(i) Nozzle 12 with $\beta_{t,\text{top/bot}}=15.0^\circ/\beta_{t,\text{side}}=22.4^\circ$ and 2-in. corner radius. Figure 8. Concluded.



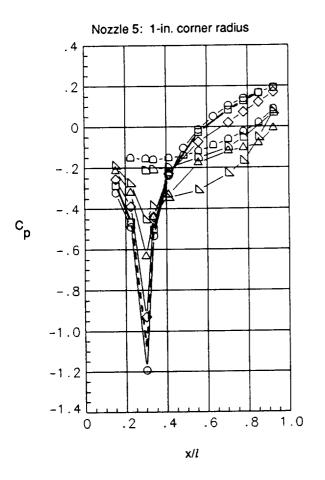
(a) Afterbody drag with plume on.

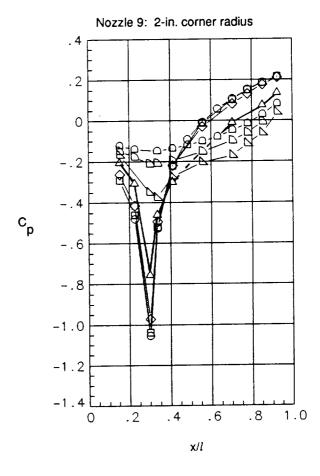
Figure 9. Effect of corner radius on nozzles with $\beta_{t,\text{top/bot}} = 17.9^{\circ}/\beta_{t,\text{side}} = 0^{\circ}$ at $\alpha = 0^{\circ}$.



Centerline side

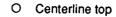
Centerline top 0 y/Y = 0.25 topy/Y = 0.50 topy/Y = 0.75 topTop/Side corner z/Z = 0.50 side $\boldsymbol{\sigma}$ Centerline side





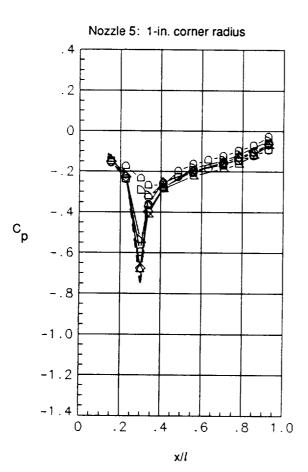
(b) Pressure distributions at $M_{\infty} = 0.6$.

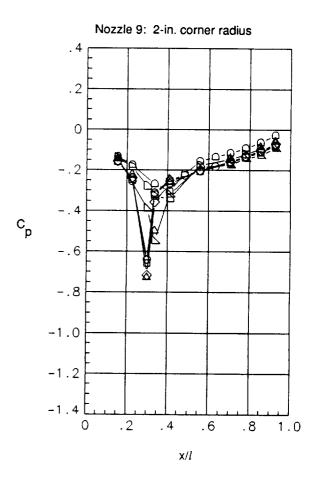
Figure 9. Continued.



- \Box y/Y = 0.50 top
- \diamondsuit y/Y = 0.75 top
- Δ y/Y = 0.875 top
- \triangle z/Z = 0.50 side
- Centerline side

- Centerline top
- y/Y = 0.25 top
- \Rightarrow y/Y = 0.50 top
- \triangle y/Y = 0.75 top
- \triangle z/Z = 0.50 side
- □ Centerline side





(c) Pressure distributions at $M_{\infty} = 0.9$.

Figure 9. Continued.

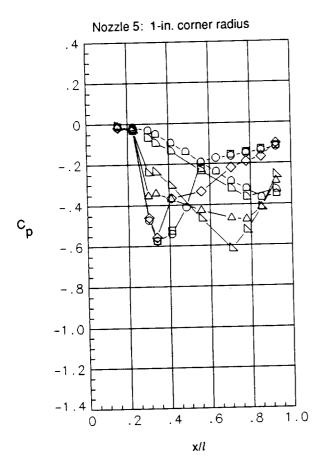


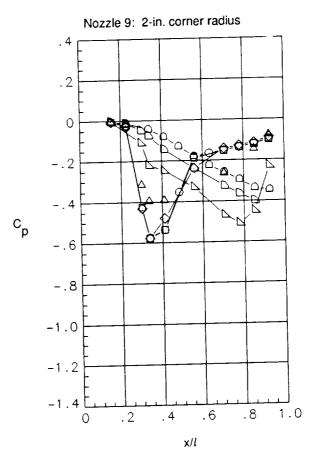
$$y/Y = 0.50 \text{ top}$$

$$\Rightarrow$$
 y/Y = 0.75 top

- \triangle y/Y = 0.875 top
- \triangle z/Z = 0.50 side
- □ Centerline side

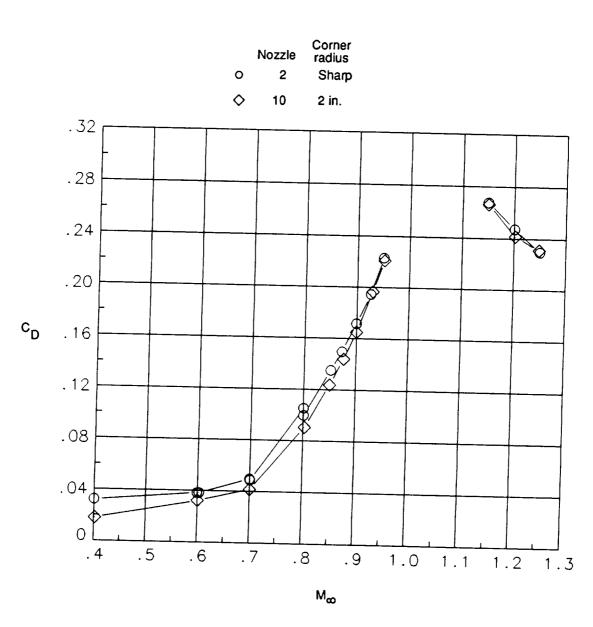
- O Centerline top
- y/Y = 0.25 top
- \Rightarrow y/Y = 0.50 top
- Δ y/Y = 0.75 top
- \triangle z/Z = 0.50 side
- □ Centerline side





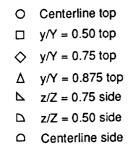
(d) Pressure distributions at $M_{\infty} = 1.2$.

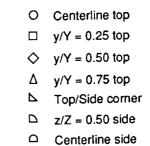
Figure 9. Concluded.

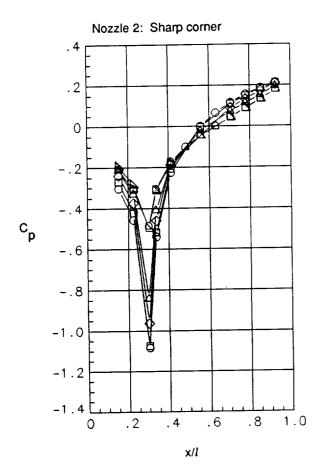


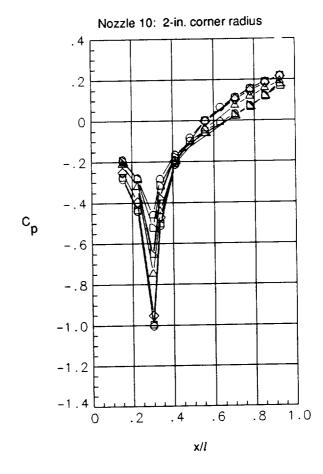
(a) Afterbody drag with plume on.

Figure 10. Effect of corner radius on nozzles with $\beta_{t,\text{top/bot}} = 17.3^{\circ}/\beta_{t,\text{side}} = 9.7^{\circ}$ at $\alpha = 0^{\circ}$.



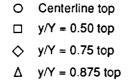






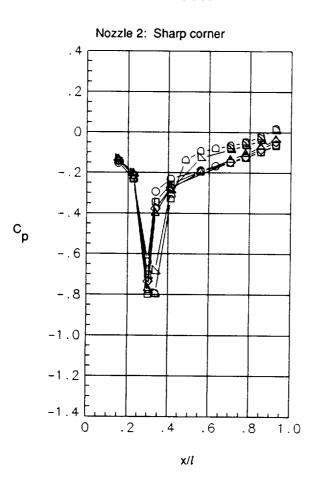
(b) Pressure distributions at $M_{\infty} = 0.6$.

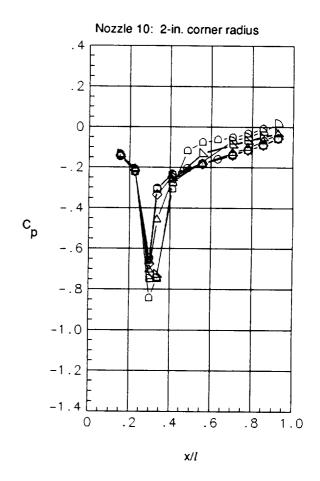
Figure 10. Continued.



- z/Z = 0.75 side \Box z/Z = 0.50 side
- Centerline side

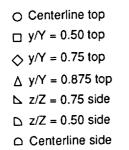
- Centerline top
- y/Y = 0.25 top
- y/Y = 0.50 top
- y/Y = 0.75 top
- Top/Side corner
- $\boldsymbol{\sigma}$ z/Z = 0.50 side
- Ω Centerline side

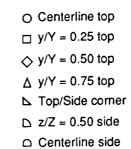


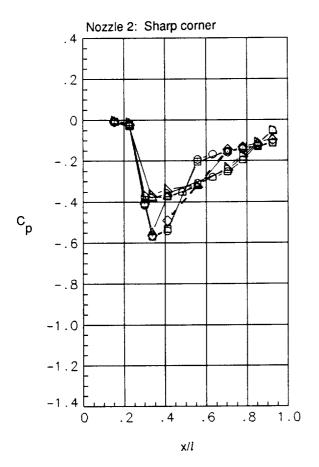


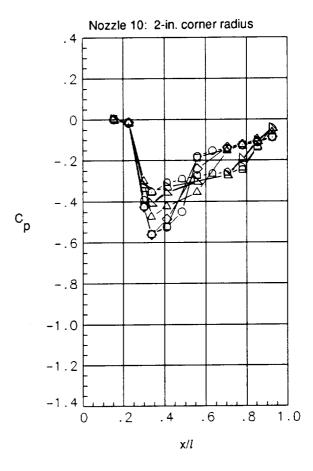
(c) Pressure distributions at $M_{\infty} = 0.9$.

Figure 10. Continued.





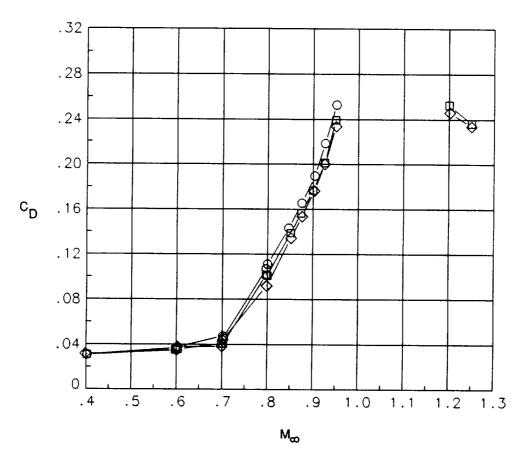




(d) Pressure distributions at $M_{\infty} = 1.2$.

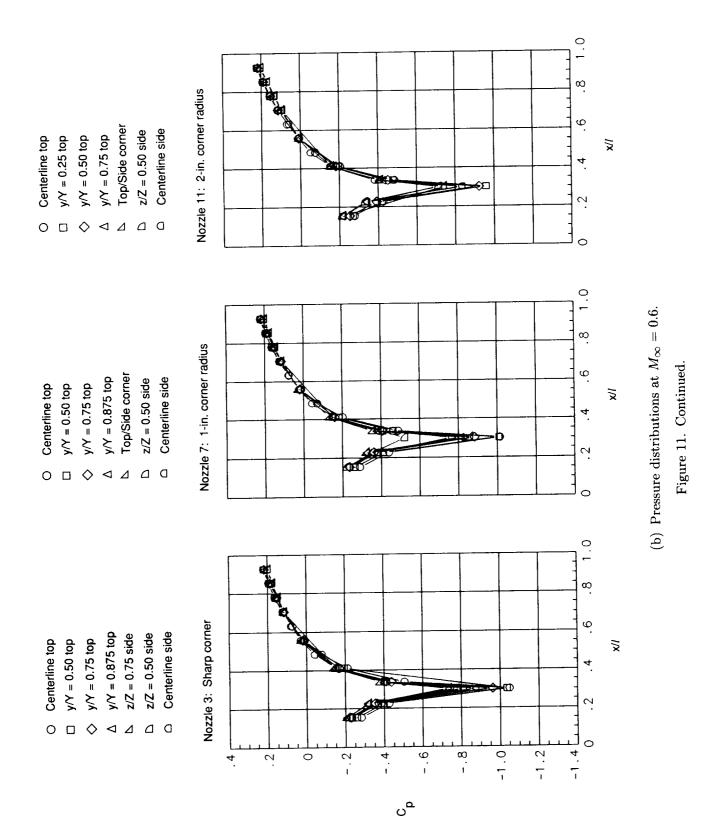
Figure 10. Concluded.

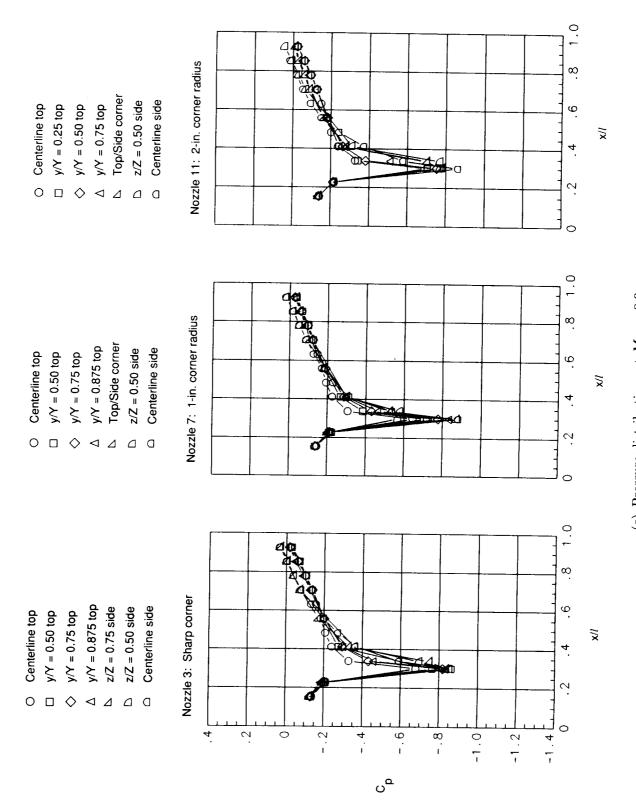
Nozzle Corner radius
O 3 Sharp
□ 7 1 in.
♦ 11 2 in.



(a) Afterbody drag with plume on.

Figure 11. Effect of corner radius on nozzles with $\beta_{t,\mathrm{top/bot}} = \beta_{t,\mathrm{side}} = 16.4^{\circ}$ at $\alpha = 0^{\circ}$.





(c) Pressure distributions at $M_{\infty}=0.9.$ Figure 11. Continued.



$$y/Y = 0.50 \text{ top}$$

$$\diamondsuit$$
 y/Y = 0.75 top

$$\triangle$$
 y/Y = 0.875 top

$$\triangle$$
 z/Z = 0.50 side

□ Centerline side

O Centerline top

$$y/Y = 0.25 \text{ top}$$

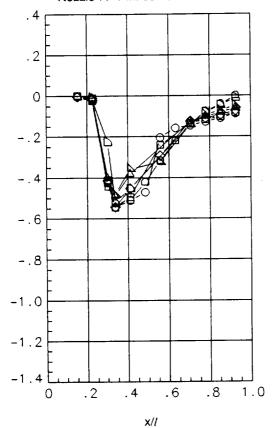
$$\diamondsuit$$
 y/Y = 0.50 top

$$\triangle$$
 y/Y = 0.75 top

$$\triangle$$
 z/Z = 0.50 side

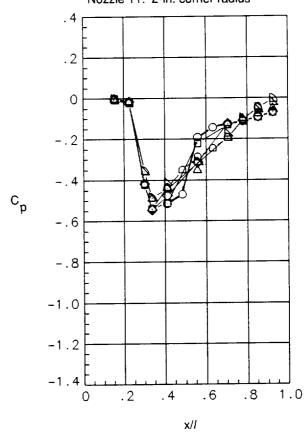
□ Centerline side

Nozzle 7: 1-in. corner radius



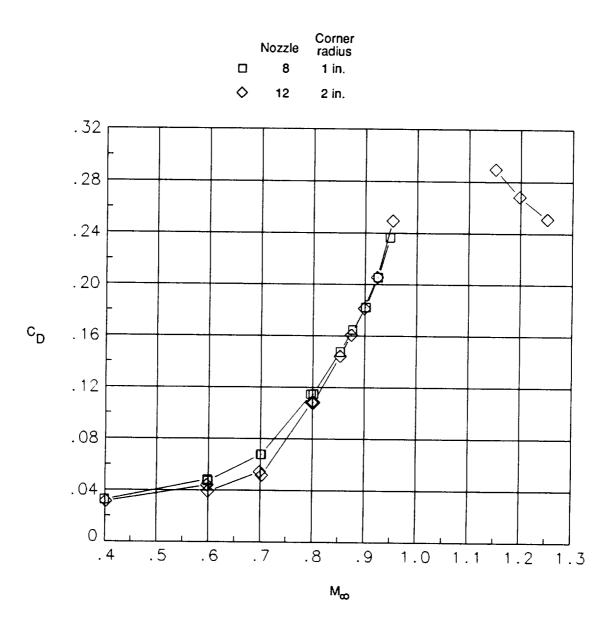
Ср

Nozzle 11: 2-in. corner radius



(d) Pressure distributions at $M_{\infty} = 1.2$.

Figure 11. Concluded.



(a) Afterbody drag with plume on.

Figure 12. Effect of corner radius on nozzles with $\beta_{t, \rm top/bot} = 15^{\circ}/\beta_{t, \rm side} = 22.4^{\circ}$ at $\alpha = 0^{\circ}$.



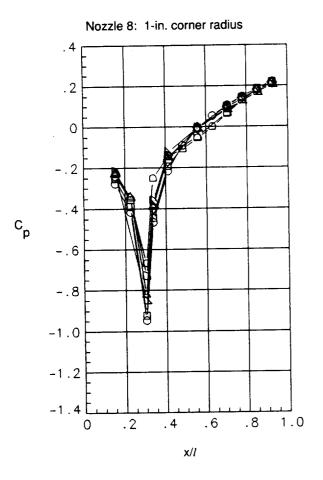
$$y/Y = 0.50 \text{ top}$$

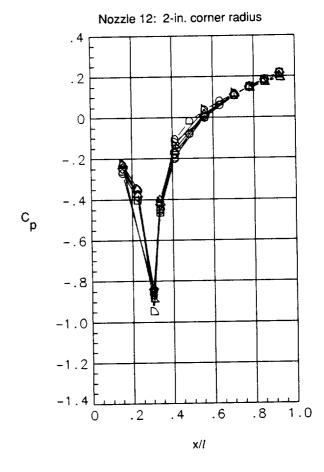
$$\Diamond$$
 y/Y = 0.75 top

$$\triangle$$
 y/Y = 0.875 top

- \triangle z/Z = 0.50 side
- □ Centerline side

- O Centerline top
- y/Y = 0.25 top
- \diamondsuit y/Y = 0.50 top
- \triangle y/Y = 0.75 top
- \triangle z/Z = 0.50 side
- □ Centerline side



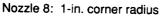


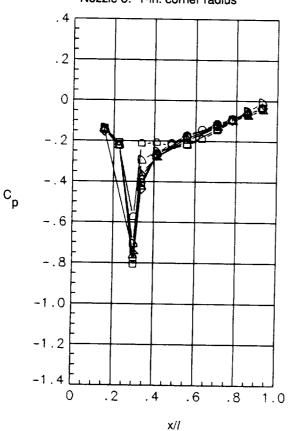
(b) Pressure distributions at $M_{\infty} = 0.6$.

Figure 12. Continued.

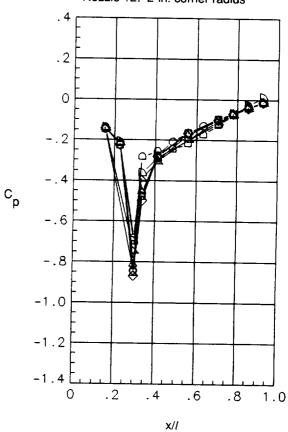
- O Centerline top
- \Box y/Y = 0.50 top
- \diamondsuit y/Y = 0.75 top
- Δ y/Y = 0.875 top
- △ Top/Side corner
- \triangle z/Z = 0.50 side
- □ Centerline side

- Centerline top
- y/Y = 0.25 top
- \diamondsuit y/Y = 0.50 top
- \triangle y/Y = 0.75 top
- \triangle z/Z = 0.50 side
- □ Centerline side





Nozzle 12: 2-in. corner radius



(c) Pressure distributions at $M_{\infty} = 0.9$.

Figure 12. Concluded.

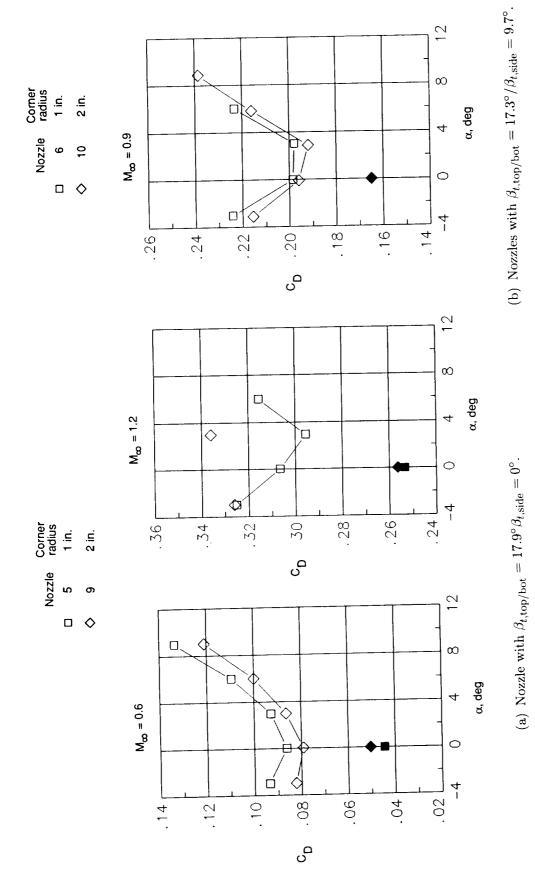
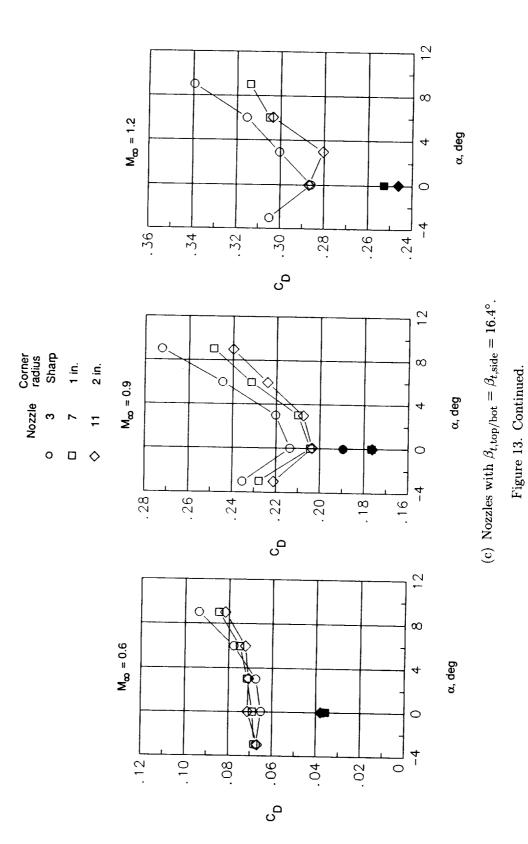
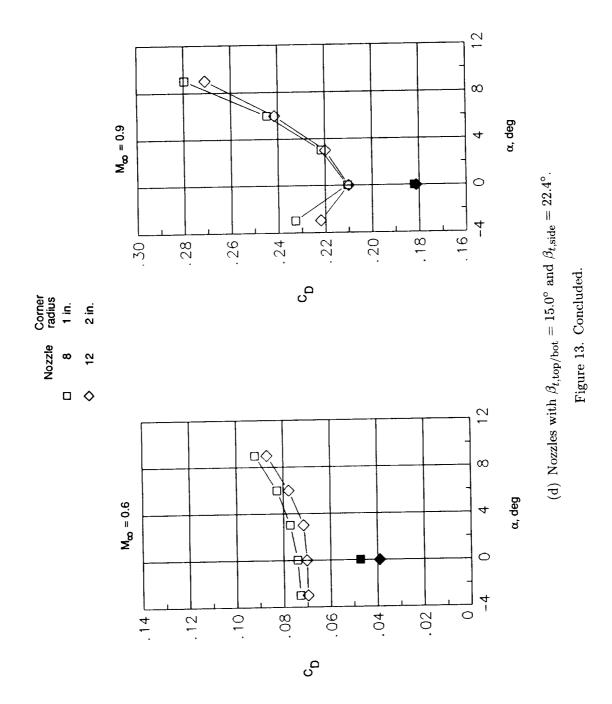
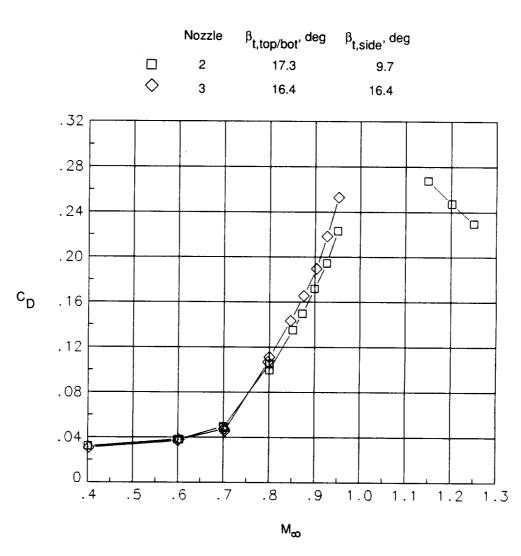


Figure 13. Effect of corner radius on afterbody drag. Open symbols denote plume off; solid symbols denote plume on.

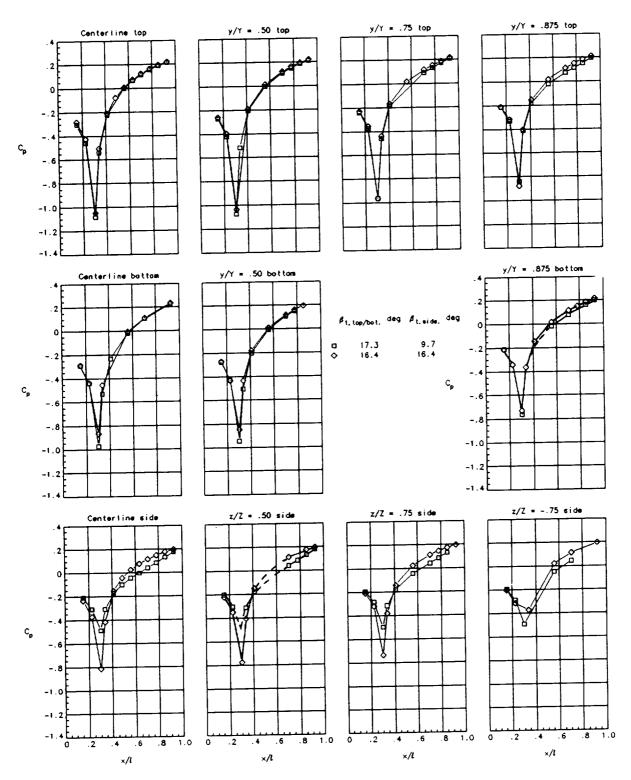






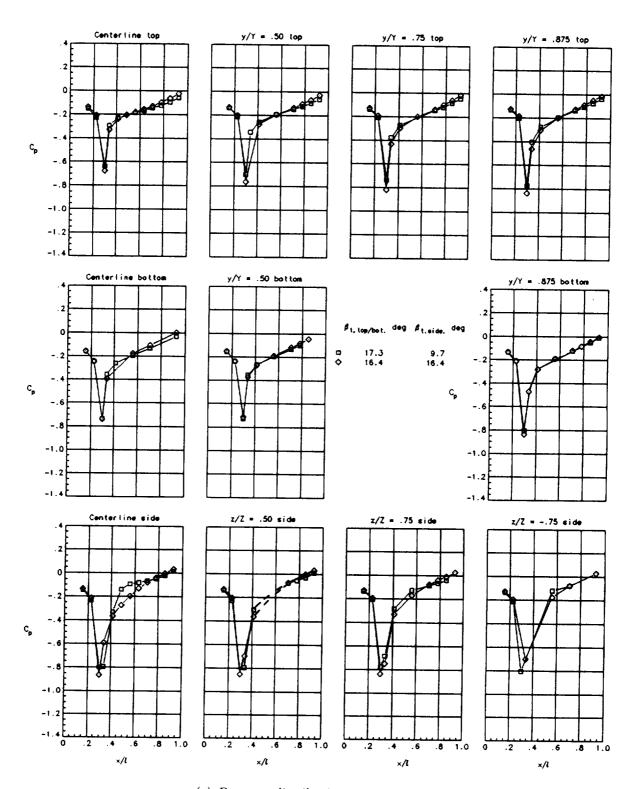
(a) Afterbody drag plume on.

Figure 14. Effect of closure distribution on nozzles with sharp corner at $\alpha=0^{\circ}$.



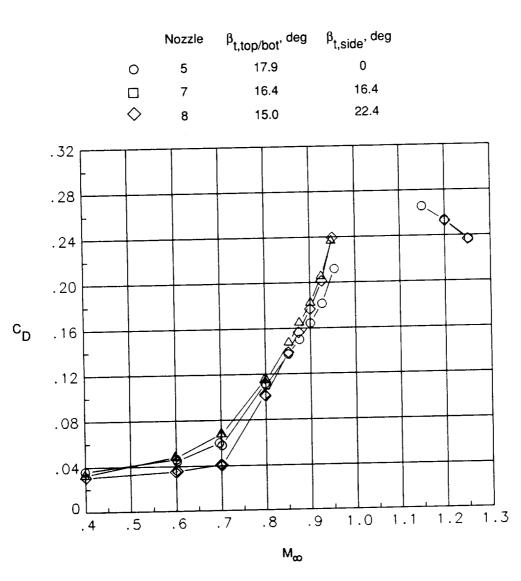
(b) Pressure distributions at $M_{\infty} = 0.6$.

Figure 14. Continued.



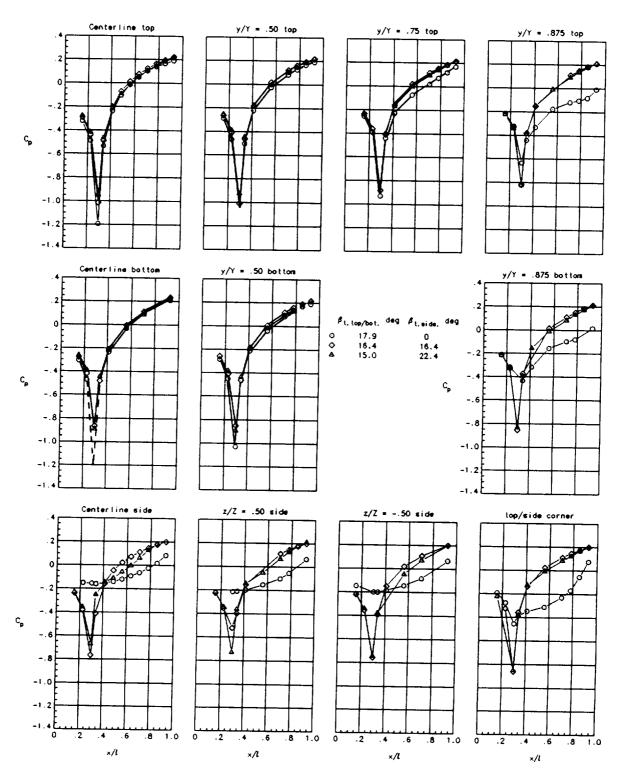
(c) Pressure distributions at $M_{\infty} = 0.9$.

Figure 14. Concluded.



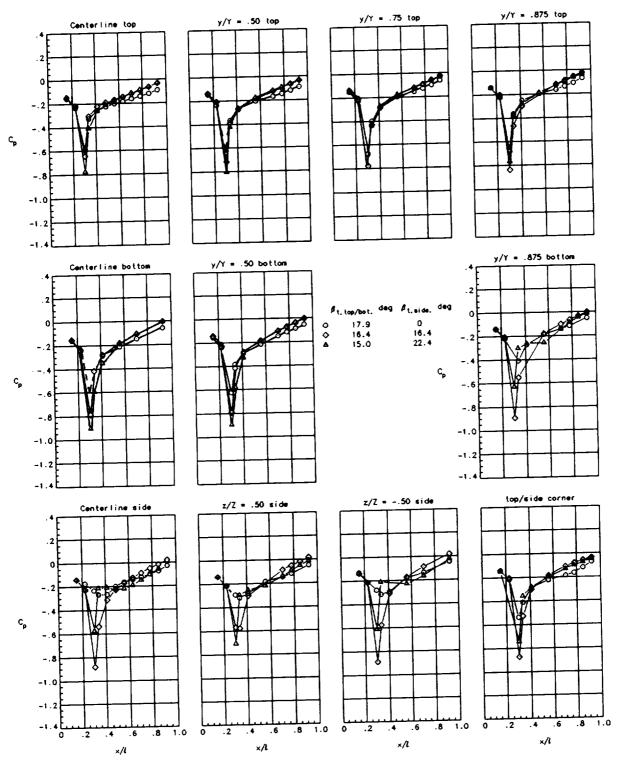
(a) Afterbody drag with plume on.

Figure 15. Effect of closure distribution on nozzles with 1-in. corner radius at $\alpha=0^{\circ}$.



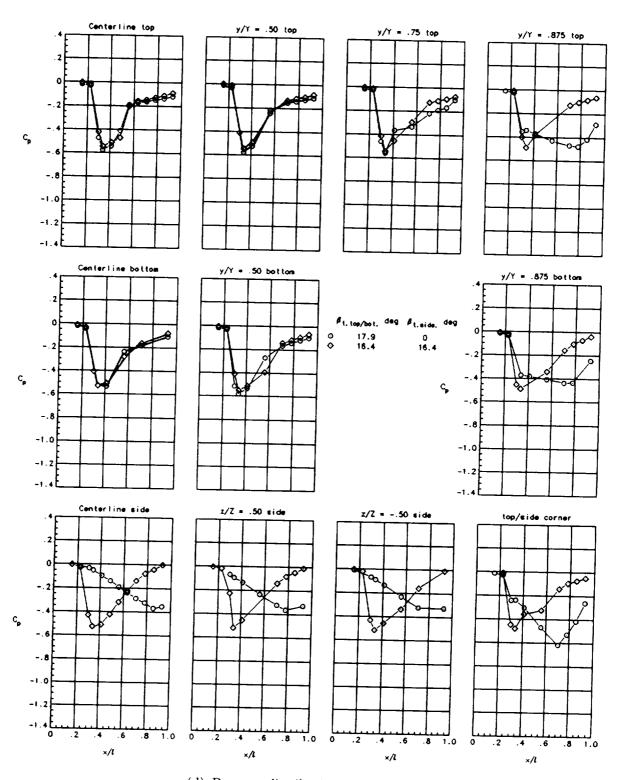
(b) Pressure distributions at $M_{\infty}=0.6$.

Figure 15. Continued.



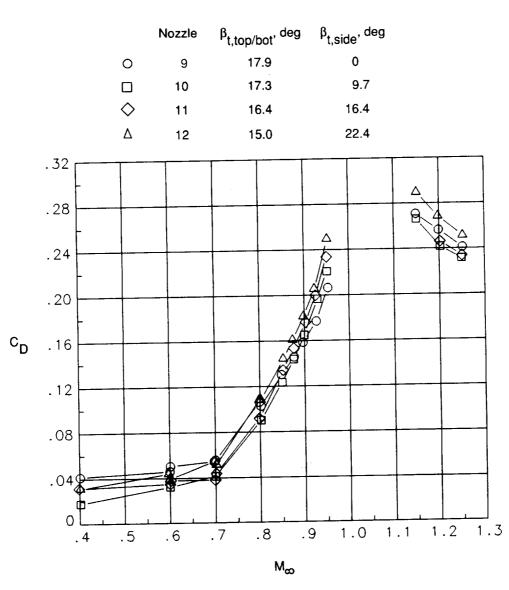
(c) Pressure distributions at $M_{\infty} = 0.9$.

Figure 15. Continued.



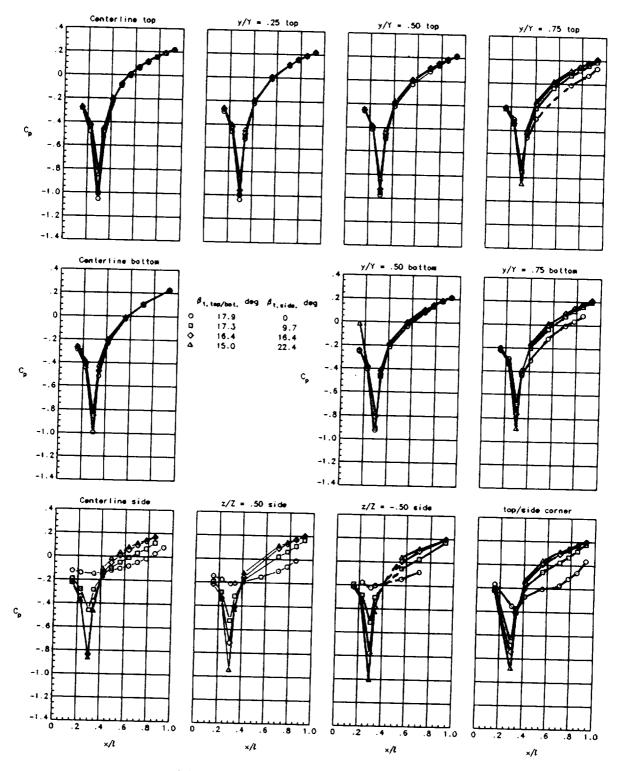
(d) Pressure distributions at $M_{\infty} = 1.2$.

Figure 15. Concluded.



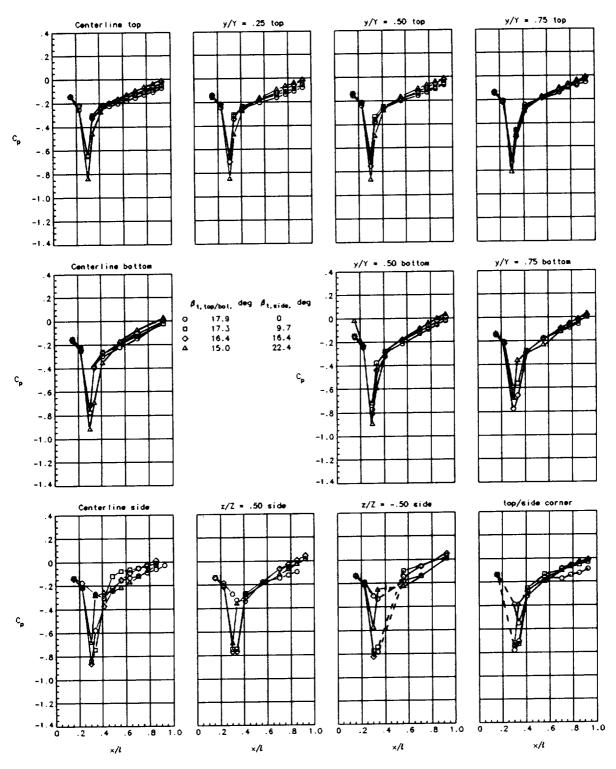
(a) Afterbody drag with plume on.

Figure 16. Effect of closure distribution on nozzles with 2-in. corner radius at $\alpha=0^{\circ}$.



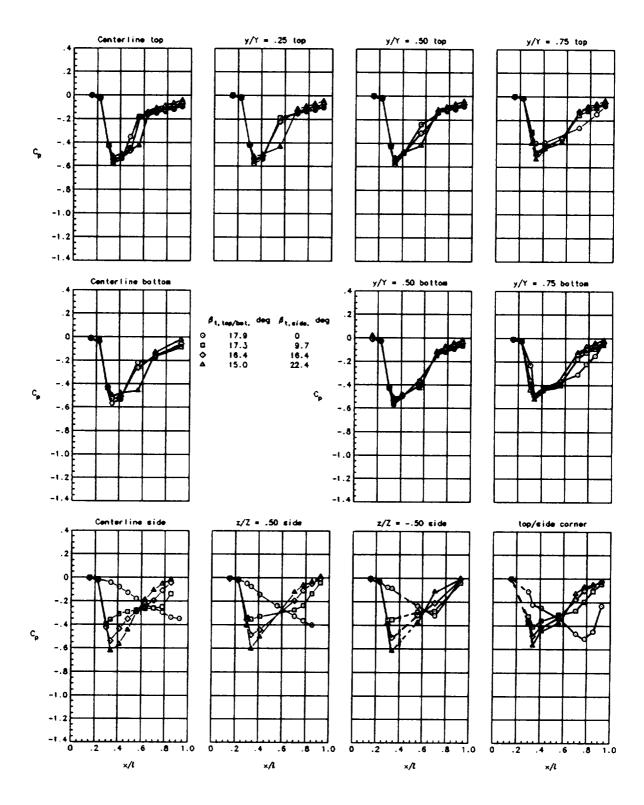
(b) Pressure distributions at $M_{\infty} = 0.6$.

Figure 16. Continued.



(c) Pressure distributions at $M_{\infty} = 0.9$.

Figure 16. Continued.



(d) Pressure distributions at $M_{\infty} = 1.2$.

Figure 16. Concluded.

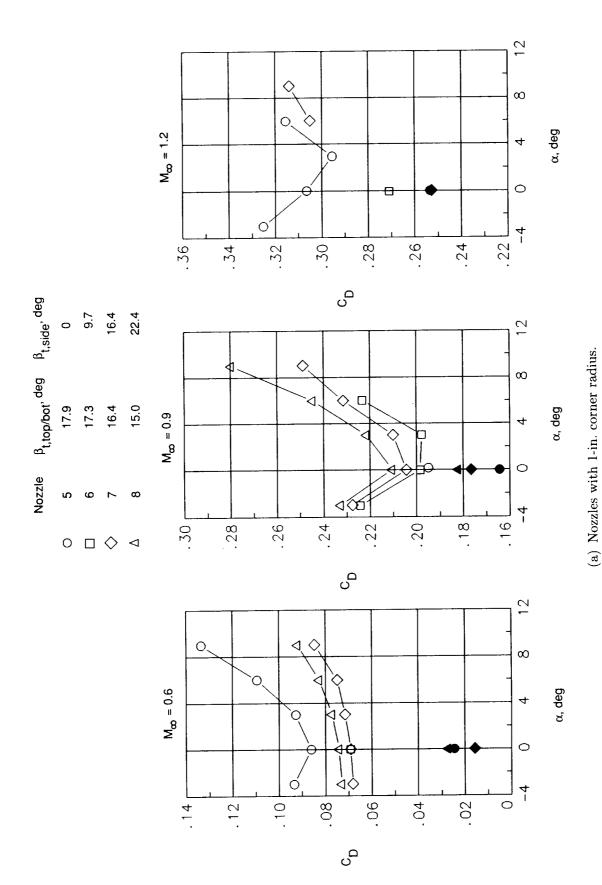
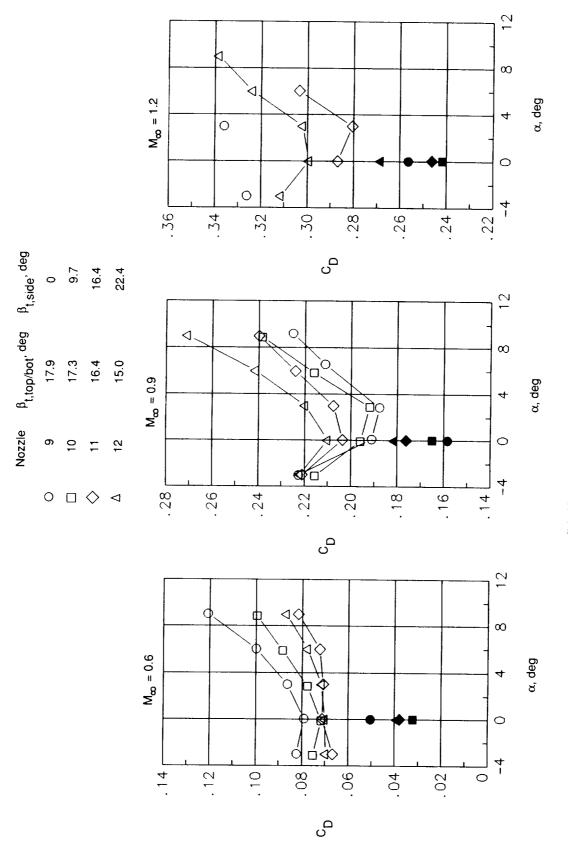


Figure 17. Effect of closure distribution on afterbody drag. Open symbols denote plume off; solid symbols denote plume on.



(b) Nozzles with 2-in. corner radius.

Figure 17. Concluded.

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Form Approved REPORT DOCUMENTATION PAGE OMB No. 0704-0188 Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway. Suite 1204. Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503. 1. AGENCY USE ONLY(Leave blank) 2. REPORT DATE 3. REPORT TYPE AND DATES COVERED September 1992 Technical Paper 4. TITLE AND SUBTITLE 5. FUNDING NUMBERS Effect of Afterbody Geometry on Aerodynamic Characteristics WU 505-62-30-01 of Isolated Nonaxisymmetric Afterbodies at Transonic Mach 6. AUTHOR(S) Linda S. Bangert and George T. Carson, Jr. 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) 8. PERFORMING ORGANIZATION REPORT NUMBER NASA Langley Research Center Hampton, VA 23681-0001 L-17034 9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) 10. SPONSORING/MONITORING **AGENCY REPORT NUMBER** National Aeronautics and Space Administration Washington, DC 20546-0001 NASA TP-3236 11. SUPPLEMENTARY NOTES 12a. DISTRIBUTION/AVAILABILITY STATEMENT 12b. DISTRIBUTION CODE Unclassified Unlimited Subject Category 02 13. ABSTRACT (Maximum 200 words) A parametric study has been conducted in the Langley 16-Foot Transonic Tunnel on an isolated nonaxisymmetric fuselage model that simulates a twin-engine fighter. The effects of aft-end closure distribution (top/bottom nozzle-flap boattail angle versus nozzle-sidewall boattail angle) and afterbody and nozzle corner treatment (sharp or radius) were investigated. Four different closure distributions with three different corner radii were tested. Tests were conducted over a range of Mach numbers from 0.40 to 1.25 and over a range of angles of attack from -3° to 9°. Solid plume simulators were used to simulate the jet exhaust. For a given closure distribution in the range of Mach numbers tested, the sharp-corner nozzles generally had the highest drag and the 2-in. corner-radius nozzles generally had the lowest drag. The effect of closure distribution on afterbody drag was highly dependent on configuration and flight condition. 14. SUBJECT TERMS 15. NUMBER OF PAGES Nonaxisymmetric afterbodies; Afterbody drag; Boattail drag 263 16. PRICE CODE 17. SECURITY CLASSIFICATION 18. SECURITY CLASSIFICATION 19. SECURITY CLASSIFICATION 20. LIMITATION OF REPORT OF THIS PAGE OF ABSTRACT OF ABSTRACT Unclassified Unclassified

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